



SLOVENSKI STANDARD
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Cellular rubbers and plastics -- Determination of dynamic cushioning performance

Caoutchoucs et plastiques alvéolaires -- Détermination de la capacité d'amortissement
dynamique

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INTERNATIONAL STANDARD

ISO
4651

Second edition
1988-12-01



INTERNATIONAL ORGANIZATION FOR STANDARDIZATION
ORGANISATION INTERNATIONALE DE NORMALISATION
МЕЖДУНАРОДНАЯ ОРГАНИЗАЦИЯ ПО СТАНДАРТИЗАЦИИ

Cellular rubbers and plastics — Determination of dynamic cushioning performance

*Caoutchoucs et plastiques alvéolaires — Détermination de la capacité d'amortissement
dynamique*

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ISO 4651 : 1988 (E)

Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

Draft International Standards adopted by the technical committees are circulated to the member bodies for approval before their acceptance as International Standards by the ISO Council. They are approved in accordance with ISO procedures requiring at least 75 % approval by the member bodies voting.

International Standard ISO 4651 was prepared by Technical Committee ISO/TC 45, *Rubber and rubber products*.

This second edition cancels and replaces the first edition (ISO 4651 : 1979), sub-clauses 3.1, 7.1, 7.2.1, 7.2.2, 8.2 and 9.2 of which have been technically revised.

Annex A of this International Standard is for information only.

Cellular rubbers and plastics — Determination of dynamic cushioning performance

1 Scope

This International Standard specifies the procedure for determining the dynamic cushioning performance of cellular rubber materials and rigid and flexible cellular plastics, by measuring the peak deceleration of a mass when it is dropped on a test piece. The test described is intended primarily for quality assurance; in addition, however, since this type of test is also used to obtain design data, notes are given in annex A to assist in the latter respect.

The method is applicable solely to materials used in packaging.

2 Normative references

The following standards contain provisions which, through reference in this text, constitute provisions of this International Standard. At the time of publication, the editions indicated were valid. All standards are subject to revision, and parties to agreements based on this International Standard are encouraged to investigate the possibility of applying the most recent editions of the standards listed below. Members of IEC and ISO maintain registers of currently valid International Standards.

ISO 291 : 1977, *Plastics — Standard atmospheres for conditioning and testing*.

ISO 471 : 1983, *Rubber — Standard temperatures, humidities and times for the conditioning and testing of test pieces*.

ISO 845 : 1977, *Cellular rubbers and plastics — Determination of apparent density*.

ISO 1923 : 1981, *Cellular plastics and rubbers — Determination of linear dimensions*.

ISO 2231 : 1973, *Fabric coated with rubber or plastics — Standard atmospheres for conditioning and testing*.

ISO 3205 : 1976, *Preferred test temperatures*.

3 Definitions

For the purposes of this International Standard, the following definitions apply.

3.1 static stress, σ_{ST} : The total mass of the hammer and any additional masses multiplied by the gravitational acceleration g_n divided by the original area of the test piece.

3.2 peak deceleration, a : The maximum deceleration of the drop hammer during the impact on the test piece. In the International System of Units (SI), this is expressed in metres per second per second (m/s^2).

3.3 displacement curve: The curve describing the displacement of the impacted surface of the test piece as a function of time during the impact. (See annex A.)

3.4 dynamic stress: The decelerating force exerted by the material upon the drop hammer divided by the original area of the test piece.

3.5 deceleration force: The mass of the drop hammer multiplied by its instantaneous deceleration.

3.6 strain: Displacement expressed as a percentage of the original thickness.

3.7 dynamic compression diagram: The curve describing the relation between the dynamic stress (decelerating force per unit area) and the strain (displacement/thickness) in the cushioning material during impact. The slope of this curve at a specified strain (dynamic compressibility) may be used as a characteristic constant for the given speed of impact and the thickness of the test piece. (See annex A.)

3.8 cushioning diagram: The diagram indicating both the peak deceleration a and the maximum value ΔL_{max} of the displacement of the impact surface as a function of the static stress σ_{ST} for the test pieces of the concerned materials having given thickness L_0 . (See annex A.)

3.9 corrected value of peak deceleration, a_c : The value of the peak deceleration after correction for any small deviation of the test piece original thickness from the standard reference thickness of 50 mm. This is obtained by multiplying the measured peak deceleration by the original thickness divided by the standard reference thickness.

