

TECHNICAL REPORT



Explanation of the mathematical addition of working voltages, insulation
between circuits and use of PELV in TC 34 standards

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INTERNATIONAL ELECTROTECHNICAL COMMISSION

EXPLANATION OF THE MATHEMATICAL ADDITION OF WORKING VOLTAGES, INSULATION BETWEEN CIRCUITS AND USE OF PELV IN TC 34 STANDARDS

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IEC TR 63139, which is a Technical Report, has been prepared by IEC technical committee 34: Lamps and related equipment.

The text of this Technical Report is based on the following documents:

DTR	Report on voting
34/415/DTR	34/493A/RVDTR

Full information on the voting for the approval of this Technical Report can be found in the report on voting indicated in the above table.

This document has been drafted in accordance with the ISO/IEC Directives, Part 2.

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INTRODUCTION

This document provides background information to the following subjects being introduced into IEC TC 34 standards to cover new technologies associated with the use of LED light sources and controllable products.

This document consists of the following subdivisions:

Clause 4 – Mathematical addition of working voltages;

Clause 5 – Insulation between circuits;

Clause 6 – Use of protective extra low voltage (PELV);

Clause 7 – Insulation between LV supply and control line conductors.

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EXPLANATION OF THE MATHEMATICAL ADDITION OF WORKING VOLTAGES, INSULATION BETWEEN CIRCUITS AND USE OF PELV IN TC 34 STANDARDS

1 Scope

This document is related to the insulation coordination in TC 34 standards and provides explanations on mathematical addition of working voltages, insulation between circuits, use of protective extra low voltage (PELV) and insulation between LV supply and control line conductors in order to cover new technologies associated with the use of LED light sources and controllable products.

It describes in which way the addition of supply voltages and working voltages can be arranged for an assessment of the electrical insulation requirements (e.g. creepage distances and clearances) in a system if a first failure occurs.

Furthermore the actual failure scenarios given in IEC 60598-1:2014 and IEC 60598-1:2014/AMD1:2017, Annex X and IEC 61347-1:2015, Clause 15 are explained in greater detail and the rationale behind the protective requirement for each situation is given (e.g. possible LV primary to ELV secondary does not lead to an overburden of the insulation in the second circuit).

This document also describes the possibility to increase immunity and reliability of electronic circuits, used in combination with LEDs, with the use of PELV and the associated safety consequences for this system.

The insulation between LV supply and control line conductors is also important and this document explains why this is an essential safety consideration for a complete installation system.

2 Normative references

There are no normative references in this document.

3 Terms and definitions

No terms and definitions are listed in this document.

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- IEC Electropedia: available at <http://www.electropedia.org/>
- ISO Online browsing platform: available at <http://www.iso.org/obp>

4 Mathematical addition of working voltages

Insulation requirements between live parts and accessible conductive parts as function of the controlgear input/output insulation classification and the insulation class of the luminaire are given in IEC 60598-1:2014, Table X.1 and IEC 61347-1:2015, Table 6.

Insulation requirements in TC 34 standards are based on a hazard assessment with the assumption that a certain failure will occur.

The required insulation is normally based on the working voltage U_{OUT} , but in some specific failure cases when the basic insulation between supply and output of a controlgear fails, the supply voltage should be added to U_{OUT} . For controlgear with double or reinforced insulation between primary (U_{SUPPLY}) and secondary (U_{OUT}) this type of failure is not expected.

In case of failure of the basic insulation within the controlgear the following assumptions are made:

- there is an increased output voltage,
- the luminaire remains working, and the increased voltage is present for a time long enough to create a conduction track across the insulation (known as tracking).

For 50/60 Hz transformers inside the controlgear, this failure condition results in the addition of the voltages that can be calculated by the simple summation of the two values. In electronic controlgear this situation may result in a more complex summation due to the complexity of the oscillating circuit that may influence the result.

The best method to check the output voltage in case of insulation failure is to measure the output voltage directly on a sample of controlgear with the fault simulated. The failure of the insulation and the output voltage should be measured against earth (or zero potential). This method has been found not to be practical due to the following reasons:

- differing supply conditions (voltage/frequency);
- difficulty in simulating exactly the failure condition;
- difficulty in making accurate and reproducible measurements.

For the above mentioned reasons the mathematical calculation of the sum of the voltages has been found to be more appropriate, reproducible and easy to calculate, even if the result may in some cases be lower than the real measurement. Designing and testing the insulation properties of the output circuit with an increased voltage value is considered as a necessary safety provision to cover this first failure condition which can occur inside basic insulated controlgear.

