This document is not an ASTM standard and is intended only to provide the user of an ASTM standard an indication of what changes have been made to the previous version. Because it may not be technically possible to adequately depict all changes accurately, ASTM recommends that users consult prior editions as appropriate. In all cases only the current version of the standard as published by ASTM is to be considered the official document.



Designation: D5811 - 08 (Reapproved 2013) D5811 - 20

# Standard Test Method for Strontium-90 in Water<sup>1</sup>

This standard is issued under the fixed designation D5811; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reapproval.

### 1. Scope

1.1 This test method covers the determination of radioactive  ${}^{90}$ Sr in environmental water samples (for example, non-process and effluent waters) in the range of 0.037 Bq/L (1.0 pCi/L) or greater.

1.2 The values stated in SI units are to be regarded as the standard. The values given in parentheses are for information only.

1.2 This test method has been used successfully with tap water. It is the <u>user'suser's</u> responsibility to ensure the validity of this test method for samples larger than 1 L and for waters of untested matrices.

1.3 The values stated in SI units are to be regarded as standard. No other units of measurement are included in this standard.

1.4 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety safety, health, and healthenvironmental practices and determine the applicability of regulatory limitations prior to use. For specific hazard statements, see Section 9.

<u>1.5 This international standard was developed in accordance with internationally recognized principles on standardization established in the Decision on Principles for the Development of International Standards, Guides and Recommendations issued by the World Trade Organization Technical Barriers to Trade (TBT) Committee.</u>

### 2. Referenced Documents

2.1 ASTM Standards:<sup>2</sup>

D1129 Terminology Relating to Water

D1193 Specification for Reagent Water Document Preview

D1890 Test Method for Beta Particle Radioactivity of Water

D2777 Practice for Determination of Precision and Bias of Applicable Test Methods of Committee D19 on Water

D3370 Practices for Sampling Water from Flowing Process Streams 2(

D3648 Practices for the Measurement of Radioactivity D4448 Guide for Sampling Ground-Water Monitoring Wells

D5673 Test Method for Elements in Water by Inductively Coupled Plasma—Mass Spectrometry

D5847 Practice for Writing Quality Control Specifications for Standard Test Methods for Water Analysis

D6001 Guide for Direct-Push Groundwater Sampling for Environmental Site Characterization

D7282 Practice for Set-up, Calibration, and Quality Control of Instruments Used for Radioactivity Measurements

D7902 Terminology for Radiochemical Analyses

2.2 Other Documents:

ANSI N42.22 Traceability of Radioactive Sources to the National Institute of Standards and Technology (NIST) and Associated Instrument Quality Control<sup>3</sup>

BIPM-5 Decay Data Evaluation Project (DDEP)<sup>4</sup>

<sup>4</sup> Available from BIPM, Sèvres Cedex, France, https://www.bipm.org.

NUDAT2<sup>5</sup>

<sup>&</sup>lt;sup>1</sup> This test method is under the jurisdiction of ASTM Committee D19 on Water and is the direct responsibility of Subcommittee D19.04 on Methods of Radiochemical Analysis.

Current edition approved June 15, 2013May 1, 2020. Published July 2013June 2020. Originally approved in 1995. Last previous edition approved in 20082013 as D5811-08: D5811-08 (2013). DOI: 10.1520/D5811-08R13.10.1520/D5811-20.

<sup>&</sup>lt;sup>2</sup> For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For Annual Book of ASTM Standards volume information, refer to the standard's standard's Document Summary page on the ASTM website.

<sup>&</sup>lt;sup>3</sup> Available from Institute of Electrical and Electronics Engineers, Inc. (IEEE), 445 Hoes Ln., Piscataway, NJ 08854-4141, http://www.ieee.org.

<sup>&</sup>lt;sup>5</sup> Available from National Nuclear Data Center at Brookhaven National Laboratory, W Princeton Ave, Yaphank, NY 11980, http://www.nndc.bnl.gov.