3.10 equivalent drop height, h : That drop height which, in conditions of free fall in vacuo under standard gravitational acceleration, would result in the same impact velocity of the hammer as was obtained during the test.

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The equivalent drop height, in metres, is given by the equation:

$$h = \frac{v^2}{2g_n}$$

where

v is the impact velocity, in metres per second, of the hammer;

g_n is the standard acceleration of free fall, i.e. 9,806 65 m/s².

4 Apparatus

4.1 General

The apparatus shall consist of a flat-based drop hammer, having a surface larger than the test piece, and an anvil of mass at least 100 times that of the drop hammer and whose face is parallel to the base of the drop hammer. Two basic types of dynamic testing equipment are in use (see figures 1 and 2). They are the guided vertical drop tester, in which the hammer drops between vertical guides on to the test piece which rests on the anvil, and the pendulum tester.

The guided vertical drop tester is preferred for high deceleration tests and/or high static stresses. The pendulum test is suitable for relatively low deceleration or low static stresses.

The hammer shall be fitted with a means of recording the peak value of deceleration on impact, with an accuracy of $\pm 5\%$, preferably by means of recording the deceleration time pulse on impact. Means shall also be available for measuring the velocity of the hammer, with an accuracy of $\pm 5\%$, immediately prior to impact. Suitable facilities such as a digital timer capable of recording the time of fall over 25 mm shall also be available for measuring the velocity of the hammer prior to impact with an accuracy of $\pm 1\%$. The measurement shall be completed, before impact, at a point on the path of the hammer which is within 5 mm of its position at initial impact.

A transducer complying with the requirements of 4.2.1 shall be mounted centrally on the hammer in such a way that distortion of the transducer is avoided. The cable carrying the signal from the impact transducer shall be mounted in such a way as to avoid excessive flexing at the transducer coupling.

The mass of the hammer shall be adjustable in the range of static stress required; alternatively, several hammers may be used. Where hammers are adjusted by means of added masses it is recommended that these be added to the top surface of the hammer.

It is important that both hammer and anvil be sufficiently rigid so that undesirable vibrations are not recorded in the deceleration-time curve. The natural frequency of vibration of the hammer shall be as high as practicable, preferably above 1 000 Hz.

Prior to testing, the velocity of the hammer at impact shall be checked; the velocity shall be at least 95 % of the equivalent free fall velocity. The equivalent free fall velocity shall be calculated using the equation

$$v = \sqrt{2g_n h}$$

where

v is the final free fall velocity, in metres per second;

g_n is the standard acceleration of free fall, i.e. 9,806 65 m/s²;

h is the measured height, in metres, of the hammer above the test piece.

CAUTION — It is essential that the drop hammer mechanism is such that the safety of the operator is assured when test pieces are placed on the anvil, and some form of safety interlock is recommended.

4.2 Recording equipment

The means of recording the deceleration-time pulses shall consist of a transducer, means of amplification, and recorder. Transducers generally are either piezoelectric or strain gauge types. The selection of specific recording equipment is optional. However, all recording equipment (including both transducer and recorders) shall have a frequency response adequate to measure the peak deceleration to an accuracy of $\pm 5\%$. The deceleration-time pulse obtained is usually a transient pulse approximating, on flexible foams, to a sinusoidal half-wavelength (half-sine) at low cushion displacements and becoming triangular or even spire-like, as illustrated in figure 3, for impacts producing high cushion displacements. On rigid foams, which crush on compression, the acceleration-time pulse may approximate to a steeply rising initial section, followed by a constant (or approximately constant) level before decreasing. The range of frequency response needed to measure these transient pulses is wider than might be anticipated. It is important, therefore, that the following requirements should be borne in mind in respect of the main elements of the recording equipment.

4.2.1 Transducers

Generally, these are either the piezoelectric or of the strain gauge type. Piezoelectric decelerometers have little inherent damping and, if the frequency of resonance is too low, they can be caused to resonate by the decelerating pulse, so producing overshoot errors. In general, these may be avoided by ensuring that the natural period of vibration of the transducer is less than 1/20 of the duration T of the deceleration pulse. However, for half-sine pulses or for pulses with a rapid initial rise, it is sufficient that the natural period of vibration is less than 1/10 of the pulse duration or 1/6 of the rise time of the pulse respectively.

