

SLOVENSKI STANDARD SIST ISO 4409:1998

01-december-1998

:`i]XbUhN\b]_U'!`<]XfUj`]_U'!`fdU_Yžachcf^]']b`ghfb^Yb]`\]XfcghUh]b]`dfYbcgb]_]'! I[chUj`^Ub^Y``Ughbcgh]`df]`ghUb]\`cVfUhcjUb]\`dc[c1]\

Hydraulic fluid power -- Positive displacement pumps, motors and integral transmissions -- Determination of steady-state performance

iTeh STANDARD PREVIEW

Transmissions hydrauliques -- Pompes, moteurs et variateurs volumétriques --Détermination du fonctionnement en régime permanent

SIST ISO 4409:1998 Ta slovenski standard je istoveten 2:31427/Stelso 4409:1986

<u>ICS:</u>

23.100.10 Pã妿ç¦ã } ^Á¦] æ{\^Á§ Á{ [d[¦bã Pumps and motors

SIST ISO 4409:1998

en



iTeh STANDARD PREVIEW (standards.iteh.ai)

SIST ISO 4409:1998 https://standards.iteh.ai/catalog/standards/sist/e3baa6d0-0984-4002-bcec-657b93831427/sist-iso-4409-1998 SIST ISO 4409:1998

International Standard



INTERNATIONAL ORGANIZATION FOR STANDARDIZATION MEX CHAROCHAR OPPAHUSALUN TO CTAHDAPTUSALUNOCRGANISATION INTERNATIONALE DE NORMALISATION

Hydraulic fluid power — Positive displacement pumps, motors and integral transmissions — Determination of steady-state performance

Transmissions hydrauliques – Pompes, moteurs et variateurs volumétriques – Détermination du fonctionnement en régime permanent

(standards.iteh.ai)

First edition - 1986-10-01

SIST ISO 4409:1998 https://standards.iteh.ai/catalog/standards/sist/e3baa6d0-0984-4002-bcec-657b93831427/sist-iso-4409-1998

UDC 621.8.032 : 621.65.001.4

Ref. No. ISO 4409-1986 (E)

Descriptors : hydraulic fluid power, hydraulic equipment, hydraulic transmission, pumps, positive displacement pumps, hydraulic motors, tests, performance tests.

SIST ISO 4409:1998

Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work.

Draft International Standards adopted by the technical committees are circulated to the member bodies for approval before their acceptance as International Standards by the ISO Council. They are approved in accordance with ISO procedures requiring at least 75 % approval by the member bodies voting.

International Standard ISO 4409 was prepared by Technical Committee ISO/TC 131, Fluid power systems. (standards.iteh.ai)

Users should note that all International Standards undergo revision from time to time and that any reference made herein to any other International Standard implies its latest edition, unless otherwise stated. International Standard Stan

© International Organization for Standardization, 1986 •

Printed in Switzerland

Contents

| | Page |
|--|------|
| 0 Introduction | 1 |
| 1 Scope and field of application | 1 |
| 2 References | 1 |
| 3 Definitions | 1 |
| iTeh STAmbols and units. PREVIEW | 3 |
| (standards.iteh.ai) | |
| 6 Test procedures | 4 |
| SIST ISO 4409:1998 Identification statement https://standards.iteh.ai/catalog/standards/sist/e3/baa6d0-0984-4002-bcec- | 7 |
| 657b93831427/sist-iso-4409-1998 | |
| A Use of practical units | 13 |
| B Errors and classes of measurement accuracy | . 14 |
| C Pre-test checklist | . 15 |

iii

SIST ISO 4409:1998

iTeh STANDARD PREVIEW (standards.iteh.ai) This page intentionally left blank

SIST ISO 4409:1998 https://standards.iteh.ai/catalog/standards/sist/e3baa6d0-0984-4002-bcec-657b93831427/sist-iso-4409-1998

Hydraulic fluid power — Positive displacement pumps, motors and integral transmissions — Determination of steady-state performance

0 Introduction

In hydraulic fluid power systems, power is transmitted and controlled through a liquid under pressure within an enclosed circuit. Pumps are components which convert rotary mechanical power into hydraulic fluid power. Motors are components which convert hydraulic fluid power into rotary mechanical power. Integral transmissions (hydraulic drive units) are a combination of one or more hydraulic pumps and motors and appropriate controls forming a component.

