



Designation: D6286/D6286M – 20

Standard Guide for Selection of Drilling and Direct Push Methods for Geotechnical and Environmental Subsurface Site Characterization¹

This standard is issued under the fixed designation D6286/D6286M; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last approval. A superscript epsilon (ϵ) indicates an editorial change since the last revision or reapproval.

1. Scope*

1.1 This guide provides descriptions of various methods for site characterization along with advantages and disadvantages associated with each method discussed. This guide is intended to aid in the selection of drilling method(s) for geotechnical and environmental soil and rock borings for sampling, testing, and installation of wells, or other instrumentation. It does not address drilling for foundation improvement, drinking water wells, or special horizontal drilling techniques for utilities.

1.2 This guide cannot address all possible subsurface conditions that may occur such as, geologic, topographic, climatic, or anthropogenic. Site evaluation for engineering, design, and construction purposes is addressed in Guide D420. Soil and rock sampling in drill holes is addressed in Guide D6169/D6169M. Pertinent guides and practices addressing specific drilling methods, equipment, and procedures are listed in Section 2. Guide D5730 provides information on most all aspects of environmental site characterization.

1.3 The values stated in either SI units or inch-pound units (given in brackets) are to be regarded separately as standard. The values stated in each system may not be exact equivalents; therefore, each system shall be used independently of the other. Combining values from the two systems may result in nonconformance with the standard.

1.4 This guide does not purport to comprehensively address all methods and the issues associated with drilling for geotechnical and environmental purposes. Users should seek qualified professionals for decisions as to the proper equipment and methods that would be most successful for their site investigation. Other methods may be available for these methods and qualified professionals should have flexibility to exercise

judgment as to possible alternatives not covered in this guide. The guide is current at the time of issue, but new alternative methods may become available prior to revisions. Therefore, users should consult with manufacturers or producers prior to specifying program requirements.

1.5 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety, health, and environmental practices and determine the applicability of regulatory limitations prior to use.*

1.5.1 Drilling operators generally are required to be trained for safety requirements such as those of construction and environmental occupational safety programs dictated by country, regional, or local requirements such as the US. OSHA training programs. Drilling safety programs are also available from the National Drilling Association (NDA4U.com) or other country drilling associations.²

1.6 *This guide offers an organized collection of information or a series of options and does not recommend a specific course of action. This document cannot replace education and experience and should be used in conjunction with professional judgment. Not all aspects of this guide may be applicable in all circumstances. This ASTM standard is not intended to represent or replace the standard of care by which the adequacy of a given professional service must be judged, nor should this document be applied without consideration of a project's many unique aspects. The word "Standard" in the title of this document means only that the document has been approved through the ASTM consensus process.*

1.7 *This international standard was developed in accordance with internationally recognized principles on standardization established in the Decision on Principles for the Development of International Standards, Guides and Recommendations issued by the World Trade Organization Technical Barriers to Trade (TBT) Committee.*

¹ This guide is under the jurisdiction of ASTM Committee D18 on Soil and Rock and is the direct responsibility of Subcommittee D18.21 on Groundwater and Vadose Zone Investigations.

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² "Drilling Safety Guide," National Drilling Federation, Columbia, SC, 1985, p. 36.

*A Summary of Changes section appears at the end of this standard

2. Referenced Documents

2.1 *ASTM Standards*:³

- D420** Guide for Site Characterization for Engineering Design and Construction Purposes
- D653** Terminology Relating to Soil, Rock, and Contained Fluids
- D1452/D1452M** Practice for Soil Exploration and Sampling by Auger Borings
- D2113** Practice for Rock Core Drilling and Sampling of Rock for Site Exploration
- D2488** Practice for Description and Identification of Soils (Visual-Manual Procedures)
- D3740** Practice for Minimum Requirements for Agencies Engaged in Testing and/or Inspection of Soil and Rock as Used in Engineering Design and Construction
- D5088** Practice for Decontamination of Field Equipment Used at Waste Sites
- D5092/D5092M** Practice for Design and Installation of Groundwater Monitoring Wells
- D5608** Practices for Decontamination of Sampling and Non Sample Contacting Equipment Used at Low Level Radioactive Waste Sites
- D5730** Guide for Site Characterization for Environmental Purposes With Emphasis on Soil, Rock, the Vadose Zone and Groundwater (Withdrawn 2013)⁴
- D5753** Guide for Planning and Conducting Geotechnical Borehole Geophysical Logging
- D5778** Test Method for Electronic Friction Cone and Piezocone Penetration Testing of Soils
- D5781/D5781M** Guide for Use of Dual-Wall Reverse-Circulation Drilling for Geoenvironmental Exploration and the Installation of Subsurface Water Quality Monitoring Devices
- D5782** Guide for Use of Direct Air-Rotary Drilling for Geoenvironmental Exploration and the Installation of Subsurface Water-Quality Monitoring Devices
- D5783** Guide for Use of Direct Rotary Drilling with Water-Based Drilling Fluid for Geoenvironmental Exploration and the Installation of Subsurface Water-Quality Monitoring Devices
- D5784** Guide for Use of Hollow-Stem Augers for Geoenvironmental Exploration and the Installation of Subsurface Water Quality Monitoring Devices
- D5872** Guide for Use of Casing Advancement Drilling Methods for Geoenvironmental Exploration and Installation of Subsurface Water Quality Monitoring Devices
- D5875/D5875M** Guide for Use of Cable-Tool Drilling and Sampling Methods for Geoenvironmental Exploration and Installation of Subsurface Water Quality Monitoring Devices
- D5876/D5876M** Guide for Use of Direct Rotary Wireline Casing Advancement Drilling Methods for Geoenviron-

- mental Exploration and Installation of Subsurface Water-Quality Monitoring Devices
- D6001** Guide for Direct-Push Groundwater Sampling for Environmental Site Characterization
- D6151/D6151M** Practice for Using Hollow-Stem Augers for Geotechnical Exploration and Soil Sampling
- D6169/D6169M** Guide for Selection of Soil and Rock Sampling Devices Used With Drill Rigs for Environmental Investigations
- D6429** Guide for Selecting Surface Geophysical Methods (Withdrawn 2020)⁴
- D6910/D6910M** Test Method for Marsh Funnel Viscosity of Construction Slurries
- D6914/D6914M** Practice for Sonic Drilling for Site Characterization and the Installation of Subsurface Monitoring Devices

2.2 *Geotechnical Sampling, In situ Testing, and Instrumentation in Drill Holes*:

- D1586/D1586M** Test Method for Standard Penetration Test (SPT) and Split-Barrel Sampling of Soils
- D1587/D1587M** Practice for Thin-Walled Tube Sampling of Fine-Grained Soils for Geotechnical Purposes
- D2573/D2573M** Test Method for Field Vane Shear Test in Saturated Fine-Grained Soils
- D3550/D3550M** Practice for Thick Wall, Ring-Lined, Split Barrel, Drive Sampling of Soils
- D4403** Practice for Extensometers Used in Rock
- D4428/D4428M** Test Methods for Crosshole Seismic Testing
- D4719** Test Methods for Prebored Pressuremeter Testing in Soils
- D6519** Practice for Sampling of Soil Using the Hydraulically Operated Stationary Piston Sampler
- D6598** Guide for Installing and Operating Settlement Points for Monitoring Vertical Deformations
- D6635** Test Method for Performing the Flat Plate Dilatometer
- D7299** Practice for Verifying Performance of a Vertical Inclinometer Probe