### 3. Terminology

3.1 Definitions—Definitions: For definitions of terms used in this test method, refer to Terminology D1129.

3.1.1 For definitions of terms used in this standard, refer to Terminology D1129.

3.1.2 For definitions of terms used in this standard relating to radiochemical analysis, refer to Terminology D7902.

### 4. Summary of Test Method

4.1 This test method is based on the utilization of solid phase extraction of strontium from water samples with detection of the radioactive strontium by gross beta gas proportional counting.

4.2 An aliquant of the sample is measured into a beaker, strontium carrier added, digested with nitric acid, sorbed on an ion exchange column, eluted, evaporated to dryness, dissolved in nitric acid (8M), (8 M), selectively sorbed on a solid phase extraction column, eluted with dilute nitric acid, dried on a planchet, and planchet. The sample test source (STS) is counted for beta radiation.

4.3 Fig. 1 shows a flow diagram for this test method.

### 5. Significance and Use

5.1 This test method was developed to measure the concentration of  $^{90}$ Sr in non-process water samples. This test method may be used to determine the concentration of  $^{90}$ Sr in environmental samples.

### 6. Interferences

6.1 Significant amounts of stable strontium present innative to the sample will interfere with the yield determination. If it-natural strontium is to be present in the sample at levels that will compromise the determination of the chemical yield, blankanalyze sample aliquots to which no strontium carrier is added shall be analyzed has been added to determine the natural strontium content. The Alternatively, the elemental strontium concentration may be determined using an appropriate method such as ICP-MS, Test Method D5673. Account for the amount of natural strontium contained in the sample shall be reflected when calculating the chemical yield correction factor.

6.2 Strontium-89 present in the sample will cause a high bias in proportion to the  $^{89}$ Sr/ $^{90}$ Sr ratio. This technique is not applicable when it is suspected or known that  $^{89}$ Sr is present in the sample.

6.3 Strontium nitrate  $(Sr(NO_3)_2)$  is hygroscopic. This chemical property may add uncertainty in the gravimetric yield determination. determination of the chemical yield.

### 7. Apparatus

7.1 Analytical Balance, 0.0001 g.

7.2 Low Background Gas Proportional Beta Counting System.

7.3 Ion Exchange Columns, 10 mL resin capacity, glass or acid-resistant plastic. An attached reservoir of at least 50 mL is desirable.

7.4 *Planchets*, stainless steel to match calibration source.<sup>6</sup>

### 8. Reagents and Materials

8.1 *Purity of Reagents*—Reagent grade chemicals shall be used in all tests. Unless otherwise indicated, it is intended that all reagents shall conform to specifications of the Committee on Analytical Reagents of the American Chemical Society.<sup>7</sup> Other grades may be used, provided it is first ascertained that the reagent is of sufficiently high purity to permit its use without lessening the accuracy of the determination. Reagent blanks shall be run with all determinations.Some reagents, even those of high purity, may contain naturally-occurring radioactivity, such as isotopes of uranium, radium, actinium, thorium, rare earths, potassium compounds, or artificially produced radionuclides, or combinations thereof. Consequently, when such reagents are used in the analysis of low-radioactivity samples, the activity of the reagents should be determined under analytical conditions that are as close as practicable to those used for the test sample. The activity contributed by the reagents should be accounted for and applied as a correction when calculating the test sample result.

8.2 *Purity of Water*—Unless otherwise indicated, reference to water shall be understood to mean reagent water conforming to Specification D1193, Type III.

8.3 Cation Exchange Resin, 100 to 200 mesh, hydrogen form. 8%-8 % cross linked, analytical grade.

<sup>&</sup>lt;sup>6</sup> Stainless steel planchets available commercially have been found satisfactory.

<sup>&</sup>lt;sup>7</sup> Reagent Chemicals, American Chemical Society Specifications, ACS Reagent Chemicals, Specifications and Procedures for Reagents and Standard-Grade Reference Materials, American Chemical Society, Washington, DC. For Suggestions on the testing of reagents not listed by the American Chemical Society, see AnnualAnalar Standards for Laboratory Chemicals, BDH Ltd., Poole, Dorset, U.K., and the United States Pharmacopeia and National Formulary, U.S. Pharmacopeial Convention, Inc. (USPC), Rockville, MD.