With very few exceptions, all hydraulic fluid power pumps and motors are of the positive displacement type, i.e. they have internal sealing means which make them capable of maintain ing a relatively constant ratio between rotational speed and fluid flow over wide pressure ranges. They generally use gears,

vanes or pistons. Non-positive displacement components, such 4409:1998 as centrifugal or turbine types, are seldom associated with rds/sistSOba.5598,09 Fluid 00 power - systems and components -hydraulic fluid power systems. 657b93831427/sist-iso-Vocabulary.

Pumps and motors are available either as "fixed" or "variable" displacement types. Fixed displacement units have preselected internal geometries which maintain a relatively constant volume of liquid passing through the component per revolution of the component's shaft. Variable displacement components have means for changing the internal geometries so that the volume of liquid passing through the component per revolution of the component's shaft can be changed.

This International Standard is intended to unify testing methods for hydraulic fluid power positive displacement hydraulic pumps, motors and integral transmissions to enable the performance of different components to be compared.

1 Scope and field of application

This International Standard specifies methods for determining the performance and efficiency of hydraulic fluid power positive displacement pumps, motors and integral transmissions. It applies to components having continuously rotating shafts.

This International Standard describes requirements for test installations, test procedures (under steady-state conditions) and the presentation of test results.

Annex A gives guidance as to the use of practical units for the expression of results.

Annex B contains information on errors and classes of measurement accuracy. The measurement accuracy is divided into three classes: A, B and C.

Annex C provides a pre-test checklist of those items on which agreement is recommended between the parties concerned.

2 References

symbols. ISO 4391, Hydraulic fluid power — Pumps, motors and integral

transmissions – Parameter definitions and letter symbols.

ISO 1219, Fluid power systems and components - Graphic

//sist-iso-4909409607. IEC Publication 34-2, Rotating electrical machines — Part 2: Methods for determining losses and efficiency of rotating elec-

Methods for determining losses and efficiency of rotating electrical machinery from tests (excluding machines for traction vehicles).

IEC Publication 51, Recommendation for direct acting indicating electrical measuring instruments and their accessories.

3 Definitions

The definitions of quantities and units, and the letters used as symbols are given in ISO 31 and ISO 4391.

For the purposes of this International Standard the following definitions of concepts together with their respective symbols (except for concepts in general use defined in ISO 5598) are applicable.

NOTE — When there is no risk of ambiguity (i.e. when a test has been carried out on a pump or a motor), the superscripts "P", "M" and "T" specifying that the quantity concerns, respectively, a pump, a motor or an integral transmission, can be omitted.

3.1 Volume flow rate

3.1.1 volume flow rate, q_V : The measured flow volume per unit of time.

3.1.2 drainage flow rate, q_{V_d} : The volume rate of flow from the casing of a component.

3.1.3 effective outlet flow rate of a pump, $q_{V_{2,e}}^{\rm P}$: The actual flow rate measured at the pump outlet at the temperature $\theta_{2,e}$ and pressure $p_{2,e}$ at the outlet of the pump. If the flow rate is measured downstream of the pump at temperature θ and pressure p, that flow rate is corrected to give the effective outlet value as follows:

$$q_{V_{2,e}}^{\mathsf{P}} = q_{V} \left[1 - \left(\frac{p_{2,e} - p}{\overline{K}_{\tau}} \right) + \alpha \left(\theta_{2,e} - \theta \right) \right]$$

