

Edition 3.0 2021-10

# INTERNATIONAL STANDARD

# NORME INTERNATIONALE

HORIZONTAL PUBLICATION

**PUBLICATION HORIZONTALE** 

Fire hazard testing Teh STANDARD PREVIEW

Part 5-1: Corrosion damage effects of fire effluent - General guidance (Standards.iteh.ai)

Essais relatifs aux risques du feu – Partie 5-1: Effets des dommages de corrosion des effluents du feu – Recommandations générales 69dc6507/iec-60695-5-1-2021





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# INTERNATIONAL STANDARD

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HORIZONTAL PUBLICATION

**PUBLICATION HORIZONTALE** 

Fire hazard testing Teh STANDARD PREVIEW
Part 5-1: Corrosion damage effects of fire effluent General guidance

Essais relatifs aux risques du feu <u>C 60695-5-1:2021</u>

Partie 5-1: Effets des dommages de corrosion des effluents du feu – Recommandations générales fb9dc6507/iec-60695-5-1-2021

INTERNATIONAL
ELECTROTECHNICAL
COMMISSION

COMMISSION ELECTROTECHNIQUE INTERNATIONALE

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#### INTERNATIONAL ELECTROTECHNICAL COMMISSION

#### FIRE HAZARD TESTING -

### Part 5-1: Corrosion damage effects of fire effluent – General guidance

#### **FOREWORD**

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International Standard IEC 60695-5-1 has been prepared by IEC technical committee 89: Fire hazard testing.

This third edition cancels and replaces the second edition, published in 2002, and constitutes a technical revision.

This edition includes the following significant technical changes with respect to the previous edition:

- a) References to IEC TS 60695-5-3 (withdrawn in 2014) have been removed.
- b) References to IEC 60695-1-1 are now to its replacements: IEC 60695-1-10 and IEC 60695-1-11.
- c) ISO/TR 9122-1 has been revised by ISO 19706.
- d) Table 1 has been updated.

- e) References to ISO 11907-2 and ISO 11907-3 have been removed.
- f) Terms and definitions have been updated.
- g) Text in 6.4 has been updated.
- h) Bibliographic references have been updated.

The text of this International Standard is based on the following documents:

FDIS	Report on voting
89/1539/FDIS	89/1543/RVD

Full information on the voting for its approval can be found in the report on voting indicated in the above table.

The language used for the development of this International Standard is English.

This document was drafted in accordance with ISO/IEC Directives, Part 2, and developed in accordance with ISO/IEC Directives, Part 1 and ISO/IEC Directives, IEC Supplement, available at <a href="https://www.iec.ch/members\_experts/refdocs">www.iec.ch/members\_experts/refdocs</a>. The main document types developed by IEC are described in greater detail at <a href="https://www.iec.ch/standardsdev/publications">www.iec.ch/standardsdev/publications</a>.

It has the status of a basic safety publication in accordance with IEC Guide 104 and ISO/IEC Guide 51.

iTeh STANDARD PREVIEW

In this standard, the following print types are used: (Standards.iteh.ai)

Arial **bold**: terms referred to in Clause 2

IEC 60695-5-1:2021

This standard is to be read in conjunction with IEC TS 60695-5-2134-47f4-8dda-

A list of all parts in the IEC 60695 series, published under the general title *Fire hazard testing*, can be found on the IEC website.

The committee has decided that the contents of this document will remain unchanged until the stability date indicated on the IEC website under webstore.iec.ch in the data related to the specific document. At this date, the document will be

- reconfirmed,
- withdrawn,
- replaced by a revised edition, or
- amended.

#### INTRODUCTION

In the design of an electrotechnical product the risk of fire and the potential hazards associated with fire need to be considered. In this respect the objective of component, circuit and equipment design, as well as the choice of materials, is to reduce the risk of fire to a tolerable level even in the event of reasonably foreseeable (mis)use, malfunction or failure.

IEC 60695-1-10, IEC 60695-1-11, and IEC 60695-1-12 [1]<sup>1</sup> provide guidance on how this is to be accomplished.

Fires involving electrotechnical products can also be initiated from external non-electrical sources. Considerations of this nature are dealt with in an overall fire hazard assessment.

The aim of the IEC 60695 series is to save lives and property by reducing the number of fires or reducing the consequences of the fire. This can be accomplished by:

- trying to prevent ignition caused by an electrically energised component part and, in the event of ignition, to confine any resulting fire within the bounds of the enclosure of the electrotechnical product.
- trying to minimise flame spread beyond the product's enclosure and to minimise the harmful effects of fire effluents including heat, smoke, and toxic or corrosive combustion products.