2.3 *Sampling, Testing, and Installations in Drill Holes*:

- D4700** Guide for Soil Sampling from the Vadose Zone
- D4044/D4044M** Test Method for (Field Procedure) for Instantaneous Change in Head (Slug) Tests for Determining Hydraulic Properties of Aquifers
- D4050** Test Method for (Field Procedure) for Withdrawal and Injection Well Testing for Determining Hydraulic Properties of Aquifer Systems
- D4630** Test Method for Determining Transmissivity and Storage Coefficient of Low-Permeability Rocks by In Situ Measurements Using the Constant Head Injection Test
- D6282/D6282M** Guide for Direct Push Soil Sampling for Environmental Site Characterizations
- D6724/D6724M** Guide for Installation of Direct Push Groundwater Monitoring Wells
- D6725/D6725M** Practice for Direct Push Installation of Prepacked Screen Monitoring Wells in Unconsolidated Aquifers

³ For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

⁴ The last approved version of this historical standard is referenced on www.astm.org.

- D6907** Practice for Sampling Soils and Contaminated Media with Hand-Operated Bucket Augers
- D7242/D7242M** Practice for Field Pneumatic Slug (Instantaneous Change in Head) Tests to Determine Hydraulic Properties of Aquifers with Direct Push Groundwater Samplers
- D7352** Practice for Volatile Contaminant Logging Using a Membrane Interface Probe (MIP) in Unconsolidated Formations with Direct Push Methods
- D7648/D7648M** Practice for Active Soil Gas Sampling for Direct Push or Manual-Driven Hand-Sampling Equipment
- D8037/D8037M** Practice for Direct Push Hydraulic Logging for Profiling Variations of Permeability in Soils

3. Terminology

3.1 Definitions:

3.1.1 For definitions of common technical terms used within this guide, refer to Terminology **D653**.

3.2 Definitions of Terms Specific to This Standard:

3.2.1 *borehole wall, n*—refers to the naturally-occurring soil(s)/rock(s) surrounding the borehole.

3.2.2 *kelly bar, n—in drilling*, a formed or machined section of hollow drill steel used in rotary drilling, which is joined directly to the swivel at the top and to the drill pipe below.

3.2.2.1 *Discussion*—The flats or splines of the kelly bar engage the rotary table so that the rotation of the rotary table turns the kelly bar, which in turn, rotates the drill pipe and the rotary bit.

3.2.3 *mud rings, n—in drilling*, soil or rock cuttings that form a ring or rings on the drill rod(s) during a rotary-drilling method, and as such, prevent drill cuttings from being carried up and out of the borehole.

3.2.3.1 *Discussion*—These rings can cause drill rods to become stuck in the borehole if sufficient drilling fluid is not injected or pumped downhole to keep the cuttings fluid so that the ring(s) cannot form on the drill rods and block the cuttings return as drilling progresses.

3.2.4 *orange-peel bucket, n—in drilling*, a bucket-type device, somewhat elliptical in shape resembling an orange peel, that is lowered down the borehole and used to remove boulders from the bottom of a borehole.

3.2.5 *unconsolidated geologic materials, n—in groundwater, geology, or hydrogeology*, a loosely aggregated solid (particulate) material of geologic origin (soil, sediments, etc.).

3.2.5.1 *Discussion*—Groundwater hydrologists, and geologists, use the terms unconsolidated formations, deposits, sediments, units, materials, etc., to refer to the general term “soil” including other soils (alluvium, glacial till, etc.) as defined in **D653**. These terms are often found in groundwater standards applied to aquifers. Unconsolidated materials are non-lithified, typically lacking cementation of individual particles (clay, silt sand, gravel, etc.). The term “unconsolidated” should not be confused with geotechnical terms of the degree of soil consolidation (over, normally, under-consolidated) as defined in **D653**.

4. Significance and Use

4.1 The 1998 edition of this standard was written solely for selection of drilling methods for environmental applications and specifically for installation of groundwater monitoring wells. The second revision was made to include geotechnical applications since many of the advantages, disadvantages, and limitations discussed extensively throughout this document also apply to geotechnical design use such as data collection (sampling and in-situ testing) for construction design and instrumentation. Besides installation of monitoring wells (**D5092/D5092M**, **D6724/D6724M**), Environmental investigations are also made for sampling, in-situ testing, and installation of aquifer testing boreholes (**D4044/D4044M**, **D4050**).

4.2 There are other guides for geotechnical investigations addressing drilling methods such as in Eurocode (**1, 2**)⁵, U.S. Federal Highway Administration, (**3, 4**), U.S. Army Corps of Engineers, (**5**), and U.S. Bureau of Reclamation (**6, 7**). An authoritative Handbook on Environmental Site Characterization and Ground-Water Monitoring was compiled by Nielsen (**8**) which addresses drilling methods in detail including the advent of Direct Push methods developed for environmental investigations. Two other major drilling guides have been written by the National Drilling Association (**9**) and from the Australia Drilling Industry Training Committee (**10**) and these guides are user for the drillers.

4.3 **Table 1** lists sixteen classes of methods addressed in this guide. The selection of particular method(s) for drilling/push boring requires that specific characteristics of each site be considered. This guide is intended to make the user aware of some of the various drilling/push boring methods available and the applications, advantages, and disadvantages of each with respect to determining geotechnical and environmental exploration.

4.3.1 On **Table 1**, practically all methods allow for coring, but some are much more efficient than others. Some drilling systems such as hollow-stem augers or wireline coring allow for practically continuous coring with minimal time for switching barrels while other drilling methods require the whole drilling equipment be removed from the hole. A prime example is the rate of rock coring using fluid rotary and conventional core barrels versus wireline rock coring. Wireline line rock coring is fast with long continuous runs whereas fluid rotary requires more “trip time” to add and remove shorter length core barrels using drill rods. **Table 1** delineates methods where coring is possible, and in general, by either continuous (c) or incremental (i) sampling.

4.3.2 Sampling for environmental contaminants in soil, unconsolidated formations or groundwater often requires special considerations. In many environmental applications the use of drilling fluids (air, water, mud or foam) is often discouraged or even prohibited as these fluids may dilute the analytes of interest or even introduce analytes of concern not previously present (see **5.4**).

⁵ The boldface numbers in parentheses refer to the list of references at the end of this standard.

