



Standard Test Methods for Impact Resistance of Rigid Poly(Vinyl Chloride) (PVC) Building Products¹

This standard is issued under the fixed designation D4226; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ϵ) indicates an editorial change since the last revision or reapproval.

1. Scope*

1.1 These test methods cover the determination of the energy required to crack or break rigid poly(vinyl chloride) (PVC) plastic sheeting and profile flat sections used in building products, as well as extruded or molded test samples, under specified conditions of impact from a freefalling standard weight striking an impactor with either of two configurations in contact with the specimen.

1.2 Two test procedures are included:

1.2.1 *Procedure A*, used to determine minimum impact energy required to cause failure (hole, crack, split, shatter, or tear).

1.2.2 *Procedure B*, used to determine minimum impact energy required to cause brittle failure.

1.3 The values stated in inch-pound units are to be regarded as standard. The values given in parentheses are mathematical conversions to SI units that are provided for information only and are not considered standard.

NOTE 1—There is no known ISO equivalent to this standard.

1.4 The text of this standard references notes and footnotes which provide explanatory material. These notes and footnotes (excluding, those in tables in figures) shall not be considered as requirements of this standard.

1.5 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety, health, and environmental practices and determine the applicability of regulatory limitations prior to use.* Specific precautionary statements are given in Section 8.

1.6 *This international standard was developed in accordance with internationally recognized principles on standardization established in the Decision on Principles for the Development of International Standards, Guides and Recommendations issued by the World Trade Organization Technical Barriers to Trade (TBT) Committee.*

¹ These test methods are under the jurisdiction of ASTM Committee D20 on Plastics and are the direct responsibility of Subcommittee D20.24 on Plastic Building Products.

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2. Referenced Documents

2.1 *ASTM Standards*:²

D618 Practice for Conditioning Plastics for Testing

D883 Terminology Relating to Plastics

D5947 Test Methods for Physical Dimensions of Solid Plastics Specimens

E178 Practice for Dealing With Outlying Observations

E456 Terminology Relating to Quality and Statistics

E691 Practice for Conducting an Interlaboratory Study to Determine the Precision of a Test Method

E2935 Practice for Conducting Equivalence Testing in Laboratory Applications

3. Terminology

3.1 *Definitions*—Definitions are in accordance with Terminology D883, unless otherwise specified. For terms relating to precision and bias and associated issues, the terms used in this standard are defined in accordance with E456.

3.2 *Definitions of Terms Specific to This Standard*:

3.2.1 *failure (of test specimen, as related to impact resistance)*—signified by the presence of a punched hole, crack, split, shatter, or tear that was created in the target area by the impact of the falling weight (see Fig. 1).

3.2.2 *ductile failure (ductile break, as related to impact resistance)*—a tear or split having an angle greater than 0° at the tip and extending through the entire thickness of the specimen such that light is directly visible through the tear or split (see Fig. 1).

3.2.3 *brittle failure (brittle break, as related to impact resistance)*—a punched hole, split, or shatter where a piece of the specimen separates from the main part of the specimen or a crack that has a 0° angle at the tip as viewed by the naked eye (see Fig. 1).

3.2.4 *mean failure height (Procedure A)*—the height from which the falling weight will cause 50 % of the specimens to fail.

² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

*A Summary of Changes section appears at the end of this standard

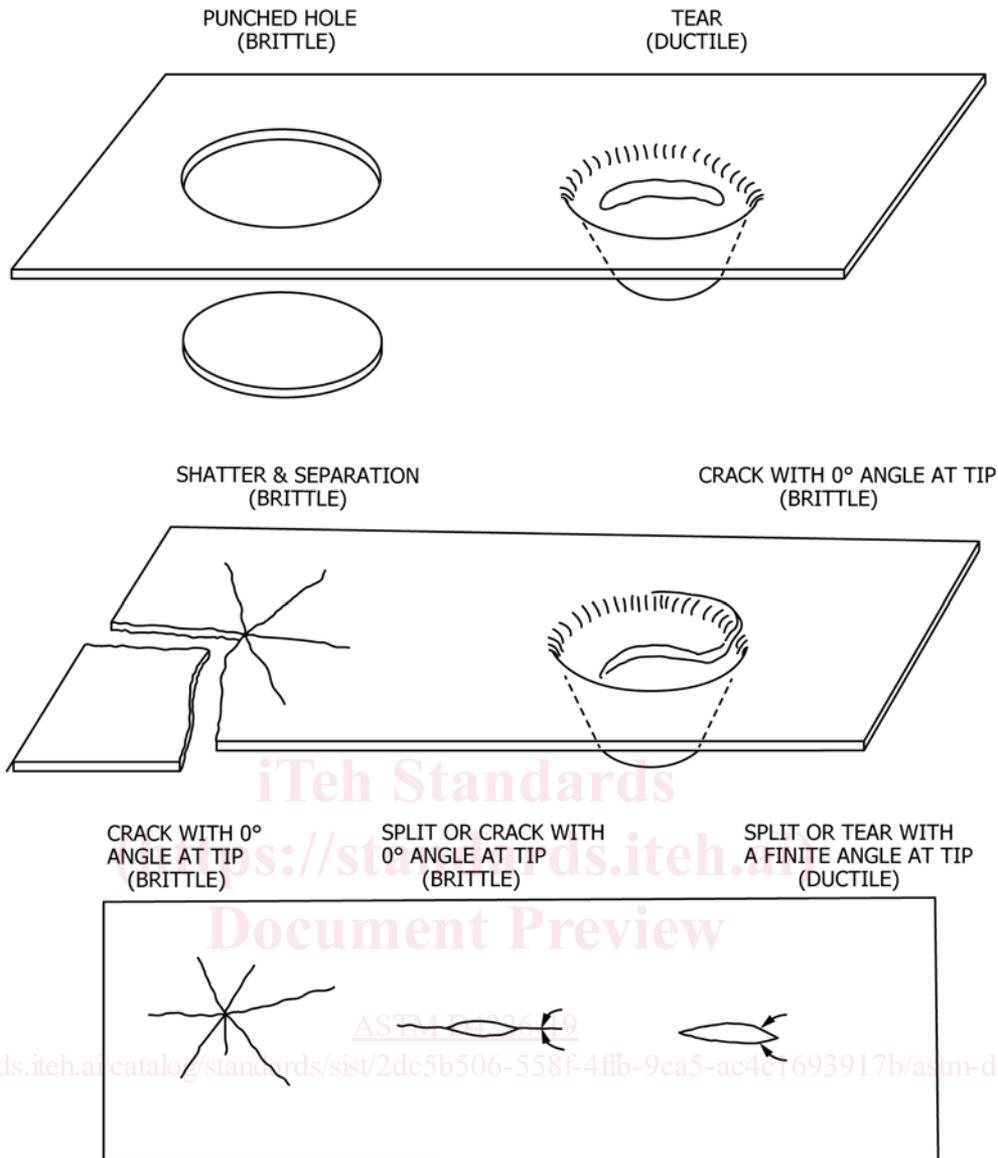


FIG. 1 Types of Failures of the Specimen

3.2.5 *mean failure energy (mean impact resistance)*, (Procedure A)—energy required to produce 50 % failures; the product of the weight and mean failure height.

3.2.6 *normalized mean failure energy (normalized mean impact resistance)*—the mean failure energy per unit (average) specimen thickness (Procedure A).

3.2.7 *mean brittle failure height*—the height from which the falling weight will cause 50 % brittle failures in specimens (Procedure B).

3.2.8 *mean brittle failure energy (mean energy of ductile-to-brittle transition)*, (Procedure B)—energy required to produce 50 % brittle failures; the product of the weight and mean brittle failure height.

3.2.9 *normalized mean brittle failure energy (normalized mean energy of ductile-to-brittle transition)*, (Procedure B)—the mean brittle failure energy per unit (average) specimen thickness.

3.2.10 *outlier*—an observation that appears to deviate markedly from other members of the sample in which it occurs.

4. Summary of Test Method

4.1 Flat sections of a PVC building profile are tested by means of an impactor driven by a falling weight to determine impact resistance of the profile. If necessary, cut the profile into smaller sections or coupons in order to properly position the profile on the tester support plate.

4.2 Procedure A establishes the height from which a standard falling 8-lb (3.6-kg) weight will cause 50 % of the specimens to fail.

4.3 Procedure B establishes the height from which a standard falling 8-lb (3.6-kg) weight will cause 50 % of the specimens to fail in a brittle mode.

4.4 Both procedures employ either of two configurations of impactor heads resting on the specimen. The specimen lays flat