All **fire effluent** is corrosive to some degree and the level of potential to corrode depends on the nature of the fire, the combination of combustible materials involved in the fire, the nature of the substrate under attack, and the temperature and relative humidity of the environment in which the **corrosion damage** is taking place. There is no evidence that **fire effluent** from electrotechnical products offers greater risk of **corrosion damage** than the **fire effluent** from other products such as furnishings or building materials.

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The performance of electrical and electronic components can be adversely affected by corrosion damage when subjected to fire effluent. A wide variety of combinations of small quantities of effluent gases, **smoke** particles, moisture and temperature may provide conditions for electrical component or system failures from breakage, overheating or shorting.

Evaluation of potential **corrosion damage** is particularly important for high value and safety-related electrotechnical products and installations.

Technical committees responsible for products will choose the test(s) and specify the level of severity.

The study of **corrosion damage** requires an interdisciplinary approach involving chemistry, electricity, physics, mechanical engineering, metallurgy and electrochemistry. In the preparation of this part of IEC 60695-5, all of the above have been considered.

IEC 60695-5-1 defines the scope of the guidance and indicates the field of application.

IEC TS 60695-5-2 provides a summary of test methods including relevance and usefulness.

Numbers in square brackets refer to the bibliography.

#### FIRE HAZARD TESTING -

### Part 5-1: Corrosion damage effects of fire effluent – General guidance

#### 1 Scope

This part of IEC 60695 provides guidance on the following:

- a) general aspects of corrosion damage test methods;
- b) methods of measurement of corrosion damage;
- c) consideration of test methods;
- d) relevance of **corrosion damage** data to hazard assessment.

This basic safety publication is primarily intended for use by technical committees in the preparation of standards in accordance with the principles laid down in IEC Guide 104 and ISO/IEC Guide 51. It is not intended for use by manufacturers or certification bodies.

One of the responsibilities of a technical committee is, wherever applicable, to make use of basic safety publications in the preparation of its publications. The requirements, test methods or test conditions of this basic safety publication will not apply unless specifically referred to or included in the relevant publications.

### 2 Normative references <u>IEC 60695-5-1:2021</u>

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The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

IEC 60695-1-10, Fire hazard testing – Part 1-10: Guidance for assessing the fire hazard of electrotechnical products – General guidelines

IEC 60695-1-11, Fire hazard testing – Part 1-11: Guidance for assessing the fire hazard of electrotechnical products – Fire hazard assessment

IEC TS 60695-5-2, Fire hazard testing – Part 5-2: Corrosion damage effects of fire effluent – Summary and relevance of test methods

IEC GUIDE 104, The preparation of safety publications and the use of basic safety publications and group safety publications

ISO/IEC Guide 51, Safety aspects - Guidelines for their inclusion in standards

ISO 11907-1:2019, Plastics – Smoke generation – Determination of the corrosivity of fire effluents – Part 1: General concepts and applicability

ISO 13943:2017, Fire safety – Vocabulary

ISO 19706:2011, Guidelines for assessing the fire threat to people

#### Terms and definitions

For the purposes of this document, the following terms and definitions apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- IEC Electropedia: available at http://www.electropedia.org/
- ISO Online browsing platform: available at http://www.iso.org/obp

#### corrosion damage

physical and/or chemical damage or impaired function caused by chemical action

[SOURCE: ISO 13943:2017, 3.69]

#### 3.2

#### corrosion target

sensor used to determine the degree of corrosion damage (3.1), under specified conditions

Note 1 to entry: This sensor may be a product, a component. It may also be a reference material or object used to simulate the behaviour of a product or a component.

# [SOURCE: ISO 13943:2017, 3.70] TANDARD PREVIEW

(standards.iteh.ai)

#### 3.3

#### fire decay

stage of fire development after a fire has reached its maximum intensity and during which the heat release rate and the temperature of the fire are decreasing

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[SOURCE: ISO 13943:2017, 3.1221cfb9dc6507/iec-60695-5-1-2021

#### 3.4

### fire effluent

all gases and aerosols, including suspended particles, created by combustion or pyrolysis (3.9) and emitted to the environment

[SOURCE: ISO 13943:2017, 3.123]

#### 3.5

#### fire scenario

qualitative description of the course of a fire with respect to time, identifying key events that characterize the studied fire and differentiate it from other possible fires

Note 1 to entry: See fire scenario cluster (ISO 13943:2017, 3.154) and representative fire scenario (ISO 13943:2017, 3.153).

