



Designation: **E2001—13 E2001 – 18**

Standard Guide for Resonant Ultrasound Spectroscopy for Defect Detection in Both Metallic and Non-metallic Parts¹

This standard is issued under the fixed designation E2001; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ϵ) indicates an editorial change since the last revision or reapproval.

1. Scope*

1.1 This guide describes a procedure for detecting defects in metallic and non-metallic parts using the resonant ultrasound spectroscopy method. The procedure is intended for use with instruments capable of exciting and recording whole body resonant states within parts which exhibit acoustical or ultrasonic ringing. It is used to distinguish acceptable parts from those containing defects, such as cracks, voids, chips, density defects, tempering changes, and dimensional variations that are closely correlated with the parts' mechanical system dynamic response.

1.2 The values stated in SI units are to be regarded as standard. No other units of measurement are included in this standard.

1.3 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety, health, and environmental practices and determine the applicability of regulatory limitations prior to use.*

1.4 *This international standard was developed in accordance with internationally recognized principles on standardization established in the Decision on Principles for the Development of International Standards, Guides and Recommendations issued by the World Trade Organization Technical Barriers to Trade (TBT) Committee.*

2. Referenced Documents

2.1 *ASTM Standards:*²

[E1316 Terminology for Nondestructive Examinations](#)

[E1876 Test Method for Dynamic Young's Modulus, Shear Modulus, and Poisson's Ratio by Impulse Excitation of Vibration](#)

[E2534 Practice for Process Compensated Resonance Testing Via Swept Sine Input for Metallic and Non-Metallic Parts](#)

[E3081 Practice for Outlier Screening Using Process Compensated Resonance Testing via Swept Sine Input for Metallic and Non-Metallic Parts](#)

3. Terminology

3.1 *Definitions*—The definitions of terms relating to conventional ultrasonics can be found in Terminology [E1316](#).

3.2 *Definitions of Terms Specific to This Standard:*

3.2.1 *resonant ultrasonic spectroscopy (RUS), n*—a nondestructive examination method, which employs resonant ultrasound methodology for the detection and assessment of variations and mechanical properties of a test object. In this procedure, whereby a rigid part is caused to resonate, the resonances are compared to a previously defined resonance pattern. Based on this comparison the part is judged to be either acceptable or unacceptable.

3.2.2 *swept sine method, n*—the use of an excitation source to create a transient vibration in a test object over a range of frequencies. Specifically, the input frequency is swept over a range of frequencies and the output is characterized by a resonant amplitude response spectrum.

3.2.3 *impulse excitation method, n*—striking an object with a mechanical impact, or electromagnetic field (laser and/or EMAT) Electromagnetic Acoustic Transducer (EMAT) causing multiple resonances to be simultaneously stimulated.

3.2.4 *resonant inspection (RI), n*—any induced resonant nondestructive examination method employing an excitation force to create mechanical resonances for the purpose of identifying a test object's conformity to an established acceptable pattern.

¹ This guide is under the jurisdiction of ASTM Committee [E07](#) on Nondestructive Testing and is the direct responsibility of Subcommittee [E07.06](#) on Ultrasonic Method. Current edition approved Dec. 1, 2013/Nov. 1, 2018. Published January 2014/November 2018. Originally approved in 1998. Last previous edition approved in 2008/2013 as [E2001 – 08](#)/E2001 - 13. DOI: [10.1520/E2001-13](#). [10.1520/E2001-18](#).