TABLE 1 Drilling Selection Guide

Drilling Method	Drilling Fluid	Casing Advance	Type of Material Drilled	Typical Depth, in m [ft] ^A	Typical Range of Borehole Sizes, in cm [in.]	Samples Obtainable ^B	Coring Possible (see 4.3.1) ^C	Reference Section
Power auger (Hollow-stem)	none, water, mud	yes	soil, weathered rock	<45 [150]	12.7-55 [5-22]	S, F	Yes(c)	6.2
Power auger (Solid-stem)	none	no	soil, weathered rock	<45 [150]	5-25 [2-10]	S	Yes(i)	6.3
Power bucket auger	none, water (below water table)	no	soil, weathered rock	<45 [150]	45-120 [18-48]	S	Yes(i)	6.4
Hand auger	none	no	soil	<20 [70] (above water table only)	5-15 [2-6]	S	Yes(i)	6.5
Direct fluid rotary	water, mud	yes	soil, rock	>300 [1000]	5-90 [2-36]	S, R	Yes(i)	7
Sonic (vibratory)	none, water, mud, air	yes	soil, rock, boulders	<150 [500]	10-30 [4-12]	S, R, F	Yes(c)	8
Direct-push technology	none	yes	soil, weathered rock	Typical 15-30 [50-100] Maximum 60 [200]	3.8-15 [1.5-6]	S, F	Yes(c)	9
Air rotary, Casing-advancer	air, water, mud	yes	soil, rock, boulders	<600 [2000]	5-40 [2-16]	S, R, F	Yes(c)	10.3
Reverse circulation, air rotary	air, water, foam	yes	soil, rock	>300 [1000]	30-90 [12-36]	S, R, F	Yes(i)	12
Reverse circulation, fluid rotary	water, mud	yes	soil, rock	<600 [2000]	30-90 [12-36]	S, R, F	Yes(i)	12.3
Cable tool	water	yes	soil, rock	<1500 [5000]	10-60 [4-24]	S, R, F (F—below water table)	Yes(i)	13
Jet percussion	water	no	soil	<15.0 [50]	5-10 [2-4]	S	no	14
Jetting	water	yes	soil	<15 [50]	10 [4]	S	no	14

^AActual achievable drilled depths will vary depending on the ambient geohydrologic conditions existing at the site and size of drilling/push boring equipment used. For example, large, high-torque rigs can drill to greater depths than their smaller counterparts under favorable site conditions. Boreholes drilled using air/air foam can reach greater depths more efficiently using two-stage positive-displacement compressors having the capability of developing working pressures of 12 to 17 kPa [250 to 350 psi] and 14 to 21 m³/h [500 to 750 cfm], particularly when submergence requires higher pressures. The smaller rotary-type compressors only are capable of producing a maximum working pressure of 6 kPa [125 psi] and produce 14 to 34 m³/h [500 to 1200 cfm]. Likewise, the rig mast must be constructed to safely carry the anticipated working loads expected. To allow for contingencies, it is recommended that the rated capacity of the mast be at least twice the anticipated weight load or normal pulling load.

^BSoil = S (Cuttings), Rock = R (Cuttings), Fluid = F (some samples might require accessory sampling devices to obtain).

^CI = Incremental sampling, C = continuous sampling.

4.4 This guide is most often used in conjunction with Guide **D6169/D6169M** on soil and rock sampling because sampling is the primary activity during drilling/push borings. There are several guides that deal with individual drilling methods (see Guides **D5781/D5781M**, **D5782**, **D5783**, **D5784**, **D5872**, **D5875/D5875M**, and **D5876/D5876M**) and how to the complete them for water quality monitoring well installations (see Practice **D5092/D5092M**). Practices on hollow-stem auger (**D6151/D6151M**) and sonic drilling (**D6914/D6914M**) were written for both geotechnical and environmental purposes and address sampling methods. Practice **D2113** on rock core drilling includes sampling methods.

4.4.1 This guide covers direct push methods that are only used to make open holes for testing and sampling. This most often accomplished using dual tube systems and using the tubes for access of the subsurface for water sampling, **D6001**,

soil sampling (**D6282/D6282M**), well installation (**D6724/D6724M**, **D6725/D6725M**) and aquifer testing (**D7242/D7242M**).

4.5 Predominant or Typical Drilling/Push Boring Methods Used for Geotechnical and Environmental Applications:

4.5.1 *Geotechnical Investigations in Soils (unconsolidated deposits)*—The most commonly used drilling methods for geotechnical exploration are fluid rotary drilling when groundwater is present. Hollow-stem auger drilling is also frequently used especially in arid regions where introduction of fluids is to be avoided in unsaturated soils.

4.5.2 *Environmental Investigations in soils (unconsolidated deposits)*—Most of these investigations are focused on soil contamination or, groundwater quality investigations so introduction of drilling fluids is not desirable and methods which



generate minimal waste are highly favored. Direct Push methods were developed because they develop minimal investigative derived waste (IDW). Sonic methods are frequently used and generate minimal IDW but large cores. Hollow-stem augers and fluid rotary are used yet they generate large amounts of IDW.

4.5.2.1 At most environmental sites hazardous contaminants are present in the subsurface. Because of this fact any drill cuttings or drilling fluids returned to the surface should be properly handled, contained and stored (drums or roll-off bins, etc.) for sampling and laboratory analysis. Laboratory analyses may be required to verify that hazardous contaminants are not present above regulatory action levels prior to proper disposal. If concentrations of hazardous chemicals in cuttings or waste drilling fluids exceed regulatory action levels the waste may require treatment before disposal or may need to be properly disposed in a hazardous waste landfill. Review pertinent regulations before drilling/push boring to maintain compliance. The generation of contaminated waste drill cuttings and fluids significantly increase the potential for worker exposure to hazardous contaminants. Review pertinent regulations (such as OSHA 1910.120, etc.) to maintain compliance with worker safety and monitoring requirements.

4.5.3 *Rock, Weathered Rock, and Coarse Cobble Boulder Drilling*—Wireline rock coring is used in competent rock and results in the best core recovery. For coarse grained unconsolidated deposits and weathered bedrock samples are very difficult to recover and, rotary air drill through drive casing advancers are often used and require larger drills. Larger sonic drills can also drill and recover rock and boulder formations.

4.5.4 Sonic drilling methods have increased in use for both geotechnical and environmental explorations. The method offers very rapid continuous coring with the ability to drill difficult formations with large diameter equipment.

4.5.5 Shallow hand auger (D4700) is used for both disciplines but in most cases hand applications are used as part of initial site surveys prior to drilling/push boring or just for characterization of shallow soil sampling. Hand auguring is very labor intensive and has almost been abandoned in favor of using direct push equipment.

NOTE 1—The reliability of data and interpretations generated by this practice is dependent on the competence of the personnel performing it and the suitability of the equipment and facilities used. Agencies that meet the criteria of Practice D3740 generally are considered capable of competent testing. Users of this practice are cautioned that compliance with Practice D3740 does not assure reliable testing. Reliable testing depends on several factors and Practice D3740 provides a means of evaluating some of these factors.

Practice D3740 was developed for agencies engaged in the testing, inspection, or both, of soils and rock. As such, it is not totally applicable to agencies performing these field practices. Users of this test method should recognize that the framework of Practice D3740 is appropriate for evaluating the quality of an agency performing drilling. Currently, there is no known qualifying national authority that inspects agencies that perform this test method. There is training and certification for drillers that are normally required for critical installations such as water well drilling (NGWA, NDA).