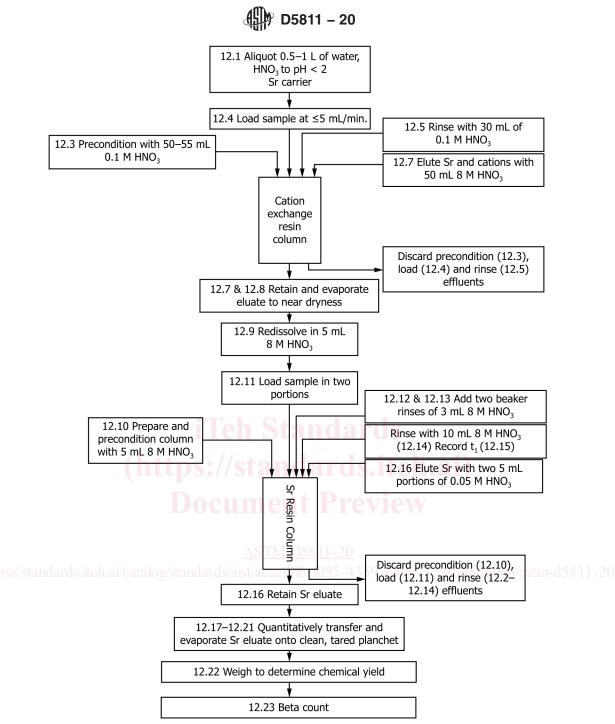


FIG. 1 Flow Diagram for the Procedure

8.4 Nitric Acid (sp gr 1.42)—Concentrated HNO<sub>3</sub>.

8.5 Nitric Acid (8M-(8 M HNO3)-Add 500 mL of concentrated HNO3 to 400 mL of water. Dilute to 11-1 L with water.

8.6 Nitric Acid (0.1 HNO<sub>3</sub>)-Add 6.4 mL of concentrated HNO<sub>3</sub> to 600 mL of water. Dilute to H-1 L with water.

8.7 Nitric Acid (0.05 M HNO<sub>3</sub>)—Add 3.2 mL of concentrated HNO<sub>3</sub> to 600 mL of water. Dilute to H-1 L with water.

8.8 *Strontium Carrier* (10 g/L)—Preferably use 10 000  $\mu$ g/mL ICP standard. Alternatively, dissolve 24.16 g <u>dry</u> strontium nitrate (Sr(NO<sub>3</sub>)<sub>2</sub>) in water, add 20 mL concentrated nitric acid, and dilute with water to 1 L. Use the following procedure to standardize the prepared strontium carrier: Carefully pipet a 5.0 mL portion of the strontium carrier solution onto a clean, dried, and tared planchet. Dry the planchet under the same conditions used for the final evaporation in 12.20. Allow the planchet to cool to room temperature and reweigh the planchet to the nearest 0.0001 g. Divide the net weight by 10. This result is the amount of strontium

## ∰ D5811 – 20

nitrate actually added. Use an average of three values in the denominator of the recovery chemical yield equation in 11.12 and 13.1. This value should be within 3 % of 12.08 mg/0.5 mL.

8.9 Strontium Extraction Chromatography Column, 2 mL bed volume consisting of an octanol solution of  $4,4^{2}(5^{2})$ -bis (t-butyl-cyclohexano)-18-crown-6-sorbed 4,4'(5')-bis (t-butyl-cyclohexano)-18-crown-6 sorbed on an inert polymeric support.<sup>8</sup>

8.10 Strontium-90 Standardizing Solution—Traceable to a national standard body such as National Institute of Standards and Technology or National Physical Laboratory solution with less than 0.1 mg of stable strontium per mL of final solution with a typical concentration range from 85 to 125 Bq/mL.Solution with a final concentration typically ranging from 85 to 125 Bq/mL and less than 0.1 mg of stable strontium, traceable to the SI through a national metrology institute (NMI), such as National Institute of Standards and Technology (NIST).