² For referenced ASTM standards, visit the ASTM website, [www.astm.org](#), or contact ASTM Customer Service at [service@astm.org](#). For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

*A Summary of Changes section appears at the end of this standard

4. Summary of the Technology (1)³

4.1 Introduction:

4.1.1 In addition to its basic research applications in physics, materials science, and geophysics, Resonant Ultrasound Spectroscopy (RUS) has been used successfully as an applied nondestructive testing tool. Resonant ultrasound spectroscopy in commercial, nondestructive testing has a few recognizable names including, RUS Nondestructive Testing, Acoustic Resonance Spectroscopy (ARS), and Resonant Inspection. Resonant Inspection (RI) and Process Compensated Resonance Testing (PCRT). Early references to this body of science often are termed the “swept sine method.” It was not until 1990 (2) that the name Resonant Ultrasound Spectroscopy appeared, but the two techniques are synonymous. Additionally, impulse methods, like the striking of a rail car wheel with a hammer, and listening for the responses, have been used for over 100 years to detect the existence of large cracks. RUS based techniques are becoming commonly used in the manufacture of steel, ceramic, and sintered metal parts: commonly used to evaluate metallic and nonmetallic material and finished parts made from a variety of processes including casting, forging, sintering, machining and additive manufacturing. In these situations, a part is vibrated mechanically, and defects are detected based on changes in the pattern of resonances or variations from theoretically analytically or numerically calculated or empirically measured acceptable spectra. RUS measures all resonances, resonances of the part in a defined range, of the part frequency range rather than scanning for individual defects. In a single measurement, RUS-based techniques potentially can test for numerous defects including cracks, chips, cold shuts, inclusions, voids, porosity, oxides, contaminants, missed processes or operations, and variations in dimension, hardness, porosity, nodularity, density, and heat treatment. Since the RUS measurement yields a whole-body-whole-body response, it is often difficult to discriminate between defect types. The technique is effective for detecting parts with structural anomalies, but less effective for diagnosing the exact location or cause of an anomaly within a part. Nevertheless, on certain types of parts, it can be accurate, fast, inexpensive and for an expansive range of parts RUS provides accurate, fast, quantitative and cost-effective results that require no human judgment, making 100 % examination possible in selected circumstances of a part population possible. Many theoretical texts (3) discuss the relationship between resonances and elastic constants and include the specific application of RUS to the determination of elastic constants (4). The technology received a quantum increase in attention when Migliori published a review article, including the requisite inexpensive electronic designs and procedures from which materials properties could be measured quickly and accurately (5). The most recent applications include studies in ultrasonic attenuation, modulus determinations, thermodynamic properties, structural phase transitions, superconducting transitions, magnetic transitions, and the electronic properties of solids. A compendium of these applications may be found in the Migliori (1) text. Resonant ultrasound spectroscopy also found use in the study of the elastic properties of the Apollo moon rocks (6).

4.1.2 This guide is intended to provide a practical introduction to RUS-based nondestructive testtesting (NDT), highlighting successful applications and outlining failures, limitations, and potential weaknesses. Vibrational resonances are considered from the perspective of defect detection in 4.2. In 4.3 and 4.4, a review of some of the types of RUS measurements are given and 4.6 examines the common practice of using the impulse excitation method. In 4.6, some example implementations and configurations of RUS systems and their applications are presented. Finally, the guide concludes with a discussion of constraints, which limit the effectiveness of RUS.

4.2 Mode Shapes and Defects:

4.2.1 Resonant ultrasound spectroscopy/NDT techniques, operate by driving a part at given frequencies and measuring its mechanical response (Fig. 1 contains a schematic one embodiment of a RUS apparatus). The process proceeds in small frequency