Note 2 to entry: It typically defines the ignition and fire growth processes, the fully developed fire stage, the fire decay (3.3) stage, and the environment and systems that will impact on the course of the fire.

Note 3 to entry: Unlike deterministic fire analysis, where fire scenarios are individually selected and used as design fire scenarios, in fire risk assessment, fire scenarios are used as representative fire scenarios within fire scenario clusters.

[SOURCE: ISO 13943:2017, 3.152]

#### 3.6

#### flashover

<stage of fire> transition to a state of total surface involvement in a fire of combustible materials within an enclosure

[SOURCE: ISO 13943:2017, 3.184]

#### 3.7

#### full developed fire

state of total involvement of combustible materials in a fire

[SOURCE: ISO 13943:2017, 3.192]

#### 3.8

#### leakage current

electrical current flowing in an undesired circuit

#### 3.9

#### physical fire model

laboratory process, including the apparatus, the environment and the fire test procedure intended to represent a certain phase of a fire

[SOURCE: ISO 13943:2017, 3.298]

### iTeh STANDARD PREVIEW

#### 3.10

## pyrolysis (standards.iteh.ai) chemical decomposition of a substance by the action of heat

Note 1 to entry: Pyrolysis is often used to refer to a stage of fire before flaming combustion has begun.

Note 2 to entry: In fire science, no assumption is made about the presence or absence of oxygen.

[SOURCE: ISO 13943:2017, 3.316]

#### 3.11

#### small-scale fire test

fire test performed on a test specimen of small dimensions

Note 1 to entry: There is no clear upper limit for the dimensions of the test specimen in a small-scale fire test. In some instances, a fire test performed on a test specimen with a maximum dimension of less than 1 m is called a small-scale fire test. However, a fire test performed on a test specimen of which the maximum dimension is between 0,5 m and 1,0 m is often called a medium-scale fire test.

[SOURCE: ISO 13943:2017, 3.346]

#### 3.12

#### smoke

visible part of a fire effluent

[SOURCE: ISO 13943:2017, 3.347]

#### 4 Fire scenarios and physical fire models

During recent years, major advances have been made in the analysis of **fire effluents**. It is recognized that the composition of the mixture of combustion products is particularly dependent upon the nature of the combusting materials, the prevailing temperatures and the ventilation conditions, especially access of oxygen to the seat of the fire. Table 1 shows how the different stages of a fire relate to the changing atmosphere. Conditions for use in laboratory scale tests can be derived from the table in order to correspond, as far as possible, to full-scale fires.

Fire involves a complex and interrelated array of physical and chemical phenomena. As a result, it is difficult to simulate all aspects of a real fire in laboratory scale apparatus. This problem is perhaps the single most perplexing technical problem associated with all fire testing.

General guidance for assessing the fire hazard of electrotechnical products is given in IEC 60695-1-10. Guidance concerning fire hazard assessment is given in IEC 60695-1-11.

ISO 11907-1 defines terms related to smoke corrosivity as well as smoke acidity and smoke toxicity. It presents the scenario-based approach that controls smoke corrosivity. It describes the test methods to assess smoke corrosivity at laboratory scale and deals with test applicability and post-exposure conditions.

After ignition, fire development may occur in different ways depending on the environmental conditions, as well as on the physical arrangement of the combustible materials. However, a general pattern can be established for fire development within a compartment, where the general temperature-time curve shows three stages, plus a **fire decay** stage (see Figure 1).

Stage 1 (non-flaming decomposition) is the incipient stage of the fire prior to sustained flaming, with little lise in the fire room temperature. Ignition and smoke generation are the main hazards during this stage. 66cfb9dc6507/iec-60695-5-1-2021

Stage 2 (developing fire) starts with ignition and ends with a rapid rise in fire room temperature. Spread of flame and heat release are the main hazards in addition to **smoke** during this stage.

Stage 3 (fully developed fire) starts when the surface of all of the combustible contents of the room has decomposed to such an extent that sudden ignition occurs all over the room, with a rapid and large increase in temperature (**flashover**).

At the end of Stage 3, the combustibles and/or oxygen have been largely consumed and hence the temperature decreases at a rate which depends on the ventilation and the heat and mass transfer characteristics of the system. This is known as the **fire decay** stage.