### 9. Hazards

9.1 Use extreme caution when handling all acids. They are extremely corrosive and skin contact could result in severe burns.

9.2 When diluting concentrated acids, always use safety glasses and protective clothing, and add the acid to the water.

### 10. Sampling

10.1 Collect a sample in accordance with Practice Practices D3370, Guide D4448, and Guide D6001, or other documented procedure.

### 11. Calibration

11.1 Calibrate the low background gas proportional beta counting system in accordance with Practice D7282-, Sections 14, 15, and 16. Prepare a set of three working calibration samples standards (WCS) according to the calibration procedure outlined in the subsequent steps.

11.2 Pipet 0.5 mL of strontium carrier into a small beaker.

11.3 Add 1 mL of traceable <sup>90</sup>Sr solution and evaporate to near dryness on a hot plate.

11.4 Redissolve the residual in 5 mL of 8M-8 M nitric acid.

11.5 Follow the steps described in 12.10 through 12.23.

11.6 Count to accumulate 10 000 net counts in the counting period. Counting should be completed within 3 h of column elution. Record the time and date of the midpoint of this counting period as  $t_2$ . Count each sample mount WCS twice, once for this step having a counting date designated as  $t_2$  and a second time as specified below.

11.7 Calculate the net count rate of the count <u>WCS</u> at time  $t_2(R_{n(2)})$  by subtracting the instrument background count rate from the gross count rate.

11.8 Store the calibration mount WCS for at least 7 days to allow for <sup>90</sup>Y ingrowth. <sup>644b98db0a8/astm-d5811-20</sup>

11.9 Recount the calibration mount <u>WCS</u> to amass 10 000 counts in a counting period. Record the time and date of the midpoint of this count period as  $t_3$ .

11.10 Calculate the net count rate of the second count at time  $t_3(R_{n(3)})$  by subtracting the instrument background count rate from the gross count rate.

11.11 Calculate the <sup>90</sup>Sr detection efficiency,  $\varepsilon_{Sr}$ , and the <sup>90</sup>Y detection efficiency,  $\varepsilon_Y$ , for each <del>calibration mount WCS</del> using the equations presented below. Calculate the mean and standard deviation of the three  $\varepsilon_{Sr}$  and  $\varepsilon_Y$  values. Use the relative standard deviation of these parameters to estimate the relative uncertainty of the ingrowth efficiency factor, (defined in Eq 5),  $u_r(\varepsilon_1)$  and used in Eq 7.

11.12 *Efficiency Calculations*—<sup>90</sup>Sr detection efficiency  $\varepsilon_{Sr}$ :

$$\frac{\left(R_{n(2)} \times IF_{3}\right) - \left(R_{n(3)} \times IF_{2}\right)}{Y_{ss} \times A_{star} \times (IF_{s} - IF_{s})}$$
(1)

$$S_{\rm Sr} = \frac{\left(R_{\rm n(2)} \times IF_3\right) - \left(R_{\rm n(3)} \times IF_2\right)}{Y_{\rm Sr} \times A_{\rm C(2)} \times (IF_3 - IF_2)} \tag{1}$$

<sup>90</sup>Y detection efficiency  $\varepsilon_{\rm Y}$ :

$$\varepsilon_{\rm Y} = \frac{R_{n(3)} - R_{n(2)}}{Y_{\rm NC} \times A_{C(2)} \times (IF_3 - IF_2)} \tag{2}$$

<sup>&</sup>lt;sup>8</sup> The sole source of supply of the apparatus known to the committee at this time is Sr Resin available from Eichrom Technologies, Inc. If you are aware of alternative suppliers, please provide this information to ASTM International Headquarters. Your comments will receive careful consideration at a meeting of the responsible technical eommittee, Sr resin available commercially have been found satisfactory.<sup>1</sup>-which you may attend.