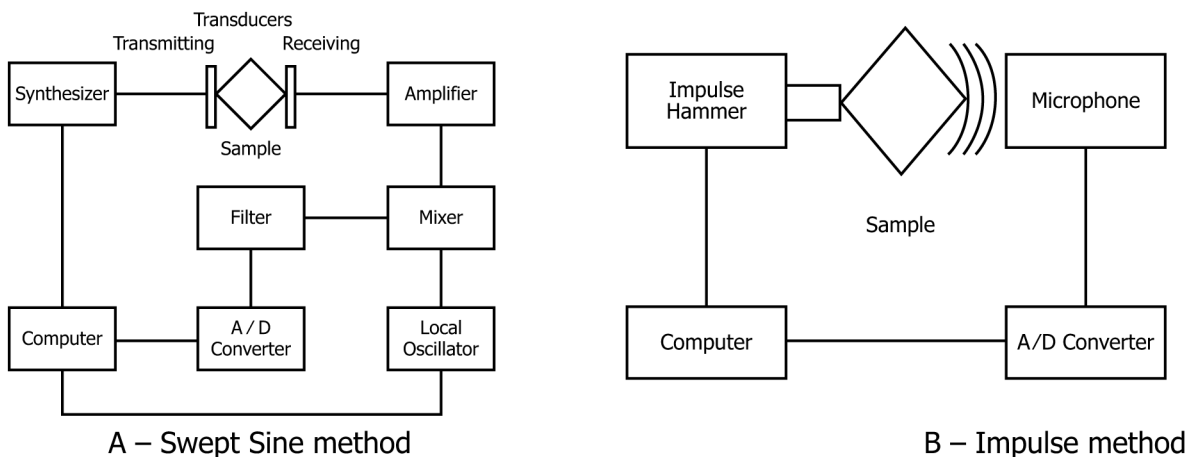


FIG. 1 Schematic of the Essential Electronic Building Blocks to Employ RUS in a Manufacturing Environment

³ The boldface numbers in parentheses refer to the list of references at the end of this guide.

steps over some previously determined region of interest. During such a sweep, the drive frequency typically brackets a resonance. When the excitation frequency is not matched to one of the part's resonance frequencies, very little energy is coupled to the part; that is, there is little mechanical vibration. At resonance, however, the energy delivered to the part is coupled generating much larger mechanical vibrations. A part's resonance frequencies are determined by the standard dynamic equations of motion, which include variables for mass, stiffness, and damping. From a materials perspective, this is affected by its dimensions (to include the shape and geometry) and by the density and the mass, stiffness, and damping properties are determined by geometry, density, and material elastic constants of the material part. The required frequency window and data collection parameters for a scan depends on the size of the part, its mechanical rigidity, and the size of the defect being sought depend on the part geometry, mass, material properties, and the characteristics of the defects of interest.

4.2.2 Vibrational resonances produce a wide range of distortions. These distortions include shapes, which bend and twist. It is known that increasing the length of a cylinder will lower some resonant frequencies. Similarly, reducing the stiffness, that is, reducing the relevant elastic constant, lowers the associated resonant frequency for most modes; thus, for a given part, the resonant frequencies are measures of stiffness, and knowledge of the mode shape helps to determine what qualities Exciting a part at its resonance frequencies will cause the part to deform in an array of patterns that correspond to different frequencies. These deformation patterns are called mode shapes. Bending, torsional (twisting) and extensional (breathing) modes are common shapes in simple geometries like cylinders. More complex and/or localized variations on these shapes will be excited in more complex geometries. A large enough frequency range excited by either a swept sine or impulse input will excite multiple harmonics of the same mode shape (first bending mode, second bending mode, and so on). Fig. 2 of the part affect those frequencies. If a defect, such as a crack, is introduced into shows an example of mode shapes excited in a portion of the resonance spectra for a basic cylinder. Modes 7 and 8 are a pair of degenerate bending modes (see 4.3.4.1 a region under strain, it will reduce the effective stiffness, that is, the part's resistance to deformation, and will shift downward the frequency of resonant modes that introduce strain at the crack. This is one basis for detecting defects with RUS-based techniques. for a description of degenerate modes). Mode 9 is a torsional mode. Mode 10 is an extensional mode. Modes 11 and 12 are the next harmonic of the bending mode. Mode 13 is the next harmonic of the torsional mode.