5. Program Planning and Drilling/Push Boring Considerations

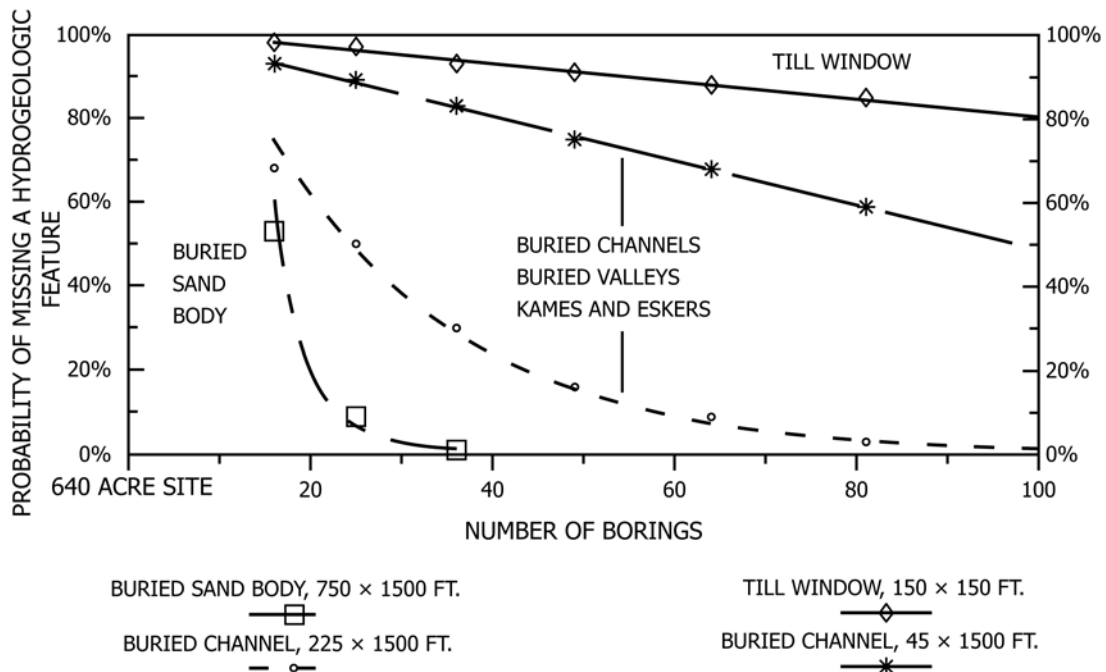
5.1 All factors affecting both surface and subsurface environment at a specific site requires professional judgment and

must be considered by the geologist/hydrologist or experienced driller before a drilling/push boring method is selected. Development of a Conceptual Site Model (CSM) of significant soil and rock masses and groundwater conditions within a given site should be described and defined, both vertically and horizontally, before drilling. Site planning requires a reconnaissance site investigation that considers access to the site and conditions for setting up the drilling/push boring equipment (1-8). The extent of site characterization and specific methods used will be determined by study objectives. Study objectives also will affect the type and complexity of data collected. Sources of data that may be useful during initial site evaluation include, but are not limited to, topographic maps, aerial photography, satellite imagery, information from reconnaissance drilling/push borings, borehole geophysical-log data, geologic maps and reports, statewide or county soil surveys, water-resource reports, well databases, and mineral-resource surveys covering the proposed project area. Available reports of surface and subsurface investigations of nearby or adjacent projects should be considered and the information applicable to the current project evaluated and applied if determined reliable and beneficial. At any site review nearby, available borings and discuss drilling/push boring methods with local contractors experienced with the geologic conditions.

5.2 Once the desk studies and field reconnaissance are performed, onsite explorations are normally phased using subsurface screening methods to refine the CSM before final selection of drill hole locations. Site-specific surface geophysical surveys (D6429) (11-15), direct-push soil or water sampling (D6282/D6282M, D6001), hydraulic profiling (D8037/D8037M), cone penetrometers (D5778), dynamic cone penetrometers, or solid stem power augers (D1452/D1452M) can be performed in grid patterns across the site to refine the stratigraphy of the geology at the site and may detect problem areas for targeting with drilling/push boring and sampling. Surface geophysical methods, such as seismic surveys and electrical-resistivity imaging and electromagnetic-conductance surveys, can be valuable particularly when distinct differences in the properties of contiguous subsurface materials are indicated (16, 17). When free product petroleum fuels are present in the subsurface, membrane interface probe (D7352), or high-resolution fluorescence logging with induced fluorescence or optical image probes can be used to identify depths and locations to target for sampling by drilling/push boring methods (18, 19).

5.2.1 The odds of detecting certain critical geologic features of interest on large sites are greatly improved using screening methods prior to drilling/push boring and can be used to reduce the amount of expensive drill holes. Fig. 1 shows the number of drill holes and the probability of detecting several types of geologic features at a 260 ha [640-acre, 1 square mile] site (8). Without screening methods using geophysics and low-cost probing or drilling/push boring methods, some geologic features could be totally missed even with 100 drill holes. Further, the screening methods can be used to reduce the amount of drill holes and target them on critical layers.

5.3 *Geotechnical Considerations*—Drilling/push boring activities for geotechnical investigations include sampling (both



The probability of finding many types of subsurface geologic features using borings alone is fairly low. The use of supportive studies such as surface geologic mapping, aerial photo interpretation, and surface and borehole geophysics can greatly improve the chances of successfully mapping the subsurface. Without a complete and accurate map of the subsurface, site models can be misleading.

FIG. 1 Probability of Finding Geologic Features Using Only Drill Holes on a Large Site (8)

disturbed or intact for laboratory testing), in situ testing, and installation of monitoring devices such as piezometers (observation wells), or inclinometers (see ASTM procedures cited in 2.2). Ideal drilling/push boring methods often are dictated by soil or rock types and the likelihood of the method to disturb soils ahead of the drilling operation, but more importantly is the presence of groundwater. Fluid rotary drilling predominates in humid areas with shallow groundwater, whereas in arid areas, the hollow-stem auger is more commonly used. With unsaturated soils in arid regions it may not be desirable to use fluid drilling methods that could wet soil samples prematurely ahead of laboratory testing of samples. A common drilling/push boring test is the standard penetration test (D1586/D1586M) and only certain drilling/push boring methods are suitable. When drilling in hydraulic structures such as dams and levees, drill methods should be selected that minimize the potential for hydraulic fracturing (see 5.6.2). Air drilling should not be used in impervious cores of dams and levees.

5.4 Environmental Considerations—Environmental drilling/push boring is primarily for the collection of samples and installation of groundwater monitoring wells (see standards listed in 2.3). An authoritative reference for well drilling and installation can be found in groundwater and wells (20). Environmental considerations include preservation of sample representativeness for chemical contamination, aquifer integrity, and reduction in waste (IDW). Drilling/push boring methods that do not use fluids are most often used and measures are taken given in 5.4.1 below. Direct push and sonic methods using no fluids and generate minimal waste (IDW) and provide the borehole wall protection with casings. Direct

push equipment has the potential to perform many different in-situ tests as drilling progresses (2.3). Groundwater monitoring wells using drilling/push boring methods in this standard are designed and installed in accordance with D5092/D5092M and direct push wells are installed with accordance with ASTM D6724/D6724M and D6725/D6725M for prepacked wells.