יוושי	
$R_{\rm n(3)} - R_{\rm n(2)}$	
$\varepsilon_{\rm Y} = \frac{1}{Y_{\rm Sr} \times A_{\rm C(2)} \times (IF_3 - IF_2)}$	

(2)

where:

- = activity of  ${}^{90}$ Sr in becquerels (Bq) at the time of the first count of the calibration mount,  $A_{C(2)}$
- = ingrowth factor for  ${}^{90}$ Y at the midpoint of the count at time  $t_2$ ,  $e^{-[\lambda_1 \times (t_2 t_1)]}$  $HF_2$
- $IF_2$
- = ingrowth factor for <sup>90</sup>Y at the midpoint of the count at time  $t_3$ ,  $e^{-[\lambda_4 \times (t_3 t_4)]}$  $H_{\overline{3}}$
- $\equiv$  ingrowth factor for <sup>90</sup>Y at the midpoint of the count at time  $t_3$ ,  $t = e^{-\lambda_y(t_3 t_1)}$ ,  $IF_3$
- $= \frac{\text{decay constant for } {}^{90}\text{Y} (0.2600 \text{ d}^{-1})^{9}}{\text{decay constant for } {}^{90}\text{Y} (0.2599 \text{ d}^{-1})^{9}}$  $\lambda_{\rm Y}$
- $\lambda_{\mathbf{Y}}$
- = net count rate of the calibration test source at the midpoint of the first count, in counts per second,  $R_{n(2)}$
- = net count rate of calibration test source at the midpoint of the second count, in counts per second, = date and time of  ${}^{90}$ Y separation,  $R_{n(3)}$
- $t_1$
- = date and time of midpoint of first count,  $t_2$
- = date and time of midpoint of second count.  $t_3$
- $Y_{\rm Sr}$ = fractional chemical yield of strontium carrier (see Eq 4).

Note 1—The time differences  $(t_2 - t_1)$  and  $(t_3 - t_1)$  are expressed in days.

### 12. Procedure

12.1 Add 0.5 mL of strontium carrier to a maximum of 1 L of sample. Add 1 mL of 8M-8 M HNO<sub>3</sub> per 100 mL of sample and mix. Bring sample to a boil for 30 min and then cool.

🕮 D5811 – 20

12.2 Prepare a cation exchange column containing 10 mL of cation exchange resin.

12.3 Precondition the column by passing 50 to 55 mL of 0.1M-0.1 M HNO<sub>3</sub> through the column.

12.4 Pass the sample through the column at a rate of not more than 5 mL/min.

12.5 Rinse the column with 25 to 30 mL of 0.1 M HNO3. UZTUS

12.6 Properly dispose of the feed and rinse.

12.7 Elute the strontium (and other cations) with 50 mL of 8M-8 M HNO<sub>3</sub> into a 150 mL beaker.

12.8 Evaporate the eluate to near dryness on a hot plate in a fume hood. The residue will dissolve more easily in the next step if the evaporation is stopped just as the sample starts to go dry.

12.9 Dissolve the saltsresidues in 5 mL of 8M-8 M HNO<sub>3</sub>. If necessary, cover with a watchglass and heat gently to facilitate complete dissolution.

12.10 Prepare a strontium extraction chromatography column by removing the bottom plug and the cap. Press the top frit down snugly to the resin surface using a glass rod (or equivalent) and let the water drain out. Add 5 mL of HNO<sub>3</sub> (8M) (8 M) and let the solution drain by gravity.

12.11 Carefully transfer the sample solution to the reservoir of the column. Add half and let the solution drain before adding the second half.

12.12 Rinse the beaker with 3 mL of 8M-8 M HNO<sub>3</sub> and add to the column after the feed has passed through.

12.13 Repeat step-12.12.

12.14 Rinse the column with 10 mL of 8M-8 M HNO3.

12.15 Record the end time of the last rinse as the time of  ${}^{90}$ Y separation (start of  ${}^{90}$ Y ingrowth,  $t_1$ ).

12.16 Elute the strontium with two 5 mL portions of 0.05 M HNO<sub>3</sub> into a suitable container (for example, a liquid scintillation counting vial or centrifuge tube).