4.2.3 The torsional modes represent a twisting of a cylinder about its axis. These resonances are easily identified because their frequencies remain constant for fixed length, independent of diameter. A crack will Different mode shapes have varying sensitivities to geometric variations, material state variations, and flaws in parts. Knowledge of the mode shape helps to determine what qualities of the part affect those frequencies. The resonance frequencies of a part correlate directly to its stiffness (resistance to deformation). Reducing the part stiffness by reducing the relevant elastic constant lowers the associated resonant frequency for most modes. If a defect, such as a crack, is introduced into a region under strain, it will reduce the effective stiffness in that area and cause a downward shift of the frequency of resonant modes that introduce strain at the crack. For example, a crack may reduce the ability of the part to resist twisting, thereby reducing the effective stiffness, stiffness and thus, the frequency of a torsional mode. Geometric variations also affect resonance modes to varying degrees. For example, increasing the length of a cylinder will lower resonant frequencies of bending modes more than torsional or extensional modes. Torsional modes in a cylinder remain constant for fixed length, independent of diameter variation. Variation in the size of a given defect also changes which modes are affected and the magnitude of that effect. A large defect can be detected readily by its effect on the first few modes; however, smaller modes. Smaller defects have much more subtle effects on stiffness, and therefore, require requiring higher frequencies (high-order modes) to be detected. Detection of very small defects may require using the frequency corresponding to the fiftieth, or even higher, mode. Some In the cylinder example, some modes do not produce strain in the end of the cylinder, therefore, they cannot detect end

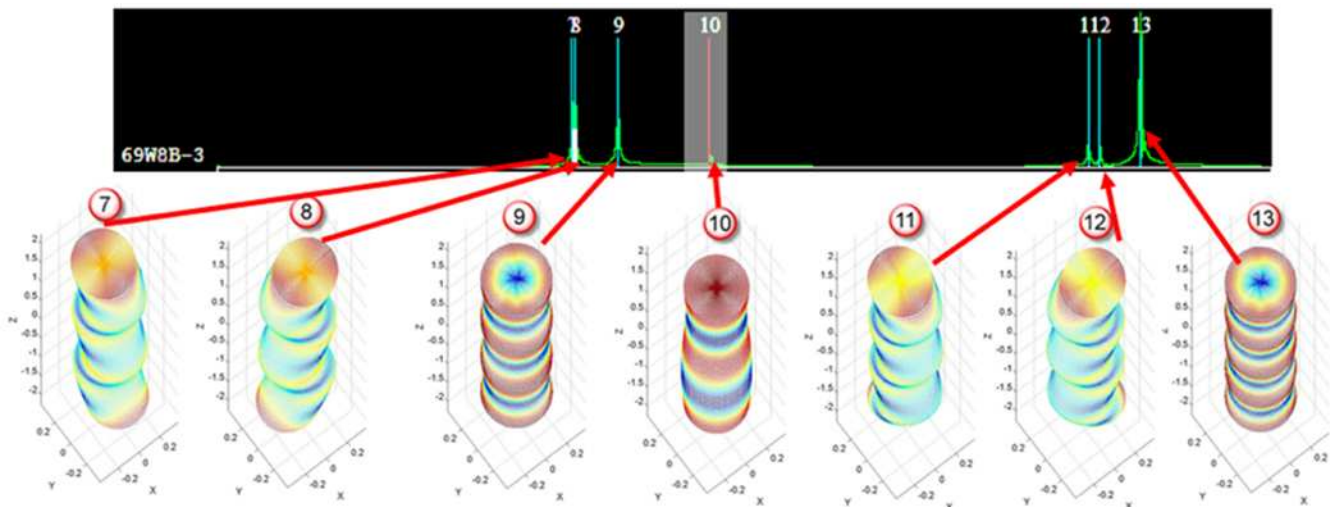


FIG. 2 Examples of Modes of Vibration Matched to Their Peaks in a Resonance Spectrum

defects. To detect this type of defect, a more complex mode is required, the description of which is beyond the scope of this specification. A defect in the cylinder end will reduce the effective stiffness for this type of mode, and thus, will shift downward the frequency of the resonance. In general, it must be remembered that most modes will exhibit complex motions, and for highly symmetric objects, can be linear combinations of several degenerate modes, as discussed in 4.3.2.