5.4.1 If the monitoring well also is to be sampled for water quality during the fluid drilling process, the possible damage and subsequent aquifer contamination caused by drilling-fluid invasion of the borehole wall that may occur during drilling must be considered. Drilling-fluid invasion of the borehole wall normally results from the use of a poorly-controlled and improperly-designed drilling-fluid program. Drill fluids are designed to coat and partially penetrate the wall of the drill hole to stabilize the boring. Water used as a drilling fluid or to prepare drilling muds must be tested to verify it is clean and free of the contaminants of interest or other potential contaminants not present at the site. Often, municipal water is chlorinated and as such could contain trihalomethanes which are regulated contaminants in groundwater.

5.4.2 The project manager should review the project work plan, sampling plan and quality assurance plan prior to selection of the drilling/push boring method(s) to be used at the facility under investigation to assure the proper drilling and sampling practices are used to meet specified project requirements. While some drilling/push boring practices may be more time efficient if they yield non-representative samples then the resulting geological, water quality and analytical results may be inaccurate and misleading for the purposes of an environmental investigation. This could result in the development of

an inaccurate (CSM) and remediation action, and significant lifetime cost increases to achieve site closure for contaminated facilities.

5.4.3 Dry Drilling/Push Boring Methods Preferred—Drilling/push boring methods that do not use a drilling fluid are preferable because they preclude possible aquifer contamination from such fluids. Direct push methods for monitoring well installation minimize or preclude the use of drilling fluids. Other drilling methods that normally preclude the use of drilling fluids include hollow- and solid-stem auger drilling, hand auger drilling (only an effective shallow-drilling method when used to drill above the water table), bucket auger drilling, resonant sonic-drilling method, and cable-percussion drilling methods. Methods that normally require the use of a drilling fluid for drilling include jet-wash and jet-percussion drilling, reverse-circulation drilling, and fluid- and air-rotary drilling. In cases where drilling-fluid loss occurs during drilling, estimates of the amounts of fluid loss and depth(s) of these occurrences in the borehole should be documented. Drilling-fluid loss data may be useful in planning well-development techniques to be used upon completion of the borehole. Another crucial factor to be considered when evaluating this data is well-screen placement.

5.4.3.1 Use of Dry drilling/Push Boring Methods Below the Water Table—Dry drilling/push boring methods such as direct push, sonic, and hollow-stem augers all suffer from problems when used below the water table, especially in sands which are the target aquifers for testing or well placement. Sand below the water table can be unstable and heave into the casings. In these cases, and if permitted, in the work plan water may have to be added to stabilize water levels in the boring (5.4.1). The alternative is to retract casings which may have further disturbance to the base of the boring. Any borings with casing left overnight will likely fill with groundwater to the level of the groundwater table and provisions may have to be made to remove this water via bailing or air lifting prior to well installation or resumed sampling if required in the work plan. Alternately, the water in the casing may have to remain and create a balance with the existing aquifer during the resumption of drilling activities.

5.4.4 Use of Cased Methods—Drilling/push boring methods that advance the casing as drilling proceeds are very effective methods to minimize the effects of groundwater migration along the casing and can maintain seal across multiple aquifers. Dual tube direct push equipment, sonic drilling, casing advancer methods (10.3) and reverse circulation all advance casings continuously during the drilling process. Hollow-stem augers provide a stable inner casing but allow mixing of soil and water on the auger flights. Incremental open hole drilling and sampling such as fluid rotary drilling may require telescoped casing (5.4.4.1) to seal off multiple aquifer zones separated by confining units.

5.4.4.1 Sealing Across Aquifers in Open Hole Drilling – Telescoping—The practice of incremental open hole drilling/push boring and sampling in uncased borings, using temporary casings through separate aquifers, can result in cross-contamination. To avoid or minimize the possibility of borehole cross-contamination or leakage from occurring whenever

an aquitard or impermeable confining layer of material is drilled through, using any drilling/push boring method or a combination thereof, the following technique is suggested, particularly when drilling under saturated conditions. The impermeable material should be drilled into but not completely through. Casing should be installed into the impermeable material and pressure cemented/grouted into place with the use of centralizers. After the cement/grout has adequately cured, the material remaining in the casing can be drilled out. Borehole geophysical methods (see D5753) then can be used to evaluate the seal between the borehole annulus and the wall of the casing. After an acceptable seal has resulted, drilling completely through the confining layer can be done. Continue drilling/sampling/coring operations until the desired borehole depth has been reached. If other confining layer(s) are to be drilled in the same borehole, the above technique(s) can be followed. The next casing installed should be the next smaller size to the previously-installed casing (21).

5.4.5 Casing advancers are often used in coarse grained deposits and weather bedrock. If the tendency of this method is to over ream the hole, contamination may move along the casing during drilling. Air rotary drilling should not be used for most environmental investigations, especially when Volatile Organic Compounds (VOCs) are under investigation or contaminants effected by changes in Oxidation Reduction Potential (ORP) are under investigation. Air rotary drilling can strip VOCs from the formation and groundwater resulting in low biased analytical data for environmental investigations. Additionally, air rotary drilling can and has contaminated formations with compressor oils or VOCs present in the local ambient atmosphere. Air rotary drilling can also fracture the surrounding ground mass if circulation is lost.

5.4.6 Ultimately, selection of a drilling/push boring method from several possible methods must be made only after weighing all of the advantages and disadvantages of each method against data-collection objectives. In some cases, a drilling/push boring method that minimizes the potential for subsurface contamination by the drilling process might limit the types of other data that can be collected, for example, borehole-geophysical data (5.9), from the well. For example, fluid-rotary drilling methods are good drilling methods to use for determining subsurface lithologic characterization because most borehole electric and sonic geophysical-logging tools require uncased fluid-filled boreholes

5.4.7 Selection of a drilling method must consider all aspects of monitoring-well installation, including casing materials and composition, screen(s), subsurface monitoring equipment and installation(s), grouting materials and placement procedure(s), as well as any other plans for well completion and development. For example, when a drilling/push boring method is used that might affect groundwater chemistry, the well development required to remove artifacts of the drilling can be intensive, time consuming, and affect water chemistry.

5.4.8 The planning of the type(s) of drilling/push boring equipment to be used on the project should include sampling requirements and well-completion requirements consideration(s). For instance, grouting and placement of well screen(s) are common well-completion requirements, and the ability to

accomplish either of these is dependent greatly on the type of equipment used. The accomplishment of satisfactory hole-abandonment procedures, as well as the ease at which any drilling/push boring equipment can be decontaminated are also important factors to be considered. It is standard procedure to have to clean equipment prior to entrance and exit from the site as well as decontamination of sampling and installation equipment during drilling operations using procedures given in **D5088** and **D5608**.

5.5 Drill Hole Diameter—Drilling depth and borehole diameters shown in **Table 1** are nominal values for the method and may vary for specific cases or conditions. Drill hole diameter is probably the most important consideration for selection or drilling/push boring methods.

5.5.1 Geotechnical Considerations—Drill hole diameter directly affects sample quality with larger diameters yielding higher quality samples using most all sampling methods, disturbed or intact. The majority of geotechnical work requires a minimum borehole inside diameter of 100 mm [4 in.] for soils. Intact sampling of soils for laboratory testing are greatly improved by using 150 mm [6 in.] boreholes (**D1587/D1587M**). For rock coring, NQ3 is often used for mineralogical investigations but the larger HQ3 and PQ3 size yields better cores and allows for water testing.