12.17 Clean a planchet with a paper towel moistened with alcohol. Wipe the planchet and let it dry.

12.18 Weigh the planchet to the nearest 0.0001 g and record the weight.

12.19 Place the planchet under a heat lamp in a fume hood.

12.20 Evaporate the strontium eluate (see 12.16) onto the planchet by adding small portions (approximately 3 mL) to the planchet and allowing each portion to evaporate to near dryness between additions.

12.21 Rinse the liquid scintillation counting vial or centrifuge tube with approximately 3 mL of 0.05M-0.05 M HNO<sub>3</sub>, add to the planchet and evaporate.

<sup>&</sup>lt;sup>9</sup> Firestone, R. B., and Shirley, V. S., Table of Isotopes (Eighth Edition), John Wiley and Sons, Inc., New York, 1995. See BIPM-5. Other sources of nuclear data (such as NUDAT2) may be used at the user's discretion. Regardless of which reference is used, the source should be clearly documented.

12.22 After all the solution has dried, cool the STS planchet to room temperature and reweigh the planchet. Record the weightmass to the nearest 0.0001 g.

12.23 Beta count the sampleSTS as soon as possible after preparation on a low background gas proportional counting system. Count an empty planchet for an equal length of time to measure the instrument's fas a background subtraction sample for a duration that is as long or longer than associated STS to determine the instrument's beta background count rate. (See Test Method D1890 and Practices D3648.)

### 13. Calculation

13.1 Strontium-90 Radioactivity Concentration  $(AC_{SrSr})$ :

	$AC_{\rm Sr} = \frac{R_{\rm a} - R_{\rm b}}{\varepsilon_{\rm I} \times V_{\rm a} \times Y_{\rm Sr} \times e^{-[\lambda_{\rm sr} \times (t_{\rm i} - t_{\rm o})]}}$	(3)
	$AC_{\rm Sr} = \frac{R_{\rm a} - R_{\rm b}}{\varepsilon_{\rm I} \times V_{\rm a} \times Y_{\rm Sr} \times e^{-[\lambda_{\rm Sr} \times (t_{\rm I} - t_{\rm o})]}}$	(3)
	$Y_{\rm Sr} = \frac{m_{\rm a} - m_{\rm b}}{m_{\rm c}}$	(4)
	$\varepsilon_{\mathrm{I}} = \varepsilon_{\mathrm{Sr}} + \left(\varepsilon_{\mathrm{Y}} \times \left(1 - e^{-[\lambda_{\mathrm{Y}} \times (t_{\mathrm{m}} - t_{\mathrm{I}})]}\right)\right)$	(5)
	$\frac{1}{\varepsilon_{1}} = \varepsilon_{Sr} + (\varepsilon_{V} \times [1 - e^{-\lambda_{V} \times (t_{m} - t_{1})}])$	(5)
where:		