4.3 General Approaches to RUS/NDT:

4.3.1 Test Evaluation Methods (1)—Once a fingerprint has been established, for conforming parts, numerous algorithms can be employed to either accept or reject the part. For example, if a frequency ± 50 Hz can be identified for all conforming parts, the detection of a peak outside of this boundary condition will cause the computer code to signal a “test reject” condition. The code, rather than the inspector, makes the accept/reject decision. The following sections will expand on some of these sorting criteria.

4.3.2 Frequency Shifts:

4.3.2.1 Resonant ultrasound spectroscopy measurements generally produce strains (even on resonance) that are well within the elastic limit of the materials under test, that is, the atomic displacements are small in keeping with the “nondestructive” aspect of the testing. If strains are applied above the elastic limit, a crack will tend to propagate, causing a mechanical failure. Note that certain important engineering properties, for example, the onset of plastic deformation, yield strength, etc., generally are not derivable from low-strain elastic properties. Sensitivity of the elastic properties of an object to the presence of a crack depends on the stiffness and geometry of the sample under test. This concept is expanded upon under 4.4.3.

4.3.2.2 Fig. 23 shows an example of the resonance spectrum for a conical ceramic part. Several specific types of modes are present in this scan, and their relative shifts could be used to detect defects as discussed above; however, the complexity is such that, for NDT purposes, some selections must be made so that only a portion of such a large amount of information is used. For simple part geometries, the mode type and frequency can be calculated, and selection of diagnostic modes can be based on these results. For complex geometries, empirical approaches have been developed to identify efficiently diagnostic modes for specific defects. In this process, a technician measures the spectra for a batch of known good and bad parts. The spectra are compared to identify diagnostic modes whose shift correlates with the presence of the defect. The key is to isolate a few resonances, which differ from one another, when known defects are present in the faulty parts.

4.3.3 Peak Splitting—One of the techniques employed for axially symmetric parts is identified in texts on basic wave physics (7). Some test procedures are based on simple frequency changes while others include the recognition that symmetry is broken when a defect is present in a homogeneous, isotropic symmetrical part. These techniques employ splitting of degeneracies or simply “splitting.” A cylinder actually has two degenerate bending modes, both orthogonal to its axis. The bending stiffness for both of these modes, and therefore their resonance frequency, is proportional to the diameter of the cylinder. Because the part is symmetric, both modes have the same stiffness, and therefore, the same frequency (the modes are said to be degenerate and appear to be a single resonance). When the symmetry is broken by a chip, however, the effective diameter is reduced for one of the orthogonal modes. This increases the frequency for that mode, so both modes are seen. In addition, a crack or inclusion affects