In each of these stages, a different mixture of decomposition products may be formed and this, in turn, influences the corrosive potential of the **fire effluent** produced during that stage.

Characteristics of these fire stages are given in Table 1.

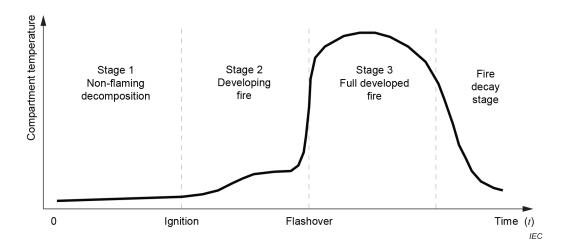


Figure 1 - Different stages in the development of a fire within a compartment

#### 5 General aspects of the corrosivity of fire effluent

#### 5.1 Corrosion damage scenarios

With respect to electrotechnical equipment and systems, there are three corrosion damage scenarios which are of concern:

- a) within electrotechnical equipment and systems when exposed to **fire effluent** caused by unusual, localized, internal sources of excessive heat and ignition;
- b) within electrotechnical equipment and systems when exposed to fire effluent caused by external sources of flame or excessive heat:
- c) within building structures when exposed to **fire effluent** emitted from electrotechnical equipment and systems.

Table 1 - Characteristics of fire stages (from Table 1 of ISO 19706:2011)

	Heat flux to	Max. temperature	ature	Oxygen	Oxygen volume	Fuel/air	[00]	100×[CO <sub>2</sub> ] %
Fire stage	fuel surface	ANDARD PR	2 FVIEW	5	%	equivalence	[CO <sub>2</sub> ]	([CO <sub>2</sub> ]+[CO])
	kW/m²	Fuel surface	Upper layer	Entrained	Exhausted	ratio (plume)	^/^	efficiency
1. Non-flaming	1S)	andards.iten.	.al)					
a. self-sustaining (smouldering)	not applicable	IEC 45859-3-0021	25 to 85 <sup>d</sup>	20	20	I	0,1 to 1	50 to 90
b. oxidative pyrolysis from <sup>lttp:</sup> externally applied radiation	%//standards.ik -	standards.iteh.ailcatalog/standards/sist/a4669 66cfb9dc6 <b>:300/trs-600/a</b> 5-5-1-3	od55-a134-47f4-8d 2021 b	.da- 20	20	< 1	ο	o
<ul><li>c. anaerobic pyrolysis from externally applied radiation</li></ul>	I	100 to 500	q	0	0	1 <<	υ	o
2. Well-ventilated flaming <sup>d</sup>	0 to 60	350 to 650	50 to 500	≈ 20	≈ 20	<b>1</b> >	< 0,05 e	> 95
3. Underventilated flaming <sup>f</sup>								
<ul> <li>a. small, localized fire, generally in a poorly ventilated compartment</li> </ul>	0 to 30	300 to 600 <sup>a</sup>	50 to 500	15 to 20	5 to 10	1 <	0,2 to 0,4	70 to 80
b. post-flashover fire	50 to 150	350 to 650 <sup>g</sup>	009 <	< 15	< 5	> 1 h	0,1 to 0,4 <sup>i</sup>	70 to 90

The upper limit is lower than for well-ventilated flaming combustion of a given combustible.

The temperature in the upper layer of the fire room is most likely determined by the source of the externally applied radiation and room geometry.

There are few data, but for pyrolysis this ratio is expected to vary widely depending on the material chemistry and the local ventilation and thermal conditions.

The fire's oxygen consumption is small compared to that in the room or the inflow, the flame tip is below the hot gas upper layer or the upper layer is not yet significantly vitiated to increase the CO yield significantly, the flames are not truncated by contact with another object, and the burning rate is controlled by the availability of fuel. p

The ratio can be up to an order of magnitude higher for materials that are fire-resistant. There is no significant increase in this ratio for equivalence ratios up to  $\approx 0,75$ . Between  $\approx 0,75$  and 1, some increase in this ratio may occur.

The fire's oxygen demand is limited by the ventilation opening(s); the flames extend into the upper layer.

Assumed to be similar to well-ventilated flaming.

The plume equivalence ratio has not been measured; the use of a global equivalence ratio is inappropriate.

Instances of lower ratios have been measured. Generally, these result from secondary combustion outside the room vent.