3.1.4 effective inlet flow rate on a motor, $q_{V_1}^{M}$: The actual flow rate measured at the motor inlet at the temperature $\theta_{1,e}$ and pressure $p_{1,e}$ at the inlet to the motor. If the flow rate is measured downstream of the motor outlet at temperature θ and pressure p, that flow rate is corrected to give the effective inlet value as follows:

$$q_{V_{1,e}}^{\mathsf{M}} = q_{V} \left[1 - \left(\frac{p_{1,e} - p}{\overline{K}_{\tau}} \right) + \alpha \left(\theta_{1,e} - \theta \right) \right]$$

If the motor has an external drainage, the drainage flow rate $q_{V_d}^{M}$ shall be corrected to refer to the inlet condition used for A The total inlet hydraulic power of a motor. computing $q_{V_{1,e}}^{M}$ as follows:

$$q_{V_{1,e}}^{\mathsf{M}} = q_{V} \left[1 - \left(\frac{p_{1,e} - p}{\bar{K}_{\tau}} \right) + \alpha \left(\theta_{1,e} - \theta \right) \right] + q_{V_{\mathsf{d}}} \left[1 - \left(\frac{p_{1,e} - p}{\bar{K}_{\tau}} \right) + \alpha \left(\theta_{1,e} - \theta \right) \right] + q_{V_{\mathsf{d}}} \left[1 - \left(\frac{p_{1,e} - p}{\bar{K}_{\tau}} \right) + \alpha \left(\theta_{1,e} - \theta \right) \right] + q_{V_{\mathsf{d}}} \left[1 - \left(\frac{p_{1,e} - p}{\bar{K}_{\tau}} \right) + \alpha \left(\theta_{1,e} - \theta \right) \right] + q_{V_{\mathsf{d}}} \left[1 - \left(\frac{p_{1,e} - p}{\bar{K}_{\tau}} \right) + \alpha \left(\theta_{1,e} - \theta \right) \right] + q_{V_{\mathsf{d}}} \left[1 - \left(\frac{p_{1,e} - p}{\bar{K}_{\tau}} \right) + \alpha \left(\theta_{1,e} - \theta \right) \right] + q_{V_{\mathsf{d}}} \left[1 - \left(\frac{p_{1,e} - p}{\bar{K}_{\tau}} \right) + \alpha \left(\theta_{1,e} - \theta \right) \right] \right] + q_{V_{\mathsf{d}}} \left[1 - \left(\frac{p_{1,e} - p}{\bar{K}_{\tau}} \right) + \alpha \left(\theta_{1,e} - \theta \right) \right] + q_{V_{\mathsf{d}}} \left[1 - \left(\frac{p_{1,e} - p}{\bar{K}_{\tau}} \right) + \alpha \left(\theta_{1,e} - \theta \right) \right] \right] \right]$$

3.2 rotational frequency (shaft speed), n: The number of revolutions of the drive shaft per unit of time. The direction of rotation (clockwise or counter-clockwise) is specified from the point of view of the observer looking at the end of the shaft. It may also be defined by diagram, if necessary.

3.3 torque, T: The measured value of the torque in the shaft of the test component.

3.4 Pressure

3.4.1 effective pressure, p_e: The fluid pressure, relative to atmospheric pressure, having a value which is

positive, if this pressure is greater than the atmospheric pressure; or

negative, if this pressure is less than the atmospheric pressure.

3.4.2 drainage pressure, pd: The pressure, relative to atmospheric pressure, measured at the outlet of a drainage connection on a component casing.