Strain gauge or inductive decelerometers have higher inherent damping (between 0,4 and 0,7 of critical). To obtain an accuracy of better than 5 % in the measurement of peak deceleration, the decelerometer shall have a natural period of vibration of less than 1/3 of the pulse duration for half-sine or triangular pulses. For pulses with a rapid initial rise, the natural period shall be less than 1/6 of the rise time. A piezoelectric transducer of the annular shear type whose reactive elements are isolated from the mounting with a top connection is recommended.

Piezoelectric decelerometers do not respond to sustained signals and the low-frequency response depends on the succeeding part of the amplifier system. If the next stage is a cathode follower, the time-constant of the input circuit of the cathode follower, combined with that of the transducer, controls low-frequency response. To record peak decelerations to within 5 % on half-sine pulses, the time-constant shall be at least seven times the pulse duration T . For square-type pulses, the corresponding value shall be $20 T$.

If the following stage is a charge amplifier, then the response to continuous sine-waves shall not be reduced by more than 5 % at a frequency of $1/22 T$ for 5 % errors on half-sine pulses. The corresponding frequency for square pulses is $1/50 T$.

These figures, for the frequency at which the response to continuous sine-waves is reduced by 5 %, can be used also for any amplifying system where a.c. coupling is employed.

4.2.2 Recorders

The high-frequency response of cathode ray oscilloscopes is usually adequate. For galvanometer oscillographs, high-frequency response may be limited, and, as these devices are usually damped to 0,4 to 0,7 of critical, the galvanometer oscillograph should have a natural period of vibration of less than $1/3$ of the pulse duration for half-sine or triangular pulses. Oscilloscopes, and other recorders using a.c. amplifiers, can have inadequate low-frequency response, and the considerations outlined above concerning charge amplifiers shall be followed. It is possible for direct pen recorders to have inadequate response due to the inertia of the recording pen. It may be necessary to restrict the high-frequency response of the recorder in order to attenuate spurious output signals originating from mechanical resonance within the test equipment. The upper frequency shall be kept as high as possible, compatible with adequate attenuation of spurious signals. The minimum requirement is no more than 5 % attenuation at a frequency equivalent to twice the expected frequency.

Pulse durations and rise times depend on the type of material being tested and the conditions of test. For 50 mm thick test pieces, pulse durations on flexible foam in the range of 10 ms to 25 ms have been reported. For rigid materials, pulses may be short with rise times of the order of 2 to 5 ms. Peak reading meters can be used to obtain more accurate measurements of the deceleration on impact.

5 Test pieces

5.1 Shape and dimensions

The test piece shall be a right parallelepiped with the following dimensions:

- length 150 mm \pm 5 mm
- width 150 mm \pm 5 mm
- thickness 50 mm \pm 5 mm

The test piece shall be cut by any suitable means which does not alter the dynamic characteristics, for example a band-saw or a sharp knife. Hot wire shall not be used for cutting test pieces.

The difference in the mean thickness between the test pieces in a set of ten shall not be greater than 2 mm. The dimensions shall be measured in accordance with ISO 1923. The thickness of the test piece may be achieved by plying up not more than two sheets not less than 20 mm thick and of the same orientation with respect to any known direction of anisotropy.

5.2 Uniformity

The density of each test piece shall not vary by more than $\pm 10 \%$ from the average density of a set of 10 test pieces.

5.3 Orientation during testing

Test pieces cut from finished articles shall be tested so that the direction of dynamic stress corresponds with that of the dynamic stress to which the material is subjected in the finished article. If this is not possible, the relation of the direction of the principal dynamic stress in the finished article to that of the test direction shall be stated in the report.

5.4 Number

A total of at least ten test pieces shall be tested.

6 Pre-conditioning and test conditions

Samples shall be tested not less than 72 h after manufacture. Prior to testing, the test pieces shall be conditioned for at least 16 h in accordance with ISO 291, ISO 471 or ISO 2231, as appropriate. In cases of dispute, one set of conditions shall be agreed upon, preferably $23 \text{ }^\circ\text{C} \pm 2 \text{ }^\circ\text{C}$ and $50 \% \pm 5 \%$ relative humidity.

The conditioning period may form the latter part of the 72 h following manufacture. The tests shall be carried out under the same conditions unless otherwise agreed between supplier and purchaser.