The approximation given by the mathematical calculation is considered to provide sufficient severity, compared to the possible practical failure voltage, to ensure the safety of the product through its lifetime. With the selected formula most of the expected failure cases are covered. Higher voltages occurring in very rare cases will not have any serious impact.

The formulas to be used for combining the input and output voltages of the controlgear, with basic insulation between supply and output, are given in Table 1.

Table 1 – Addition of voltages

U_{supply}	U_{OUT}	Phase relationship	Voltage calculation for insulation design
AC	AC	Same frequency and no phase shift	$U = U_{\text{AC1}} + U_{\text{AC2}}$
AC	AC	Same frequency and with phase shift	$U = \sqrt{U_{\text{AC1}}^2 + U_{\text{AC2}}^2 + 2 U_{\text{AC1}} U_{\text{AC2}} \cos \varphi}$
AC	AC	Different frequency	$U = \sqrt{U_{\text{AC1}}^2 + U_{\text{AC2}}^2}$
AC	DC	No phase shift	$U = \sqrt{U_{\text{AC}}^2 + U_{\text{DC}}^2}$
DC	AC	No phase shift	$U = \sqrt{U_{\text{AC}}^2 + U_{\text{DC}}^2}$
DC	DC	No phase shift	$U = U_{\text{DC1}} + U_{\text{DC2}}$

NOTE 1 Voltages in the table are RMS values.

NOTE 2 The AC and DC calculation is typical for LED applications.

Figure 1 shows the simulation of the possible fault between input and output terminals (red line) with the mathematical calculation providing the expected output voltage that may occur.



Figure 1 – Input/output failure simulation

For background information, the formula $U = \sqrt{U_{\text{AC}}^2 + U_{\text{DC}}^2}$ (line 4 of Table 1) for the specific case of a combination of an AC and DC voltage is derived from the following Formulas (1) to (5). It may be regarded as a showcase for any of the formulas from Table 1.

U is the RMS value (U_{RMS}) of the voltage $u(t)$

$$U = U_{\text{RMS}} = \sqrt{u^2(t)} \quad (1)$$

In the particular case given, $u(t)$ consists of an AC (sinusoidal) part with peak voltage U_1 and frequency ω and a DC part U_{DC} . It can be derived that

$$U^2 = u^2(t) = \frac{\int_0^T u^2(t) dt}{T} = \frac{\int_0^T (U_1 \sin(\omega t) + U_{\text{DC}})^2 dt}{T} =$$

$$\frac{U_1^2}{T} \int_0^T \sin^2(\omega t) dt + \frac{2U_1 U_{\text{DC}}}{T} \int_0^T \sin(\omega t) dt + \frac{1}{T} \int_0^T U_{\text{DC}}^2 dt \quad (2)$$

Evaluating this integral yields

$$U^2 = \frac{1}{2} \frac{U_1^2}{T} \left(t - \frac{1}{\omega} \sin(\omega t) \cos(\omega t) \right) \Big|_{t=0}^{t=T} - \frac{2}{T\omega} U_1 U_{DC} \cos(\omega t) \Big|_{t=0}^{t=T} + \frac{1}{T} U_{DC}^2 T \quad (3)$$

$$U^2 = \frac{U_1^2}{2} + U_{DC}^2 \quad (4)$$

And thus,

$$U = \sqrt{\frac{U_1^2}{2} + U_{DC}^2} = \sqrt{U_{AC}^2 + U_{DC}^2} \quad (5)$$

5 Insulation between circuits

5.1 General

New requirements have been added to those in IEC 60598-1 and IEC 61347-1 concerning the requirements for insulation between different types of circuit and to conductive accessible parts. For insulation requirements between active parts and accessible conductive parts and examples of controlgear with different insulation systems see Table 2 and Figure 2.

In case of a failure in the basic insulation, with the assumptions made in Clause 4, between the supply voltage and the output circuit, the insulation in the second circuit will have an increase chance of failing; this can be regarded as a follow up failure, which is by definition still a single fault. This means that the insulation in the secondary circuit should be able to cope with this higher voltage.

The following explanations provide information regarding the technical rationale associated with these requirements.

The numbers in brackets (1) to (18) detailed in Table 2 refer to the content of IEC 60598-1:2014, Table X.1 and IEC 61347-1:2015, Table 6. A comparison with possible failure conditions is shown in Figures 3 to 7. Each combination has been evaluated and the consequences are listed in 5.3 with the requirements for the insulation which is needed for each numbered case.

5.2 Insulation requirements between active parts and accessible conductive parts

Explanations to the application of the insulation requirements are given in Table 2 and Figure 2.