3.5 Power

3.5.1 mechanical power, Pm: The product of the torque and rotational frequency measured at the shaft of a pump or motor

$$P_{\rm m} = 2\pi nT$$

3.5.2 hydraulic power, P_h: The product of the flow rate and pressure at any point.

$$P_{\rm h} = q_V \cdot p$$

3.5.3 effective outlet hydraulic power of a pump, P_{2h}^{P} : The total outlet hydraulic power of a pump.

$$P_{2,h}^{P} = q_{V_{2,e}} \cdot p_{2,e}$$

3.5.4 effective inlet hydraulic power of a motor, $P_{1,h}^{\mathsf{M}}$:

rds. Mtegy, ap, e and

NOTE - The total energy of a hydraulic fluid is the sum of the various Ochergies contained in the fluid. In 3.5.3 and 3.5.4, the kinetic, positional and strain energies of the fluid are ignored and the power is calculated using the static pressure only. Should these other energies have a significant effect on the test results, due account should be taken of them.

3.6 Efficiency

3.6.1 pump overall efficiency, η_t^P : The ratio of the power transferred to the liquid, at its passage through the pump, to the mechanical input power.

$$\eta_{t}^{P} = \frac{(q_{V_{2,e}} \cdot p_{2,e}) - (q_{V_{1,e}} \cdot p_{1,e})}{2\pi nT}$$

3.6.2 motor overall efficiency, η_t^M : The ratio of the mechanical output power to the power transferred from the liquid at its passage through the motor.

$$\eta_{t}^{M} = \frac{2\pi nT}{(q_{V_{1,e}} \cdot p_{1,e}) - (q_{V_{2,e}} \cdot p_{2,e})}$$

3.6.3 integral transmission overall efficiency, η_t^{T} : The ratio of the output mechanical power to the input mechanical power.

$$\eta_{t}^{\mathsf{T}} = \frac{n_2 \cdot T_2}{n_1 \cdot T_1}$$

4 Symbols and units

4.1 The symbols and units used throughout this International Standard are as shown in table 1.

4.2 The letters and figures used as subscripts to the symbols listed in table 1 are as specified in ISO 4391.

4.3 The graphical symbols used in figures 1, 2 and 3 are in accordance with ISO 1219.

5 Test installations

5.1 Pump test circuits ¹⁾

5.1.1 An open test circuit suitable for testing pumps as shown in figure 1 shall be used.

5.1.1.1 Where a pressurized inlet condition is required, a suitable means shall be provided to maintain the inlet pressure within the specified limits (see 6.2.1).

5.1.2 A closed test circuit, alternative to figure 1, is shown in figure 2. In this circuit the boost pump provides a flow slightly in excess of the total circuit losses; a greater flow may be provided for cooling purposes.

5.2 Motor test circuit¹⁾

A test circuit suitable for testing motors using a controlled fluid supply as shown in figure 3 shall be used.

5.3 General requirements

5.3.1 The installation shall be designed to prevent air entrainment and precautions shall be taken to remove all free air from the system before testing.

| Reference clause | eh STQuantity ARI | Symbol | Dimensions ¹⁾ | Unit ²⁾ |
|---------------------|--|-----------------------------|---|--------------------|
| 3.1 | Volume flow-rate ² ards. | teh ^g ai) | L3 T - 1 | m³/s |
| 3.2 | Rotational frequency | n | T1 | s ⁻¹ |
| 3.3 https://st | <u>SIST ISO 4409:</u> Andards.iteh.ai/catalog/standards/sis | <u>1998</u> t/e3baa6d0-0 | ML ² T - 2 984-4002-bcec- | N·m |
| 3.4 | Pressure657b93831427/sist-iso- | | ML-1 T-2 | Pa ³⁾ |
| 3.5 | Power | Р | ML ² T - 3 | w |
| | Mass density | Q | ML-3 | kg/m ³ |
| | Isothermal bulk modulus secant | \overline{K}_{τ} | ML-1 T-2 | Pa |
| | Kinematic viscosity | ν | L ² T ⁻¹ | m²/s |
| | Temperature | θ | Θ | к |
| | Coefficient of cubic thermal expansion | α | ⊙ −1 | K-1 |
| 3.6 | Efficiency | η | Pure number | |

Table 1 - Symbols and units

1) $M = mass; L = length; T = time; \Theta = temperature$

2) The use of practical units for the presentation of results is described in annex A.