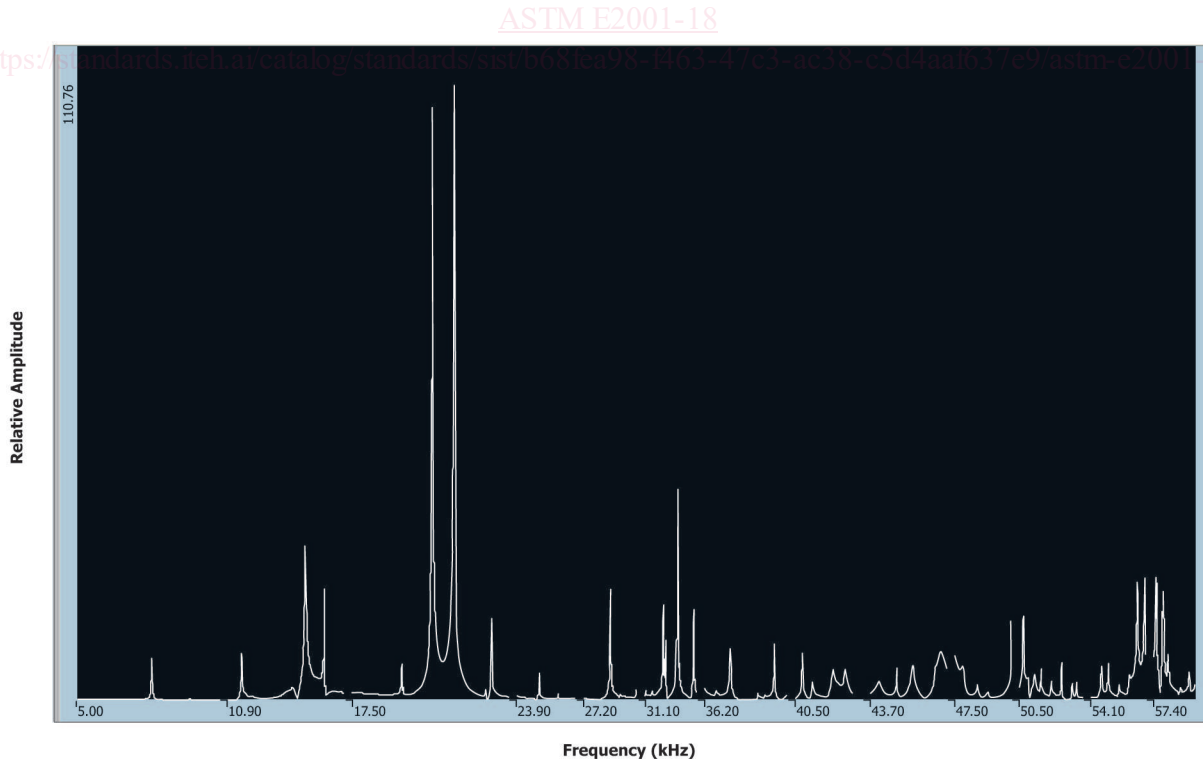


FIG. 23 Typical Broad-Spectrum Scan

the symmetry. This splitting of the resonances is illustrated in Fig. 34, which shows spectra for a good part and two defective parts. The part is a steel cylinder. Fig. 34 also demonstrates a useful feature of this particular technique, that is, the size of the splitting is proportional to the size of the defect. It is important to recognize that not all resonance peaks are degenerate. Pure torsional modes, for example, are not degenerate, so they cannot be used for splitting.

4.3.4 Phase Information and Peak Splittings:

4.3.4.1 Degenerate modes all have the same phase at low-symmetry points; therefore, if one mode is shifted slightly destructive interference occurs between them, showing up as a splitting if the sample rigidity is sufficient. Mode pairs 7 and 8, 11 and 12 from Fig. 2 are examples of degenerate mode pairs. The frequency difference between the two resulting peaks increases in direct proportion to the defect size. This does not hold for accidental degeneracies, which are modes that by coincidence rather than by symmetry have the same frequency. The actual shift in frequency is no more than would be expected for an isolated mode, but the interference enhances the visibility.

4.3.4.2 In practice, the same empirical approach described for frequency shifts is used to identify diagnostic modes whose splittings correlatesplitting correlates with the size of a defect of interest. The sensitivity of this type of measurement is enhanced by the interference, which occurs between closely-spaced peaks. The destructive interference develops into a visible spectral splitting which would not be noticeable with the amplitude spectrum (the real and quadrature components add to form the amplitude response). Most commercial systems function reasonably well without this attribute, but the problem can be exacerbated when the material exhibits resonance line widths which are greater than 1 % of the frequency. Under such circumstances, it may be impossible to detect splittingsplitting without phase information.

4.3.4.2 Degenerate modes all have the same phase at low-symmetry points; therefore, if one mode is shifted slightly destructive interference occurs between them, showing up as a splitting if the sample rigidity is sufficient. The frequency difference between the two resulting peaks increases in direct proportion to the defect size. This does not hold for accidental degeneracies, which are modes that by coincidence rather than by symmetry have the same frequency. The actual shift in frequency is no more than would be expected for an isolated mode, but the interference enhances the visibility.