7 Procedure

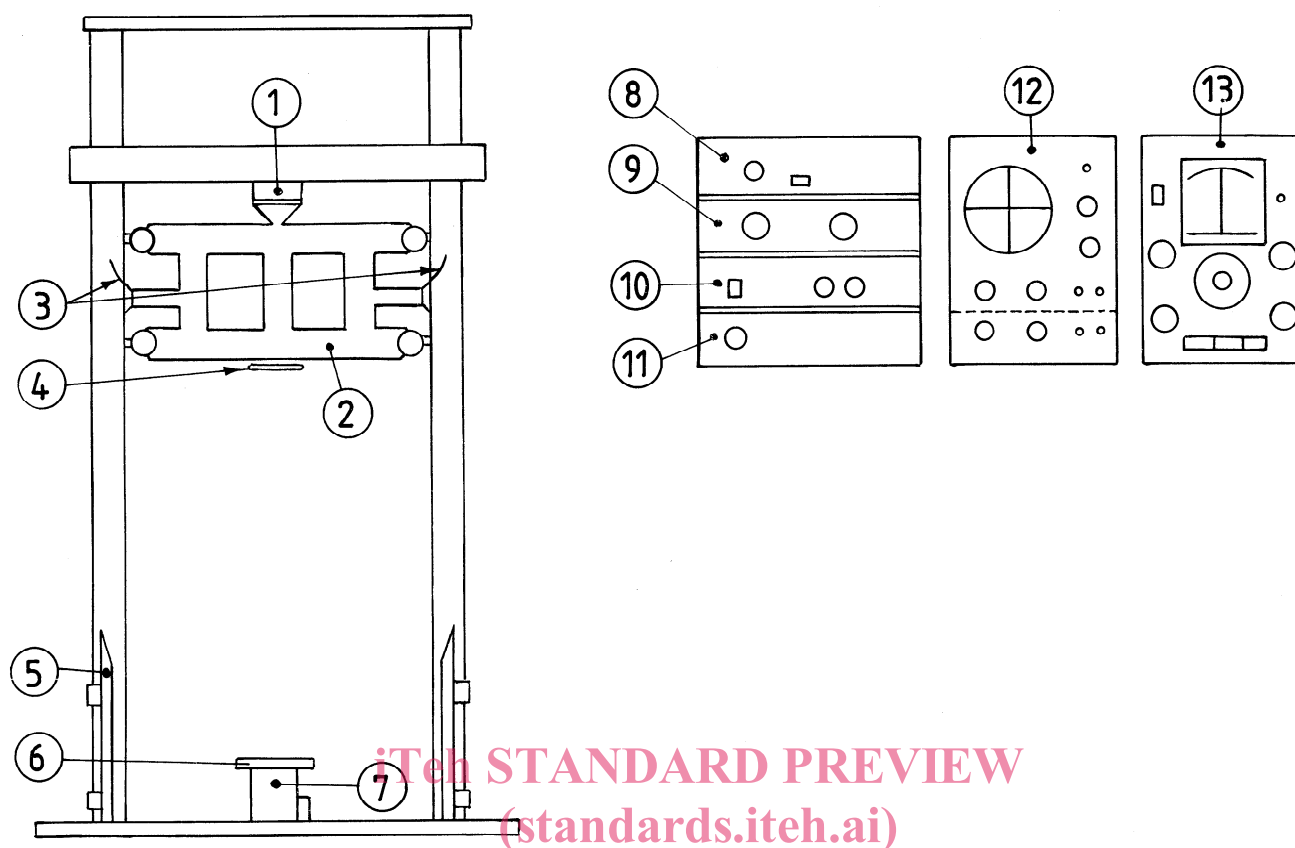
7.1 General

Record the original thickness of the test pieces, determined as indicated in 5.1. Measure the density of each test piece in accordance with ISO 845. Ensure that the drop hammer is in a safe position.

Place the test piece on the anvil of the apparatus, and prepare the drop hammer to impact on the test piece.

Impact the test piece three times at intervals of $60 \text{ s} \pm 15 \text{ s}$, using a fixed predetermined velocity and static stress as specified in 7.2 and 7.3 respectively. Measure the peak deceleration of the drop hammer on the first and third impacts. Each test piece shall be used for only one particular combination of static stress and impact velocity.

After the test piece has been subjected to the three impacts, allow it to recover for 5 min and remeasure its thickness.