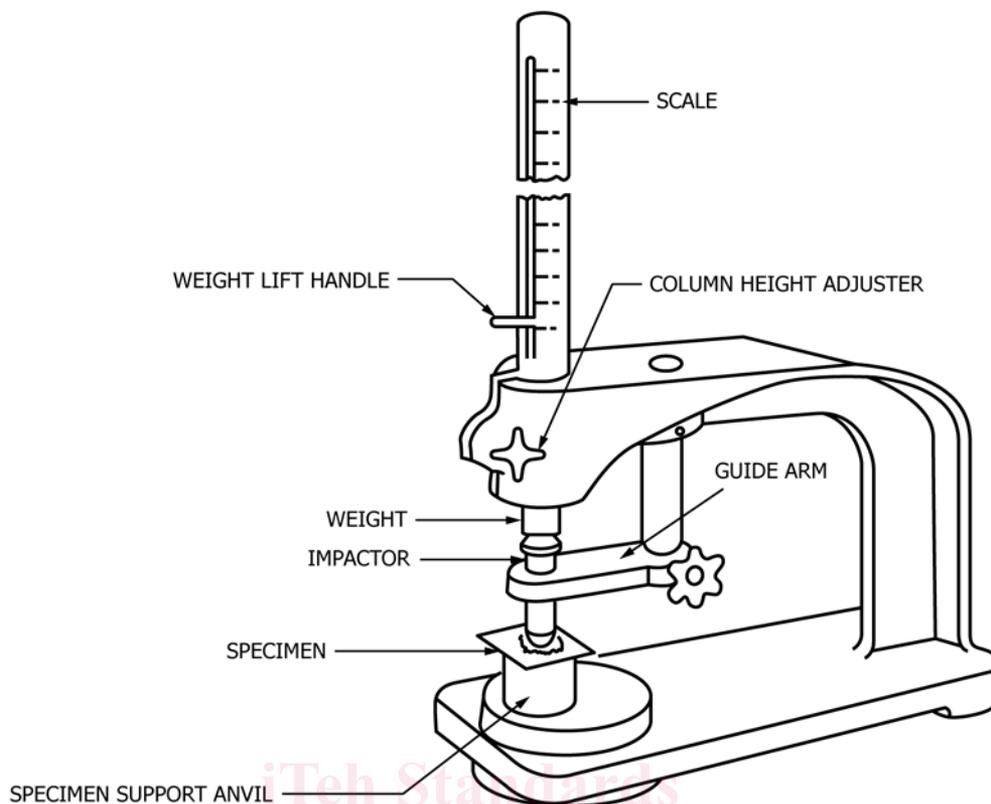


FIG. 2 Impact Tester

on a stand that has a 0.64-in. (16.3-mm) hole. The falling weight impacts on the impactor head tending to drive it through the specimen into the hole of the stand.

4.5 The technique used to find 50 % failure level in both procedures is commonly called the Bruceton Staircase Method or Up-and-Down Method. Testing is concentrated near the mean, reducing the number of specimens required to obtain a reasonably precise estimate.

5. Significance and Use

5.1 The impact strength values obtained on the flat sections of a building product profile are relevant only to the flat section that has been tested and these values do not necessarily indicate the impact resistance of the whole product, which is affected by the configuration of the profile (that is, corners, ribs, etc).

5.2 Constant weight and variable height, employed in these test methods, allow the velocity of impact to vary and, therefore, by Procedure B, can determine the energy of ductile-to-brittle transition, which cannot be determined if a variable weight is dropped from a constant height.

5.3 These test procedures have been found to be useful elements in rigid poly(vinyl chloride) (PVC) building product characterization. Compound qualification, finished product quality control, environmental and weatherability research and development studies, and fabrication tolerance prediction constitute useful applications.

5.4 Choice of the specific impactor head configuration used is related to a variety of product attributes, such as specimen

thickness and product toughness as well as abstract factors, such as the anticipated mode of failure in a specific application. The geometric uniqueness of the impactor head configurations prevents any comparison or correlation of testing results on samples tested with differing impactor head configurations. In general, the conical impactor, C.125, is useful to ensure failure of thicker specimens where the H.25 impactor caused no failure.

NOTE 2—Equivalent surface conditions are more likely to occur when specimens are prepared by compression molding or extrusion than by injection molding.

5.5 When comparing different samples tested with the same impactor head configuration, impact resistance shall be permitted to be normalized for average specimen thickness over a reasonably broad range (for example, 1 to 3 mm).³ However, this should only be done when the surface conditions listed in 6.1 are essentially equivalent.

6. Interferences

6.1 The results obtained are greatly influenced by the quality of the test specimens. Cracks usually start at the surface in tension; the surface opposite the one that is struck by the impactor head. The composition of this surface layer and the degree of orientation introduced during the formation of the specimen are very important variables. Flaws in this surface

³ O.R. Weaver, "Using Attributes to Measure a Continuous Variable in Impact Testing Plastic Bottles," Materials Research & Standards, MR & S, Vol. 6, No. 6, June, 1996, pp. 285-291.