3) $1 Pa = 1 N/m^2$

¹⁾ Figures 1, 2 and 3 illustrate basic circuits which do not incorporate all the safety devices necessary to protect against damage in the event of any component failure. It is important that those responsible for carrying out the test give due consideration to safeguarding both personnel and equipment.

5.3.2 The component shall be installed and operated in the test circuit in accordance with the manufacturer's operating instructions.

5.3.3 Tests shall normally be carried out in still air; the ambient temperature and any variation from still air conditions shall be recorded.

5.4 Filtration

5.4.1 A filter shall be installed which provides a standard of filtration approved by the pump or motor manufacturer.

5.4.2 The position, number and specific description of each filter used in the test circuit shall be stated.

5.5 Positioning of tapping points

5.5.1 Where pressure measurements are made within a pipe, the pressure-tapping point shall be positioned not less than twice and not more than four times the pipe diameter from the component port face.

NOTE - Greater distances may be used provided consideration is given to the effect of pipe losses.

The following temperature measurements shall be recorded:

- b)

C) the drainage fluid temperature (if applicable); d) the ambient temperature.

stan 5.5.2 Where temperature measurements are made within a measure some of the above. Note this on the test report. pipe, the temperature-tapping point shall be positioned best ISO 4409:1998

tween two and four times the pipe diameter from the pressuretapping point further away from the component. 657b93831427/sist-iso-4409-199

Test procedures 6

General tests 61

6.1.1 Pre-test condition

Before the tests are carried out, the component shall be "run in" in accordance with the manufacturer's recommendations.

6.1.2 Test fluids

6.1.2.1 Since the performance of a component may vary considerably with the viscosity on the fluid, a stated fluid approved by the manufacturer of the component when carrying out the tests shall be used. Information concerning the fluid shall be recorded.

6.1.2.2 The kinematic viscosity, v, and the mass density of the fluid, ρ , at the controlled temperature used during the test shall be stated.

6.1.2.3 The values used for the isothermal secant bulk modulus, $\overline{K}_{\tau r}$ and for the coefficient of cubic thermal expansion, α , shall be stated.

6.1.3 Temperatures

6.1.3.1 Controlled temperature

The tests shall be carried out at a stated fluid temperature measured at the inlet to a pump or motor within the range recommended by the component manufacturer, the indicated temperature being maintained within the limits stated in table 2.

Table 2 — Permissible variation in indicated fluid temperature

| Class of measurement accuracy (see annex B) | A | В | с |
|---|------|------|------|
| Variation of temperature indication, K | ±1,0 | ±2,0 | ±4,0 |

6.1.3.2 Other temperatures

- a) the temperature at the outlet of a pump or motor;
- the temperature at the point of measurement of flow;

NOTE For an integral transmission, it may not be possible to ar

> The absolute ambient atmospheric pressure during the test shall be recorded, if it is significant to the test.

6.1.5 Casing pressure

If the fluid pressure within the casing of a component may affect its performance, its value shall be recorded during the tests.

6.1.6 Steady-state conditions

6.1.6.1 When steady-state test conditions are reached for a specific test condition, only one set of readings of individual quantities shall be taken over concurrent common time periods. Each reading shall be recorded as the mean value of each quantity being measured.

6.1.6.2 Each set of readings taken for a controlled value of a selected parameter shall be recorded only where the indicated value of the controlled parameter is within the limits shown in table 3.

6.1.7 Test measurements

The number of sets of readings to be taken and their disposition over the range shall be selected in order to give a representative indication of the performance of the component over the full range of the quantity being varied.