5.5.2 Environmental Considerations—The diameter of the borehole and the well casing for conventionally drilled filter packed monitoring well should be selected so that a minimum annular space of 2 in. [50 mm] is maintained between the inside diameter of the casing and outside diameter of the riser to provide working space for a tremie pipe (Practice **D5092/D5092M**). Special procedures in **D6724/D6724M** and **D6725/D6725M** address methods to place groundwater monitoring wells in small diameter direct push equipment with much smaller annulus. Generally, environmental sampling does not require physically intact samples where larger diameters are required. Direct push equipment has now reached capabilities with double tube system that exceed 100 mm [4 in.] inside diameters but often are used in smaller sizes.

5.6 Drilling – Damage by Poor Drilling Procedures – Hydraulic Fracturing:

5.6.1 If drilling methods are not properly performed, poor quality samples, borehole damage, or poor-quality monitoring-well installation(s) may result. It has been shown that improper drilling, particularly when drilling in unconsolidated materials (soils), can cause borehole damage. Preferential seepage paths can be formed close to the borehole by washing fine particles and creating “draining chimneys” that can be very difficult to seal (**22-24**). Drilling damages to the borehole usually are more severe in boreholes drilled in unconsolidated materials than those occurring in boreholes drilled in consolidated materials (rock). Although documentation of these occurrences is rare, it does occur. Occurrences of this nature are probably due to poor drilling-fluid control, poor drilling practice by an inexperienced driller. Damage can occur by drilling too hastily, and by use of incorrect speeds, pressures, and other variables controlled by the driller. Any drilling method using a circulating media to control cuttings removal can cause hydraulic fractur-

ing of the drilled materials if too high of drilling rate or circulation pressure is applied.

5.6.2 Hydraulic Fracturing—Geotechnical drilling for water retaining hydraulic structures such as dams or levees should be carefully selected to avoid potential for hydraulic fracturing. Drilling methods using fluids or air have potential to hydraulically fracture soils if poor drilling practice or the formation leads to circulation blockage. For water retaining structures dry drilling methods such as hollow-stem augers or sonic drilling are preferred and fluid and especially air drilling are to be avoided. Air drilling has been banned in impervious cores of dams (**25**).

5.7 Drilling Methods – Fluid/Water Drilling:

5.7.1 Fluid/water drilling methods are commonly used for geotechnical boreholes and are often preferred for these drilling programs. Conversely, fluid drilling is typically avoided when possible for environmental borings and monitoring well installations. Drilling fluids can significantly impact the water quality of the test or installation location causing bias in basic water quality parameters such as specific conductance, dissolved oxygen, pH and ORP conditions. Accurate determination of these parameters can be vital to understanding the contaminant degradation processes occurring in the aquifer and to designing an effective remediation program. Additionally, drilling fluids can dilute the observed concentration of hazardous contaminants present at the facility or accidentally add contaminants to the formation exacerbating the existing problem. The use of drilling fluids should be avoided for environmental borings when possible.

5.7.2 Water without additives is not effective as a drilling fluid for two reasons, first, it does not have any cuttings-carrying capacity, having a Test Method **D6910/D6910M** Marsh-funnel viscosity of only 26 s, and secondly, it does not possess any gel-strength properties for building a mud rind on the borehole wall, allowing for borehole wall collapse, differential sticking of the drill tools to the borehole wall, and creation of “draining chimneys” due to fluid invasion and internal erosion of the borehole wall (**26**). Also, water containing only natural clays should not be used as a drilling mud. This fluid mixture, containing only natural clays and water, will make only a heavy, clay-laden fluid that will not have the capacity (viscosity) to carry the drill cuttings up-hole and will not make a thin mud rind on the borehole wall to inhibit its collapse (lack of gel strength). Instead, it will allow washouts of the borehole wall, fluid and clay penetration into the borehole wall, and perhaps, cause differential sticking and loss of the drill tools in the borehole. Channeling and chimneys of sand also can result in the borehole wall allowing preferential seepage paths close to the borehole.

5.7.3 When using a drilling method that requires use of a drilling fluid, it is recommended that a controlled drilling-fluid program be employed in order to minimize possible drilling-fluid invasion effects on the borehole and cores obtained (**26**). Auger drilling tends to smear fine-grained sediment cuttings onto the borehole wall during the rotation of the auger flights. Cable-tool drilling can cause borehole damage by the cyclic upward and downward surging motion of the drill bit, which can force fine-grained sediment into the borehole wall. Soil

compaction resulting from driving the casing also can occur in a cable-tool drilled borehole. Although reverse-circulation drilling commonly is considered a clean drilling method, invasion of fine-grained sediment into the borehole wall can occur because of the high positive hydrostatic head that must be maintained in the borehole during drilling. Also, if drilling mud or other additives are used in the reverse-circulation drilling method, borehole damage can occur. Air-rotary drilling methods also may damage the borehole by introducing air into the drilled materials or fracturing of the borehole wall if drilling air pressures are not closely monitored and are allowed to exceed the downhole pressure necessary to adequately keep the borehole free of cuttings.

5.8 *Drilling Methods – Air Drilling:*

5.8.1 When air-rotary drilling, downhole air pressures should be maintained and documented carefully. Uphole (return) air pressure(s) should be adequate to maintain cuttings removal from the borehole but not excessive enough to cause hydraulic fracturing of the materials being drilled. Such practice can result in a damaged borehole wall and the inability to form a proper seal between casing and the borehole wall in the completed installation. Borehole contamination, such as those discussed in Sterrett and Shuter can occur with air drilling (20, 21). When exploring for volatile organic contamination during an environmental assessment air-rotary drilling can result in loss of analytes from the borehole and surrounding formation. The use of air rotary drilling can significantly impact water quality parameters such as dissolved oxygen and ORP potential as well as change the redox state of sensitive dissolved metals and metal complexes. This can make the determination of ambient aquifer geochemistry conditions difficult or impossible. Accurate measurement of these parameters and dissolved species can be critical for understanding contaminant degradation and development of an effective remediation program at environmental sites.

5.9 *Geophysical Logging of Boreholes and Borehole Condition Evaluations:*

5.9.1 The purpose of the drilling may be for geophysical logging, or, the condition of the borehole can be evaluated using geophysical logging. The proposed geophysical logging may require a certain drilling method. For example, suspension logging requires a drill fluid filled borehole. Geophysical logging is often performed in rock core holes for better determination of rock mass properties.

5.9.2 Borehole-geophysical methods, such as fluid temperature and resistivity, natural gamma, gamma-gamma, neutron, sonic-velocity logging, caliper logging, and borehole televiewer logs (fracture logging), are useful to confirm specific subsurface geologic conditions. Borehole television logs allow a visual study of existing borehole-wall conditions, as well as viewing casing conditions in a cased borehole. Acoustic borehole televiewer logs can exhibit fracturing in the borehole. The orientation of the fractures, as well as the extent of fracture occurrence, can be determined using acoustic televiewer logs. Natural gamma logs, when used in conjunction with original driller's logs, are useful particularly for determining lithology in existing cased wells. Guide D5753 and the following references provide additional information on use of geophysi-

cal logging techniques (14, 24, 27-30). All of these data can play an important part in selecting a drilling method that can provide the best samples and most successful monitoring-well installation under the ambient hydrogeologic field conditions.