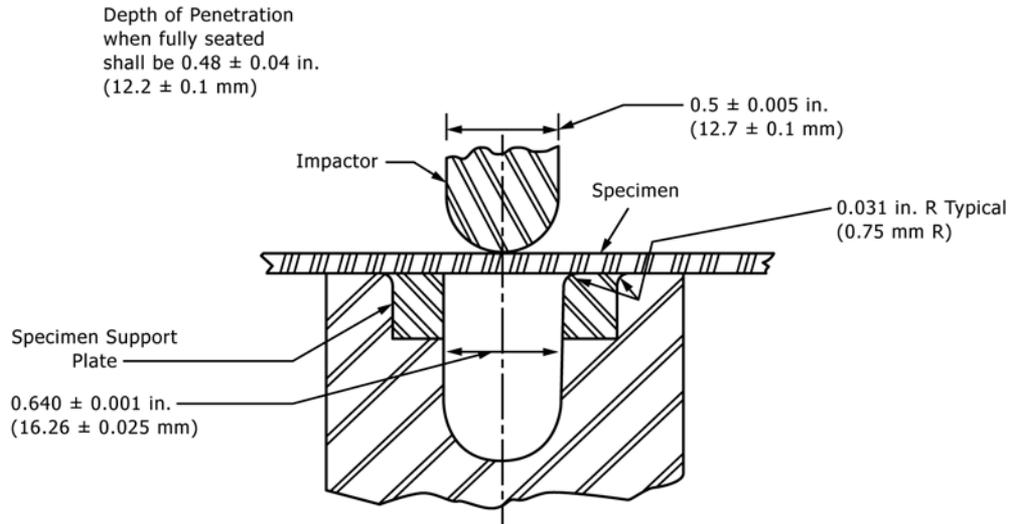


FIG. 3 Impactor Head Configuration H.25 Specimen Support Detail

will also affect results. Because of these factors, sometimes additional information about the sample is achieved by testing the sample from a variety of locations in a product or testing from both sides of a flat section.

6.2 Samples must not collapse into the hole in the specimen support plate when driven by the impactor. Sample collapse into the hole during the impact test affects impact results.

6.3 When resting on the support plate and in contact with the impactor the specimen must lie flat. Bowed samples will affect test results.

7. Apparatus

7.1 *Testing Machine*—The apparatus shall be constructed essentially as shown in Fig. 2 and Fig. 3 and shall consist of the following: suitable base to withstand the impact shock; steel-rod impact weight weighing 8 ± 0.2 lb (3.6 ± 0.1 kg); hardened steel impactors as specified in 7.1.2; a slotted guide tube 40 in. (1.0 m) in length in which the impact weights slide, having an internal diameter sufficient so that friction does not reduce the weight velocity, and having graduations in inch-pound (newton-meter) increments, or multiples thereof. A bracket is used to hold the tube in a vertical position by attaching it to the base and also to hold the hand knob, which is a pivot-arm alignment for the impactor, about 2 in. (50 mm) under the tube. The top edge of the opening in the specimen support plate should be rounded to a 0.031-in. (0.8-mm) radius. Fig. 3 shows the specimen support configuration for this test.

7.1.1 The tester shall be mounted so that the axis of the tube is plumb when measured with a spirit level at least 1 ft (300 mm) in length.

7.1.2 Impactor Configurations:

7.1.2.1 *Impactor C.125* shall be constructed, as is shown in Fig. 4, of tough, hardened (Rockwell C50-55), scratch resistant steel. It should have a conical (40°) configuration and 0.125-in. (3.18-mm) radius hemispherical tip.

7.1.2.2 *Impactor H.25* shall be constructed, as is shown in Fig. 3, of tough, hardened (Rockwell C50-55) scratch resistant steel. It should have a 0.25-in. (6.35-mm) radius hemispherical tip (see Fig. 3 and Fig. 4).

7.1.2.3 The surface of the impactor head shall be polished free of nicks, scratches, or other surface irregularities.

7.2 *Supporting Base*—In order to minimize the energy absorption, compression, and deflection of the support the tester shall be firmly fixed to a dense, solid, block or base.

7.2.1 The main body of said block or base shall have maximum dimensions of 16 in. (40 cm) (h) × 30 in. (75 cm) (w) × 30 in. (75 cm) (d) and shall have a minimum weight of 375 lb (171 kg). This block shall be placed at a height that facilitates equipment usage. It is not necessary to bolt blocks or bases of this weight to the floor.

NOTE 3—The required block weight and dimensions conform to commercially available butcher block type tables.

7.2.2 Alternative supporting bases or those lighter than 375 lb (171 kg) should be bolted to a concrete floor. Mean failure energy comparisons shall be made between these alternative supports and one where the tester is bolted directly to the concrete floor. If mean failure energy differences between the concrete floor and the alternative support are found statistically nonsignificant, use of the lighter support shall be allowed.

7.2.3 If the weight of the butcher block that was originally 375 lb (171 kg) or greater decreases with time to less than 375 lb (171 kg), increase the block weight to a minimum of 375 lb (171 kg) by adding a suitable amount of weight to the bottom of the table. The weight shall be tightly affixed and in direct contact with the bottom of the table and not cause any vibrations during the impact test.

NOTE 4—The weight of the butcher block can decrease over time, for instance, due to drying.

7.2.4 Use of rubber mats either under the tester or the supporting base is prohibited.