- $\epsilon_{Sr}$ = the mean of the values calculated using Eq 1,
- = the mean of the values calculated using Eq 2,  $\epsilon_{\rm Y}$
- = ingrowth efficiency factor,  $\epsilon_{I}$
- $\lambda_{Sr}$
- $= \frac{\text{decay constant for }^{90}\text{Sr} (6.594 \times 10^{-5} \text{ d}^{-1}),^9}{\text{decay constant for }^{90}\text{Sr} (6.592 \times 10^{-5} \text{ d}^{-1}),^9}$  $\underline{\lambda}_{Sr}$
- $= \frac{\text{decay constant for } {}^{90}\text{Y} (0.2595 \text{ d}^{-1}),^{9}}{\text{decay constant for } {}^{90}\text{Y} (0.2599 \text{ d}^{-1}),^{9}}$ =  $\frac{\text{decay constant for } {}^{90}\text{Y} (0.2599 \text{ d}^{-1}),^{9}}{\text{decay constant for } {}^{90}\text{Y} (0.2599 \text{ d}^{-1}),^{9}}$  $\lambda_{\rm Y}$  $\lambda_{\mathbf{Y}}$
- = count rate of sample aliquant, in counts per second,  $R_{\overline{a}}$
- $\underline{R}_{a}$ <u>= count rate of STS, in counts per second,</u>
- count rate of instrument background, in counts per second,  $R_{\rm b}$ =
- = count rate of background subtraction count, in counts per second,  $\underline{R}_{\rm b}$
- date and time of sample collection, date and time of  $^{90}$ Y separation, =  $t_0$
- =  $t_1$
- midpoint of count of sample aliquant (date and time), D5811-20  $t_{\rm m}$ =
- $\frac{t_{\rm m}}{V_{\rm a}}$ midpoint of count of STS (date and time), sist/acae/9/6-f055-4359-8b9b-7ea4b98db0a8/astm-d5811-20
- = volume of sample aliquant, in litres,
- $Y_{\rm Sr}$ = fractional chemical yield of strontium carrier,
- = mass of  $Sr(NO_3)_2$  for the sample aliquant,  $m_{\overline{a}}$
- = mass of Sr(NO<sub>3</sub>)<sub>2</sub> native to the sample aliquant,  $\underline{m}_{a}$
- = mass of  $Sr(NO_3)_2$  for the blank (where appropriate—see Step 6.1), and  $m_{\rm b}$
- = mass of Sr(NO<sub>3</sub>)<sub>2</sub> in the blank (where appropriate see Step 6.1), and  $\underline{m}_{\rm b}$
- = mass of  $Sr(NO_3)_2$  added as carrier.
- NOTE 2—The time differences  $(\underline{t}(t_1 t_0))$  and  $(\underline{t}(t_m t_1))$  are expressed in days.

13.2 The result of the measurement has an uncertainty due to counting statistics (counting uncertainty). The standard uncertainty of the <sup>90</sup>Sr radioactivity concentration in the sample due to counting statistics,  $u_{cC}(AC_{Sr})$ , is given by:

$$\frac{u_{cC}(AC_{sr}) = \frac{\sqrt{\frac{R_a + R_b}{t_a}}}{\varepsilon_t \times V_a \times Y_{sr} \times e^{-[\lambda_{sr} \times (t_t - t_0)]}} \tag{6}}{u_{cC}(AC_{sr}) = \frac{\sqrt{\frac{R_a}{t_a} + \frac{R_b}{t_b}}}{\varepsilon_t \times V_a \times Y_{sr} \times e^{-\lambda_{sr} \times (t_t - t_0)}} \tag{6}$$

where:

- = count duration, in seconds, of the sample aliquant.  $t_{\overline{a}}$
- count duration, in seconds, of the sample aliquant, and  $t_{\rm a}$ Ξ
- count duration, in seconds, of the background subtraction count.  $t_{\rm h}$ =
  - 13.3 Combined Standard Uncertainty:

D5811 - 20

	$u_{c}(AC_{Sr}) = \sqrt{u_{cC}^{2}(AC_{Sr}) + AC_{Sr}^{2} \times (u_{r}^{2}(\varepsilon_{t}) + u_{r}^{2}(V_{a}) + u_{r}^{2}(Y_{Sr}) + u_{r}^{2}(\dots))^{2}}$	(7)
	$u_{c}(AC_{Sr}) = \sqrt{u_{cc}^{2}(AC_{Sr}) + AC_{Sr}^{2}(u_{r}^{2}(\varepsilon_{1}) + u_{r}^{2}(V_{a}) + u_{r}^{2}(Y_{Sr}) + u_{r}^{2}())}$	(7)
where:		

- = combined standard uncertainty of the Sr-90 activity concentration (Bq/L) $u_{\rm c}(AC_{\rm Sr})$
- = relative standard uncertainty of the ingrowth efficiency factor,  $u_{\rm r}(\varepsilon_{\rm I})$
- = relative standard uncertainty of the ingrowth efficiency factor,  $u_{\rm r}(\varepsilon_{\rm I})$
- $u_{\rm r}(V_{\rm a})$ = relative standard uncertainty of the volume measurement,