4.3.5 Dimensional Measurements:

4.3.5.1 Industrial sortingevaluation of parts often occurs in two sectors: defect detection and dimensional examination. Ceramic plants often spend more resources on the latter than crack and chip investigations. several sectors: defect detection, screening of outlier spectrum, manufacturing or repair process monitoring, and dimensional examination. It is a relatively simple matter to use RUS techniques to measure physical parameters, such as weight, density, and dimensions. In practice, one measures all the physical attributes possible. For a ring, these would include weight, thickness, outer diameter, and inner diameter. It is imperative to use

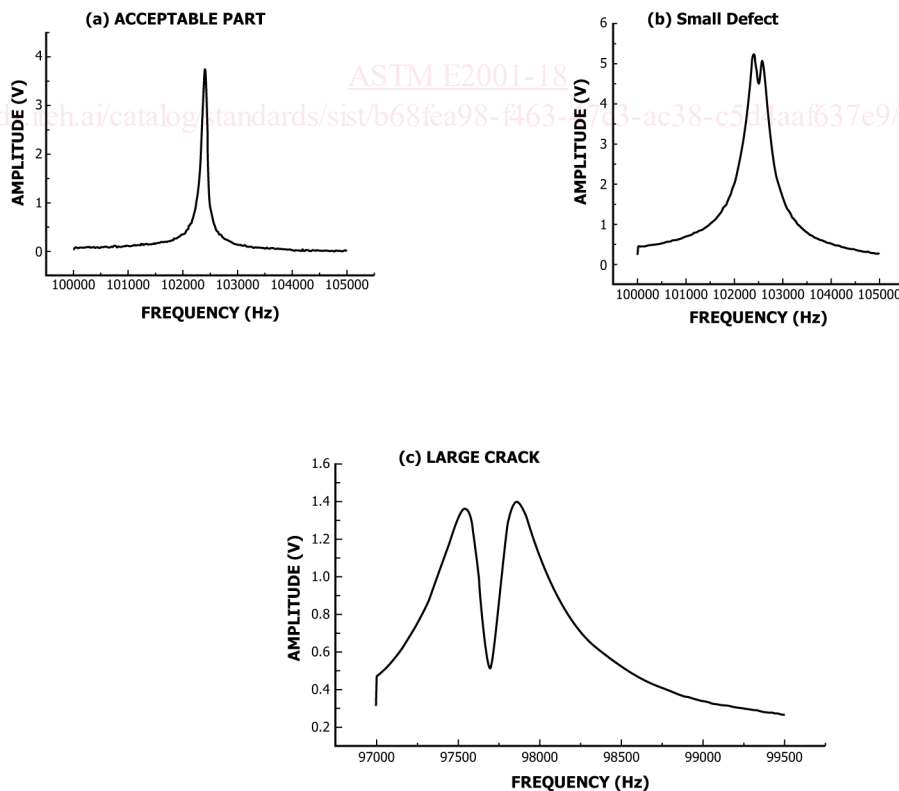


FIG. 34 Shown is a Bending Mode Within a Resonance Spectrum of an Acceptable Steel Cylinder (a), One With a Small Defect (b), and One With a Large Crack (c).

“good”, that is, as free of defects as possible, parts in this study. One measures a suitable number of the lowest resonances and either plots each resonance frequency as a function of each parameter or uses the correlation feature of standard spreadsheet programs. The best results are obtained when singlets (single resonances) or nondegenerate modes are used. Statistical analysis will reveal which resonances have significant correlations with the desired physical attribute.

4.3.5.2 Usually, these measurements are performed in conjunction with crack/chip/seam detection. Resonant ultrasound spectroscopy techniques often have to accommodate shifts in resonance frequencies associated with density differences in addition to those resulting from dimensional variations with sintered parts (ceramics and powder metals). As long as the part is within the tolerance limits, and no other critical defect is present, it is acceptable to pass the item. This is accomplished by varying the frequency window that is scanned. Fig. 45 illustrates the ability to determine the thickness of an alumina washer. Twenty washers were measured with an accuracy of $\sim 1 \mu\text{m}$ and the results are plotted against the frequency of specific resonances.