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- 1 Electromagnet
- 2 Carriage
- 3 Sliding contacts for displacement potentiometer
- 4 Hammer
- 5 Displacement potentiometer
- 6 Test piece mount (anvil), 950 g
- 7 Pressure cell, 0 to 50 kN
- 8 Overload warning device for pressure cell
- 9 Automatic supply for photographic illumination
- 10 Electromagnet supply and supply for displacement potentiometer
- 11 a.c. stabilizer for all equipment
- 12 Double-beam oscilloscope, 0 to 300 kHz with automatic camera
- 13 Carrier-frequency linear amplifier, 50 kHz

Figure 1 — Typical arrangement of drop hammer apparatus for determination of dynamic cushioning performance

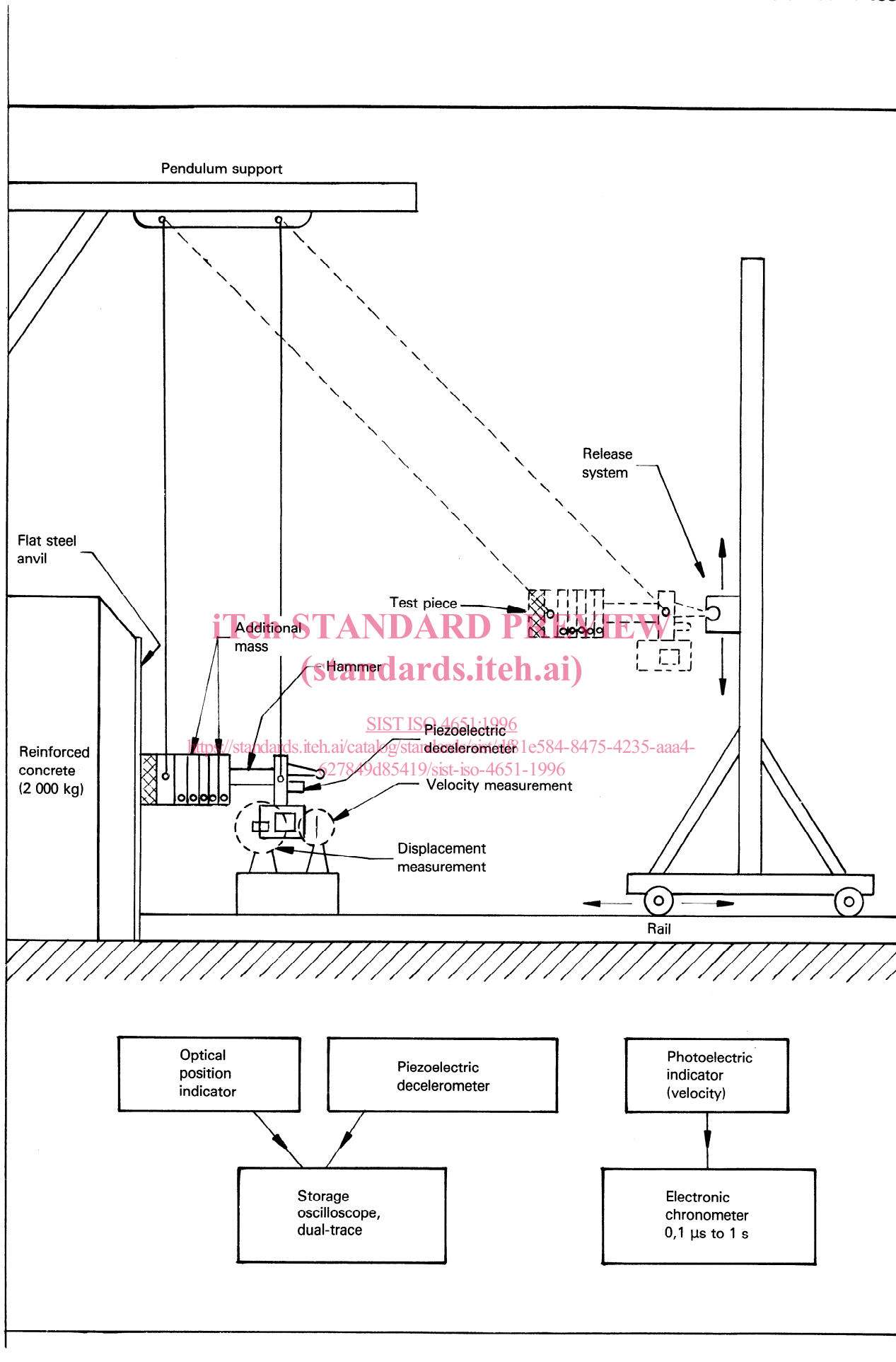


Figure 2 – Typical arrangement of pendulum apparatus for determination of dynamic cushioning performance