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Part 17: Electronic characteristic measurements – Local critical current density and its distribution in large-area superconducting films

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Part 17: Electronic characteristic measurements – Local critical current density and its distribution in large-area superconducting films

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IEC 61788-17 has been prepared by IEC technical committee 90: Superconductivity. It is an International Standard.

This second edition cancels and replaces the first edition published in 2013. This edition constitutes a technical revision.

This edition includes the following a significant technical change with respect to the previous edition:

a) A simple method to calculate theoretical coil coefficient k is described in 6.2.1.

The text of this International Standard is based on the following documents:

FDIS	Report on voting
90/462/FDIS	90/464/RVD

Full information on the voting for the approval of this International Standard can be found in the report on voting indicated in the above table.

The language used for the development of this International Standard is English.

This document was drafted in accordance with ISO/IEC Directives, Part 2, and developed in accordance with ISO/IEC Directives, Part 1 and ISO/IEC Directives, IEC Supplement, available at www.iec.ch/members_experts/refdocs. The main document types developed by IEC are described in greater detail at www.iec.ch/standardsdev/publications.

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INTRODUCTION

Over thirty years after their discovery in 1986, high-temperature superconductors are now finding their way into products and technologies that will revolutionize information transmission, transportation, and energy. Among them, high-temperature superconducting (HTS) microwave filters, which exploit the extremely low surface resistance of superconductors, have already been commercialized. They have two major advantages over conventional non-superconducting filters, namely: low insertion loss (low noise characteristics) and high frequency selectivity (sharp cut) [1][1]. These advantages enable a reduced number of base stations, improved speech quality, more efficient use of frequency bandwidths, and reduced unnecessary radio wave noise.

Large-area superconducting thin films have been developed for use in microwave devices [2]. They are also ~~used~~ considered for use in emerging superconducting power devices, such as resistive-type superconducting fault-current limiters (SFCLs) [3] [4] [5], superconducting fault detectors used for superconductor-triggered fault current limiters [6] [7] and persistent-current switches used for persistent-current HTS magnets [8] [9]. The critical current density J_c is one of the key parameters that describe the quality of large-area HTS films. Nondestructive, AC inductive methods are widely used to measure J_c and its distribution for large-area HTS films [10] [11] [12] [13], among which the method utilizing third-harmonic voltages $U_3\cos(3\omega t + \theta)$ is the most popular [10] [11], where ω, t and θ denote the angular frequency, time, and initial phase, respectively. However, these conventional methods are not accurate because they have not considered the electric-field E criterion of the J_c measurement [14] [15] and sometimes use an inappropriate criterion to determine the threshold current I_{th} from which J_c is calculated [16]. A conventional method can obtain J_c values that differ from the accurate values by 10 % to 20 % [15]. It is thus ~~necessary~~ important to establish standard test methods to precisely measure the local critical current density and its distribution, to which all involved in the HTS filter industry can refer for quality control of the HTS films. Background knowledge on the inductive J_c measurements of HTS thin films is summarized in Annex A.

In these inductive methods, AC magnetic fields are generated with AC currents $I_0\cos\omega t$ in a small coil mounted just above the film, and J_c is calculated from the threshold coil current I_{th}, at which full penetration of the magnetic field to the film is achieved [17]. For the inductive method using third-harmonic voltages U_3, U_3 is measured as a function of I_0, and the I_{th} is determined as the coil current I_0 at which U_3 starts to emerge. The induced electric fields E in the superconducting film at $I_0 = I_{th}$, which are proportional to the frequency f of the AC current, can be estimated by a simple Bean model [14]. A standard method has been proposed to precisely measure J_c with an electric-field criterion by detecting U_3 and obtaining the n-value (index of the power-law E-J characteristics) by measuring I_{th} precisely at various frequencies [14] [15] [18] [19]. This method not only obtains precise J_c values, but also facilitates the detection of degraded parts in inhomogeneous specimens, because the decline of n-value is more ~~remarkable~~ noticeable than the decrease of J_c in such parts [15]. It is noted that this standard method is excellent for assessing homogeneity in large-area HTS films, although the relevant parameter for designing microwave devices is not J_c, but the surface resistance. For application of large-area superconducting thin films to SFCLs, knowledge on J_c distribution is vital, because J_c distribution significantly affects quench distribution in SFCLs during faults.