4.4 Practical Considerations:

4.4.1 Implementation:

4.4.1.1 An integration of RUS techniques into a manufacturing process is illustrated in Fig. 56 as an example of how the ideas of 4.3 are integrated into a commercial swept sine product. The key element is the synthesizer/receiver of which several commercial instruments exist. It generates a swept sine oscillation over a defined range as a continuous wave (CW) electrical signal, and then moves to the next defined range. This pattern is replicated until the scan is completed. Either a piezoelectric or an EMAT (8) transducer converts the electrical signal into a mechanical vibration which excites the part. A second transducer senses the vibration and converts it back to electrical energy. The receiver detects the signal and performs an analog to digital conversion. Then, a computer processes the signal and displays the frequency spectrum. If the measurement is being performed in a laboratory, the spectrum is analyzed visually to observe shifts, splits, or other phenomena of interest. In a production environment, a display is neither required nor even desirable under some circumstances. The computer applies an algorithm that passes or rejects the part based on predetermined criteria as described above. The time required for a measurement depends on the size of the part and the mechanical attenuation (defined by the resonance line width) of the material, as discussed in Migliori’s textbook (1). Mode measurement times in some particular systems may typically range from 0.25 to 2 s/mode (depending on their stiffness) and a particular part may require two to five modes to check for all types of defects, as shown in Fig. 56. Practice Practices E2534 details and E3081 detail the application of the swept sine method to RUS input method to RUS using several different approaches for resonance spectra analysis.

4.4.1.2 Integration of the impulse excitation RUS technique into the manufacturing process is illustrated in Fig 1b. The key elements are: an impact device, to excite the structure with broadband energy, and a microphone to sense the acoustic response. The microphone signal is digitized and a computer is used to process the signal into a frequency representation by using a Fourier Transform. The spectrum is then analyzed, in a nearly identical fashion to that described in 4.4.1.1. The time required for this measurement is shorter than swept sine, as all modes are excited and measured simultaneously. However, the frequency range excited by the impulse method is more limited than swept sine.

4.4.1.3 A specific application requires the development of a complete NDT system. This system is defined by measuring the part for all of the types of the defects of interest and integrating the RUS measurement system with materials handling equipment and with appropriate control hardware and software. Fig. 56 illustrates the type of defects, which can be found using RUS (9). Five modes are used to detect the various defects of concern. The first mode is a bending mode, which measures mode with deformation in the top, washer-shaped section of the part. The second mode is a bending mode for in the lower, rounded conical section of the part. It is sensitive to circumferential defects. The third mode is a breathing mode for in the conical section. It is sensitive to axial defects. The fourth mode is a transverse bending mode for in the washer section, particularly sensitive to gross cracks in the section that move the first mode outside the measurement window. The fifth mode is a bending mode for in the tip. The frequencies of the

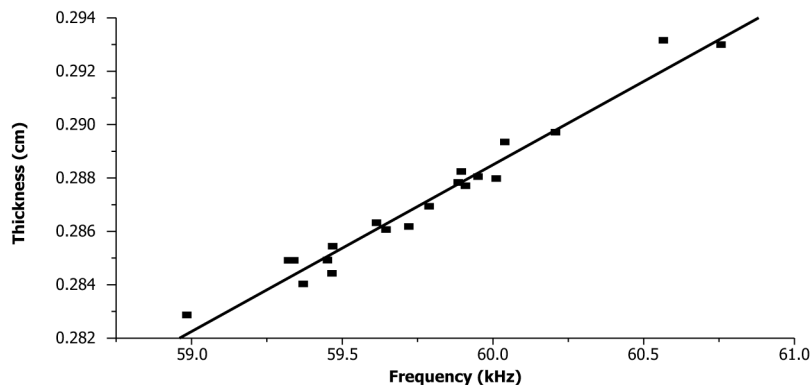


FIG. 45 Illustrates the Result of Measuring Ceramic Washers With a Digital Micrometer and Plotting the Thickness Against a Specific Resonance Mode