 $u_{\rm r}(Y_{\rm Sr})$ = relative standard uncertainty of the chemical yield of the strontium carrier, and

 $u_{r}(...)$ = any additional relative uncertainty that has been determined or estimated, and

= any additional relative uncertainty that has been determined or estimated.  $\underline{u_{r}(...)}$ 

count duration, in seconds, of the background subtraction count. t<sub>b</sub>

13.4 "A Priori" Minimum Detectable Radioactivity Concentration (MDC):

$$MDC = \frac{3.29 \sqrt{R_b \times t_a \times \left(1 + \frac{t_a}{t_b}\right) + 2.71}}{t_a \times \varepsilon_T \times V_a \times Y_{Sr} \times e^{-[2_{SN} \times (t_r - t_0]]}}$$

$$MDC = \frac{2.71}{t_a} + 3.29 \sqrt{R_b \left(\frac{1}{t_a} + \frac{1}{t_a}\right)}}{\varepsilon_T V_a Y_{Sr} e^{-\lambda_{SI} t_1 - t_0}}$$
(8)

NOTE 3-Eq 8 is only valid for Type I and Type II error rates of 5 %. The formulation will need to be modified if data/measurement quality objectives specify different tolerable decision error rates.

13.5 Critical Level Concentration  $(L_c)$ :

$$L_{c} = \frac{1.645 \sqrt{R_{b} \times t_{a} \times \left(1 + \frac{t_{a}}{t_{b}}\right)}}{t_{a} \times \varepsilon_{I} \times V_{a} \times Y_{Sr} \times e^{-[\lambda_{sr} \times (t_{i} - t_{o})]}}$$
(9)  
$$L_{C} = \frac{1.645 \sqrt{R_{b} \left(\frac{1}{t_{a}} + \frac{1}{t_{b}}\right)}}{\varepsilon_{r} \cdot V_{a} \cdot Y_{Sr} \cdot e^{-\lambda_{Si}(t_{i} - t_{o})}}$$
(9)

NOTE 4—The k factor of 1.645 assumes a Type I error rate of 5 %. Factors corresponding to other error rates may be applied as appropriate depending of the data/measurement quality objectives.

### 14. Quality Control

14.1 In order to provide reasonable assurance that the analytical results obtained using this test method are valid and accurate within the confidence limits of the method, Quality Controlquality control (QC) samples are analyzed with each batch of samples undergoing analysis. Each batch should include not more than 20 samples, excluding those used for QC purposes. Laboratory or project quality assurance plans may contain more restrictive process QC requirements. The following minimum QC procedures must be followed when running the test method: method.

14.2 Internal Standard—Chemical Yield Carrier—As indicated in 12.1, an accurately added amount of Sr carrier is used as a tracer chemical yield monitor in the determination of the <sup>90</sup>Sr in the sample.

14.2.1 The chemical yield of the Sr carrier will be calculated for each sample and associated QC samples. This yield may should be reported along with the reported analytical data.

14.3 Calibration and Calibration Verification:

14.3.1 Standards used in the method shall be traceable to a national standards laboratory (such as NIST or NPL). an NMI. Standards obtained from ANSI N42.22 reference material providers meet this requirement. In-house produced carrier solutions shall be standardized prior to use.

14.3.2 The detector counting efficiency should be determined using at least three standards standards as described in Section 11 and Practice D7282, Sections 14, 15, and 16.

14.3.3 The Verify the detector efficiency shall be verified monthly or prior to use, whichever is longer. prior to use as described in Practice D7282, Section 16..

14.3.4 Acceptance limits for the verification standard are 90-110 % of the known value. If the results for the verification standard are outside the limits, recalibrate and reanalyze samples back to the last acceptable verification standard.

14.4 Initial Demonstration of Laboratory/Instrument/Analyst Capability:

14.4.1 If a laboratory or analyst has not performed this test before or there has been a major change in the measurement system, for example, significant instrument change, new instrument, etc., perform a precision and bias study must be performed to demonstrate laboratory, analyst, or instrument capability.