The International Electrotechnical Commission (IEC) draws attention to the fact that it is claimed that compliance with this document may involve the use of a patent ~~concerning the determination of the *E-J* characteristics by inductive J_c measurements as a function of frequency, given in the Introduction, Clause 1, Clause 4 and 5.1~~. IEC takes no position concerning the evidence, validity, and scope of this patent right.

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SUPERCONDUCTIVITY –

Part 17: Electronic characteristic measurements – Local critical current density and its distribution in large-area superconducting films

1 Scope

This part of IEC 61788 ~~describes~~ specifies the measurements of the local critical current density (J_c) and its distribution in large-area high-temperature superconducting (HTS) films by an inductive method using third-harmonic voltages. The most important consideration for precise measurements is to determine J_c at liquid nitrogen temperatures by an electric-field criterion and obtain current-voltage characteristics from its frequency dependence. Although it is possible to measure J_c in applied DC magnetic fields [20] [21], the scope of this document is limited to the measurement without DC magnetic fields.

This technique intrinsically measures the critical sheet current that is the product of J_c and the film thickness d. The range and measurement resolution for $J_c d$ of HTS films are as follows.

– $J_c d$: from 200 A/m to 32 kA/m (based on results, not limitation).

– Measurement resolution: 100 A/m (based on results, not limitation).

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2 Normative references

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~~IEC 60050 (all parts), *International Electrotechnical Vocabulary* (available at http://www.electropedia.org<http://www.electropedia.org>)~~

IEC 60050-815, *International Electrotechnical Vocabulary – Part 815: Superconductivity* (available at <http://www.electropedia.org>)

3 Terms and definitions

For the purposes of this document, the terms and definitions given in IEC 60050-815~~:2000~~ apply, some of which are repeated here for convenience.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- IEC Electropedia: available at http://www.electropedia.org/
- ISO Online browsing platform: available at http://www.iso.org/obp

3.1
critical current
I_c
maximum direct current that can be regarded as flowing without resistance practically

Note 1 to entry: I_c is a function of magnetic field strength, temperature and strain.

[SOURCE: IEC 60050-815:~~2000~~2015, 815-~~03~~12-01]

3.2
critical current criterion
I_c criterion
criterion to determine the critical current, I_c, based on the electric field strength, E, or the resistivity, ρ

Note 1 to entry: E = 10 µV/m or E = 100 µV/m is often used as electric field criterion, and $\rho = 10^{-14}$ Ω · m or $\rho = 10^{-13}$ Ω · m is often used as resistivity criterion. ~~("*E* = 10 V/m or *E* = 100 V/m" in the current edition is mistaken and is scheduled to be corrected in the second edition).~~

[SOURCE: IEC 60050-815:~~2000~~2015, 815-~~03~~12-02]

3.3
critical current density
J_c
electric current density at the critical current using either the cross-section of the whole conductor (overall) or of the non-stabilizer part of the conductor if there is a stabilizer

Note 1 to entry: The overall current density is called engineering current density (symbol: J_e).

[SOURCE: IEC 60050-815:~~2000~~2015, 815-~~03~~12-03]

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3.4
transport critical current density
J_{ct}
critical current density obtained by a resistivity or a voltage measurement

[SOURCE: IEC 60050-815:~~2000~~2015, 815-~~03~~12-04]

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3.5
***n*-value**
<superconductor> exponent obtained in a specific range of electric field strength or resistivity when the voltage/current U (I) curve is approximated by the equation $U \propto I^n$

[SOURCE: IEC 60050-815:~~2000~~2015, 815-~~03~~12-10]

4 Requirements

The critical current density J_c is one of the most fundamental parameters that describe the quality of large-area HTS films. In this document, J_c and its distribution are measured non-destructively via an inductive method by detecting third-harmonic voltages $U_3\cos(3\omega t + \theta)$. A small coil, which is used both to generate AC magnetic fields and detect third-harmonic voltages, is mounted just above the HTS film and used to scan the measuring area. To measure J_c precisely with an electric-field criterion, the threshold coil currents I_{th}, at which U_3 starts to emerge, are measured repeatedly at different frequencies and the E-J characteristics are determined from their frequency dependencies.