5.10 Some methods that can be used to assess the hydraulic integrity of the borehole or a subsequent installation include the following.

5.10.1 *Indirect Method(s):*

5.10.1.1 Selected borehole geophysical logging methods (27, 31, 32).

5.10.1.2 Introduction of tracer(s) to the borehole combined with pumping tests (8, 33, Note 2).

5.10.2 *Direct Method(s) (22, 23):*

5.10.2.1 Pumping test(s) of the borehole (D4044/D4044M).

5.10.2.2 Injection test(s) of the borehole (D4050).

5.10.2.3 Inflatable-packer testing of the borehole (D4630).

5.11 The drilling/push boring method selected must be practical logistically, and to the extent possible, minimize mechanical damage to the borehole. Additionally, for environmental explorations the drilling/push boring method should have minimal impact to the chemical conditions in the borehole and surrounding formation to assure that representative samples can be obtained. Local availability of a particular type of drilling rig/equipment also will be an extremely important factor to be considered before a drilling method can be selected. For instance, the availability of cable-tool rigs might be totally out of the question in some parts of the country where primarily rotary-type drilling methods are most prevalent because of the type(s) of drilling conditions in those areas. In addition, hydrogeologic parameters might be required for the investigation and can be obtained possibly by means of sampling during drilling or subsequent borehole-geophysical logging, or a combination of both methods. Final selection of a drilling method, therefore, should be made only after due consideration of all project objectives (28).

5.12 *Borehole Installation Sealing or Sealing for Abandonments:*

5.12.1 *Annular Sealants*—Guidelines for sealing Geotechnical boreholes were recommended by Luttnegger and DeGroot (34). This report gives recommendations for both bentonite and cement grouts and use of bentonite pellets or chips. The materials used to seal the annulus may be prepared as a slurry or used un-mixed in a dry pellet, granular, or chip form. Sealants should be selected to be compatible with ambient geologic, hydrogeologic, geochemical and climatic conditions and any man-induced conditions. Regional or local regulation may specify required sealing methods for drill holes that intersect groundwater.

5.12.2 Certain backfilling and sealing operations are required for Groundwater monitoring wells and details can be found in ASTM D5092/D5092M. Research on sealing of riser pipes on conventional drinking water wells shows some leakage can be anticipated in the vadose zone for most conventional sealing methods (Note 2).

5.12.3 Sealing methods for direct push operations are discussed in D6001, D6282/D6282M, D6724/D6724M, and D6725/D6725M. Sealing methods are also addressed in the

individual drilling/push boring standards for the respective methods listed in [Table 1](#) and the discussions below.

5.12.4 *Cement Grout*—In high sulfate groundwater conditions (>0.5%) sulfate resistant Type II cement must be used. In critical cases where shrinkage is a concern with cement grouts, additives such as aluminum oxide or use of Type K cement can be used to give slightly expansive properties to the grout. Cement based grout has been shown to shrink away from PVC casing in the unsaturated zone ([35](#), [36](#)).

NOTE 2—An extensive research program on annular sealants for conventional water well installations have been conducted from 2001 through 2009 and subsequent years by the Nebraska Grout Task Force ([35](#), [36](#)). This research included cement and bentonite grouts and also use of pellets and chips. The general findings of the study indicate all sealing methods suffer from some shrinkage in the portion of the well in the un-saturated zone. The best grouts were cement-sand, bentonite chips, neat cements, and bentonite slurries with more than 20% solids. Especially problematic is the use of low solids content bentonite slurries leading to a ban on their use in California ([37](#)).

6. Auger-Drilling Methods

6.1 Auger-drilling methods include using hollow-stem continuous-flight augers, solid-stem continuous-flights augers, bucket augers, and hand-augers. All auger-drilling methods are limited usually to drilling in unconsolidated soils or weathered rock. Auger-drilling methods normally do not require the use of a drilling fluid during the drilling process; however, in cases where water-bearing sands or silts are drilled, the addition of water or drilling mud to the hollow-auger column may be necessary to inhibit the “blow in” of these fluid-like materials into the augers (see [Guide D5784](#) and [Practice D6151/D6151M](#)). The borehole is advanced by pushing the initial auger-column assembly below ground surface and initiating a low-velocity rotation to the auger flights or bucket-auger assembly. The lead auger section is equipped with a removable cutting head. The bucket auger, on the other hand, has hard-surfacing material around the bottom cutting edge of the bucket. As drilling progresses, auger flights or kelly rods, in the case of a bucket auger, are added to the drill stem until the desired depth is reached. The continuous auger flights carry drill cuttings to the surface.

6.1.1 Mechanical solid stem auger drilling and bucket auger drilling are often used as rapid screening tools of sites with large surface areas, like borrow areas, to collect disturbed samples and determine locations for more advanced drilling and field testing. The continuous auger flights carry drill cuttings to the surface and can be sorted by lithology and classified ([D2488](#)).

6.1.2 At most environmental sites hazardous contaminants are present in the subsurface. Because of this fact, any drill cuttings or drilling fluids returned to the surface should be properly handled, contained and stored (drums or roll-off bins, etc.) for sampling and laboratory analysis as required in the work plan. ([4.5.2.1](#)).

6.2 *Hollow-Stem Auger Drilling*—The hollow-stem continuous-flight auger drilling method is a continuous soil sampling system, which can be used for the installation of monitoring wells (see [Practice D6151/D6151M](#)). [Fig. 2](#) shows a typical hollow-stem auger system with the continuous

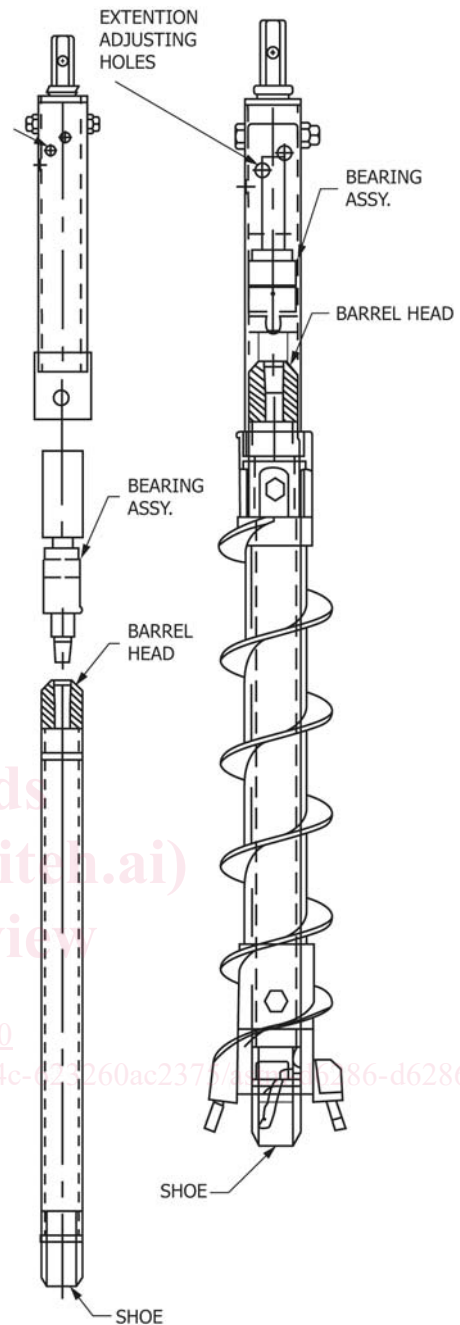


FIG. 2 Hollow-Stem Auger drilling system showing the continuous soil sample barrel (Diedrich Drill)