Table 3 – Limits of permissible variation of mean indicated values of selected parameters¹⁾

| Parameter | Permissible variation for classes of measurement accuracy (see annex B) | | | |
|---|--|----------------------|----------------------|--|
| | Α | В | С | |
| Rotational frequency, % | ±0,5 | ±1,0 | ±2,0 | |
| Torque, % | ±0,5 | ±1,0 | ±2,0 | |
| Volume flow rate, % | ±0,5 | ±1,5 | ±2,5 | |
| Pressures, where $p < 2 \times 10^5$ Pa gauge, Pa ²⁾ | ± 1 × 10 ³ | ±3 × 10 ³ | ±5 × 10 ³ | |
| Pressures, where $p > 2 \times 10^5$ Pa gauge, % | ±0,5 | ±1,5 | ±2,5 | |

1) The permissible variations listed in this table concern deviation of the indicated instrument reading and do not refer to limits of error of the instrument reading (see annex B).

These variations are used as an indicator of steady state, and are also used where graphical results are presented for a parameter of fixed value. The actual indicated value should be used in any subsequent calculation of power or efficiency.

2) $1 Pa = 1 N/m^2$

6.2.4 Reverse flow

If the direction of flow for the pump can be reversed by means of a capacity control, carry out tests for both directions of flow, if required.

6.2.5 Non-integral boost pumps

If the test pump is associated with a boost and the power inputs can be measured separately, the pumps shall be tested independently and the results presented independently for each pump.

6.2.6 Full-flow integral boost pump

6.2.6.1 If the boost pump is integral with the main pump, which results in the power inputs being inseparable, and the boost pump delivers the full flow of the main pump, the two pumps shall be treated as one integral unit and the results presented accordingly.

NOTE - The inlet pressure measured is the inlet pressure to the boost pump.

6.2.6.2 Any excess flow from the boost pump shall be iTeh STANDARD measured and recorded.

6.2 Pump tests

(standards.iteh.ai) 6.2.7 Secondary-flow integral boost pump

SIST ISO 4409:1 fothe boost pump is integral with the main pump, which results 6.2.1 Inlet pressure https://standards.iteh.ai/catalog/standards/sisite the power imputs being inseparable, but the boost pump sup-

(see table 3) at a stated value within the permissible range of inlet pressures specified by the manufacturer.

6.2.1.2 Carry out the tests at different inlet pressures, if required.

6.2.2 Test measurements

6.2.2.1 Take measurements of input torque, outlet flow rate, drainage flow rate (where applicable) and fluid temperatures, at a constant rotational frequency (see table 3) and at a number of outlet pressures so as to give a representative indication of the performance of the pump over the full range of outlet pressures.

6.2.2.2 Repeat these measurements at other rotational frequencies, as required, to give a representative indication of the performance of the pump over the full range of rotational frequencies.

6.2.3 Variable capacity

If the pump is of the variable capacity type, carry out complete tests for maximum capacity setting and such other settings, as required, e.g. 75, 50 and 25 %.

Each of these settings shall give the required percentage of the flow rate at the minimum outlet pressure at the minimum rotational frequency specified for the test.

6.2.1.1 During each test, maintain the inlet pressure constant st-iso-plies only a secondary flow to the hydraulic circuit of the main pump and the remainder is by-passed or used for some auxiliary service, such as cooling circulation, then, where practicable, the flows from the boost pump shall be measured and recorded.

6.2.8 Direct coupled pump (Class C only)

6.2.8.1 If a pump is directly coupled to an electric motor having a single rotational frequency the characteristic of which varies with load, it is permissible to derive the input mechanical power from the electrical power input. This is applicable when the rotational frequency variation between "no load" and "full load" is not more than 5 %. The measured flow at measured rotational frequency is corrected to give the calculated flow at "no-load" rotational frequency.

For this purpose, it shall be assumed that the flow/rotational frequency characteristic of the pump is linear and that the torque constant is within the range of correction at any one output pressure.

6.2.8.2 If the electrical power input to an electric motor coupled directly to the pump is used as a means of determining the pump power input, the following conditions shall be complied with:

the motor shall only be operated at conditions where the efficiency is known with sufficient accuracy;

b) the motor efficiency shall be determined in accordance with the recommendations of IEC Publication 34-2.