The target relative combined standard uncertainty in the method used to determine the absolute value of J_c is less than 10 %. However, the target uncertainty is less than 5 % for the purpose of evaluating the homogeneity of J_c distribution in large-area superconducting thin films.

5 Apparatus

5.1 Measurement equipment

Figure 1 shows a schematic diagram of a typical electric circuit used for the third-harmonic voltage measurements. This circuit is comprised of a signal generator, power amplifier, digital multimeter (DMM) to measure the coil current, band-ejection filter to reduce the fundamental wave signals and lock-in amplifier to measure the third-harmonic signals. It involves the single-coil approach in which the coil is used to generate an AC magnetic field and detect the inductive voltage. This method can also be applied to double-sided superconducting thin films ~~without hindrance~~ with no obstacles. In the methods proposed here, however, there is an additional system to reduce harmonic noise voltages generated from the signal generator and the power amplifier [14]. In an example of Figure 1, a cancel coil of specification being the same as the sample coil is used for cancelling. The sample coil is mounted just above the superconducting film, and a superconducting film with a $J_c d$ sufficiently larger than that of the sample film is placed below the cancel coil to adjust its inductance to that of the sample coil. Note that the inductance of the sample coil decreases by 20 % to 30 % due to the superconducting shielding current when it is mounted on a superconducting film. Both coils and superconducting films are immersed in liquid nitrogen (a broken line in Figure 1). Other optional measurement systems are described in Annex B.

NOTE In this circuit, coil currents of about 0,1 A (RMS) and power source voltages of > 6 V (RMS) are needed to measure the superconducting film of $J_c d \approx 10$ kA/m while using coil 1 or 2 of Table 2. A precision power amplifier~~, such as NF: HSA4011,~~ with sufficiently high power is ~~necessary~~ used to supply such large currents and voltages.

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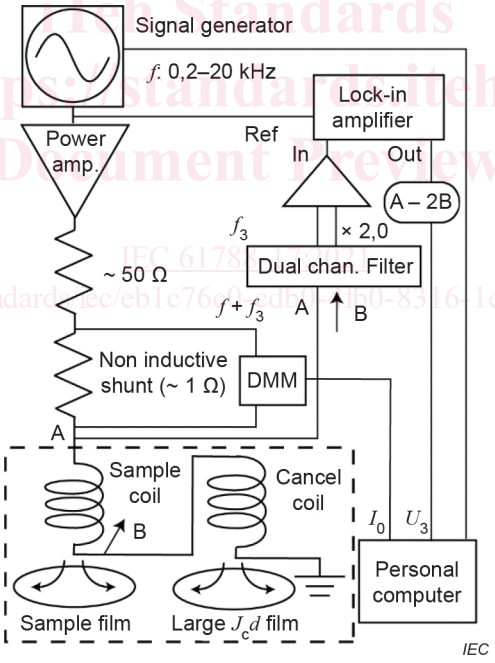

NOTE The broken line surrounds elements immersed in liquid nitrogen.