sampling barrel. The sampling barrel can be replaced with a pilot bit if no sample is required. Hollow-stem augers are used as a platform for many other testing, sampling and installation applications. Using special cutting shoes and liners intact soil cores of 75 to 125 mm [3 to 5 in.] OD can be retrieved for geotechnical laboratory testing which is important if soils need to be sampled in dry conditions. The hollow auger flights serve as a temporary casing for monitoring well installation, which prevents caving and sloughing of the borehole wall while the monitoring-well casing is installed through the hollow auger (see [Guide D5784](#)). The hollow-stem auger-drilling method also allows for the utilization of the hollow-stem auger column

as a casing for subsequent drilling activities in soils or rock (see Practice [D2113](#)). Borehole diameters up to about 500 mm [20-in.] can be drilled using hollow-stem augers. A monitoring-well casing can be installed through the hollow stem auger (auger inside diameter up to 300 mm [12 in.] available for insertion of casing or other instrumentation) once drilling is complete and prior to removing the augers from the borehole.

6.2.1 Continuous soil coring using hollow-stem augers is recommended for Environmental site characterization where detailed lithology is required for hydrogeological data and monitoring. Continuous cores can be obtained rapidly using the split barrel liner system in long runs. Continuous hollow-stem soil-coring equipment consists of a rotating outer hollow-stem auger with a crown cutter-head bit at the bottom and a non-rotating inner sample barrel equipped with a smooth cutting shoe at the bottom (see Practice [D6151/D6151M](#)). The lead and clearance ratio of the cutting shoe can be adjusted to improve sample quality.

6.2.2 Physically “intact” soil samples ([D6169/D6169M](#)) for geotechnical applications can be obtained using larger diameter equipment where the inner barrel can be equipped with clear plastic liners for laboratory testing (see 6.5.4.1 of [D6151/D6151M](#)). Intact soil sampling requires that special modifications to the auger equipment must be done to optimize the cutting shoes and clearance ratios of inside liners.

6.2.3 Other soil sampling, using a split-barrel sampler, ring-lined barrel sampler (see Practice [D3550/D3550M](#)), or thin-walled tube sampler (see Practice [D1587/D1587M](#)), is accomplished during drilling by using a continuous sampler in the hollow-stem that advances with the auger flight or by a pause in drilling, driving, or pushing the sampler into the undisturbed material beyond the cutting head, and retrieving the sample before resuming drilling (see Test Method [D1586/D1586M](#) and Practice [D1587/D1587M](#)).

6.2.4 Geotechnical in-situ tests are readily performed using these augers and groundwater samples can be obtained during drilling using a screened hollow-stem auger section. Direct-push methods also can be used in advance of the lead auger during drilling pauses to collect either fluid or soil samples or both.

6.2.5 Advantages:

6.2.5.1 Normally, precludes use of drilling fluids.

6.2.5.2 Auger drilling does not require the use of lubricants.

6.2.5.3 Rapid continuous soil sampling possible during drilling using continuous sampler.

6.2.5.4 Continuous samples of groundwater can be collected during drilling, using screened auger flight(s).

6.2.5.5 The hollow-stem auger column can be used for in situ testing during drilling and subsequent drilling installations in soils or rock materials (see Practice [D2113](#)).

6.2.5.6 Auger-drilling equipment is relatively mobile.

6.2.5.7 Drilling is moderately fast.

6.2.5.8 Large diameter intact samples can be taken using dry methods for geotechnical laboratory testing. These samples are normally encased in thick clear polycarbonate liners which allow for inspection of sample quality onsite and easy selection of lab test specimens.

6.2.6 Disadvantages:

6.2.6.1 Pressure equalization of water-bearing sands or silts and “blow in” of these fluid-like materials into the hollow-stem auger column can be a problem requiring use of fluid in the hollow auger to equalize the pressure head and keep the intrusive fluid-like materials from entering the hollow auger.

6.2.6.2 Borehole wall can be smeared by previously-drilled clay.

6.2.6.3 Gravel pack and grout seal may be difficult to install.

6.2.6.4 Borings limited to relatively shallow depths in normal soils and soft rock.

6.2.6.5 Difficult drilling in extremely hard dry, fine materials, for example, playa-lake or Caliche deposits.

6.2.6.6 Hollow-stem auger drilling difficult in saturated sandy soils ([D1586/D1586M](#)) and soils containing very coarse gravels, cobbles, or boulders.

6.2.6.7 Hollow-stem auger does mechanically affect formation intrinsic permeability due to smear at the edge of the auger flights.

6.2.6.8 During environmental investigations generated waste drill cuttings may be contaminated with hazardous chemicals and may need to be properly contained, sampled and analyzed before disposal. Generation of contaminated drill cuttings also increases the potential for worker exposure to hazardous chemicals.

6.3 *Solid-Stem Auger Drilling* ([D1452/D1452M](#))—Solid-stem continuous-flight auger drilling is a rapid and effective screening method for obtaining disturbed soil samples from the flight cuttings, generally in softer unsaturated soils. High power equipment can penetrate harder formations, but it is important not to classify processed cuttings as non-lithified materials. Solid-stem auger drilling is accomplished by pushing the auger-column assembly below the ground surface and initiating a low-velocity rotation. As drilling progresses additional auger flights are added to the auger-assembly column. The continuous auger flights carry drill cuttings to the surface. Disturbed soil samples can be obtained during drilling as augered cuttings return and cutting can be sorted by lithology for classification ([D2488](#)). Alternately, for more accurate logging, the augers may be screwed into the soil with minimal cuttings return and then retracted with soil intact on the flights in increments. Samples on the flights can then be taken from different elevations. If the borehole remains open after removing the auger-column assembly, a monitoring well can be installed in the open borehole. The solid-stem augers drilling method often is a less-effective method to be used for installing a monitoring well than the hollow-stem augers drilling method because the solid-stem augers cannot be used as temporary casing to prevent caving and sloughing of the borehole wall and placement of filter and seal materials is difficult with minimal clearances. Under saturated conditions, for example, below the water table, solid-stem auger drilled boreholes usually collapse immediately upon auger removal. In some instances, if the soil(s) drilled using the solid-stem augers contain a relatively high amount of cohesive (clay rich) materials, such as, clayey silts, silts, etc., the borehole will remain completely open for the entire auger-drilled depth after auger removal, making it very easy to install the monitoring-well casing/instrumentation to the bottom of the borehole.