Figure 1 – Diagram for an electric circuit used for inductive J_c measurement of HTS films

5.2 Components for inductive measurements

5.2.1 Coils

Currently available large-area HTS films are deposited on areas as large as about 25 cm in diameter, while films about 5 cm in diameter are commercially used to prepare microwave filters [22]. Larger $YBa_2Cu_3O_7$ (YBCO) films, about 10 cm in diameter and 2,7 cm × 20 cm, were used to fabricate fault current limiter modules [3] [4] [5]. For the J_c measurements of such films, the appropriate outer diameter of the sample coils ranges from 2 mm to 5 mm. The requirement for the sample coil is to generate as high a magnetic field as possible at the upper surface of the superconducting film, for which flat coil geometry is suitable. Typical specifications are as follows.

a) Inner winding diameter D_1: 0,9 mm, outer diameter D_2: 4,2 mm, height h: 1,0 mm, 400 turns of a 50 µm diameter copper wire.

b) D_1: 0,8 mm, D_2: 2,2 mm, h: 1,0 mm, 200 turns of a 50 µm diameter copper wire.

5.2.2 Spacer film

Typically, a polyimide film with a thickness of 50 µm to 125 µm is used to protect the HTS films. The coil has generally some protection layer below the coil winding, which also insulates the thin film from Joule heat in the coil. The typical thickness is 100 µm to 150 µm, and the coil-to-film distance Z_1 is kept to be 200 µm.

5.2.3 Mechanism for the set-up of the coil

To maintain a prescribed value for the spacing Z_1 between the bottom of the coil winding and the film surface, the sample coil should be pressed to the film with sufficient pressure, typically exceeding about 0,2 MPa [18]. Techniques to achieve this are to use a weight or spring, as shown in Figure 2. The system schematically shown in the figure left is used to scan a wide area of the film. Before the U_3 measurement the coil is initially ~~moved~~ raised up to some distance, moved laterally to the target position, and then ~~moved~~ lowered down and pressed to the film. An appropriate pressure should be determined so that too high pressure does not damage the bobbin, coil, HTS thin film or the substrate. It is reported that the YBCO deposited on biaxially-textured pure Ni substrate was degraded by transverse compressive stress of about 20 MPa [23].

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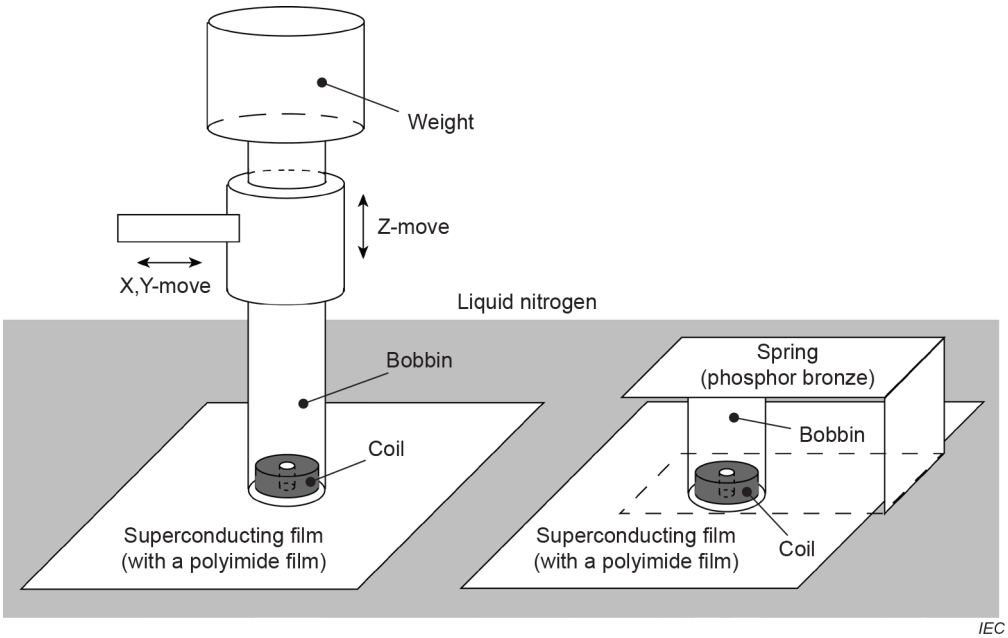

Figure 2 – Illustration showing techniques to press the sample coil to HTS films