



Standard Test Method for Calibration of Primary Non-Concentrator Terrestrial Photovoltaic Reference Cells Using a Tabular Spectrum¹

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1. Scope

1.1 This test method is intended for calibration and characterization of primary terrestrial photovoltaic reference cells to a desired reference spectral irradiance distribution, such as Tables G173. The recommended physical requirements for these reference cells are described in Specification E1040. Reference cells are principally used in the determination of the electrical performance of photovoltaic devices.

1.2 Primary photovoltaic reference cells are calibrated in natural sunlight using the relative quantum efficiency of the cell, the relative spectral distribution of the sunlight, and a tabulated reference spectral irradiance distribution. Selection of the reference spectral irradiance distribution is left to the user.

1.3 This test method requires the use of a pyrheliometer that is calibrated according to Test Method E816, which requires the use of a pyrheliometer that is traceable to the World Radiometric Reference (WRR). Therefore, reference cells calibrated according to this test method are traceable to the WRR.

1.4 This test method is used to calibrate primary reference cells; Test Method E1362 may be used to calibrate secondary and non-primary reference cells (these terms are defined in Terminology E772).

1.5 This test method applies only to the calibration of a photovoltaic cell that shows a linear dependence of its short-circuit current on irradiance over its intended range of use, as defined in Test Method E1143.

1.6 This test method applies only to the calibration of a reference cell fabricated with a single photovoltaic junction.

1.7 The values stated in SI units are to be regarded as standard. No other units of measurement are included in this standard.

1.8 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety, health, and environmental practices and determine the applicability of regulatory limitations prior to use.*

1.9 *This international standard was developed in accordance with internationally recognized principles on standardization established in the Decision on Principles for the Development of International Standards, Guides and Recommendations issued by the World Trade Organization Technical Barriers to Trade (TBT) Committee.*

2. Referenced Documents

2.1 ASTM Standards:²

- E490 Standard Solar Constant and Zero Air Mass Solar Spectral Irradiance Tables
- E772 Terminology of Solar Energy Conversion
- E816 Test Method for Calibration of Pyrheliometers by Comparison to Reference Pyrheliometers
- E927 Classification for Solar Simulators for Electrical Performance Testing of Photovoltaic Devices
- E948 Test Method for Electrical Performance of Photovoltaic Cells Using Reference Cells Under Simulated Sunlight
- E973 Test Method for Determination of the Spectral Mismatch Parameter Between a Photovoltaic Device and a Photovoltaic Reference Cell
- E1021 Test Method for Spectral Responsivity Measurements of Photovoltaic Devices
- E1040 Specification for Physical Characteristics of Nonconcentrator Terrestrial Photovoltaic Reference Cells
- E1143 Test Method for Determining the Linearity of a Photovoltaic Device Parameter with Respect To a Test Parameter
- E1362 Test Methods for Calibration of Non-Concentrator Photovoltaic Non-Primary Reference Cells

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² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

E2554 Practice for Estimating and Monitoring the Uncertainty of Test Results of a Test Method Using Control Chart Techniques

G138 Test Method for Calibration of a Spectroradiometer Using a Standard Source of Irradiance

G173 Tables for Reference Solar Spectral Irradiances: Direct Normal and Hemispherical on 37° Tilted Surface

G183 Practice for Field Use of Pyranometers, Pyrheliometers and UV Radiometers

2.2 WMO Document:³

WMO-No. 8 Guide to Meteorological Instruments and Methods of Observation, Seventh ed., 2008.

3. Terminology

3.1 *Definitions*—Definitions of terms used in this test method may be found in Terminology **E772**.

3.2 The following symbols and units are used in this test method:

3.3 *Symbols*:

3.3.1 A_x —collimator aperture identifiers (non-numeric).

3.3.2 C —calibration value, reference cell (Am^2W^{-1}).

3.3.3 \mathbf{C} —array of calibration values, reference cell (Am^2W^{-1}).

3.3.4 D —as a subscript, refers to the reference cell to be calibrated; as a variable, distance from collimator entrance aperture to reference cell top surface, or to spectroradiometer entrance optics (m).

3.3.5 E —total irradiance, measured with pyrheliometer (Wm^{-2}).

3.3.6 \mathbf{E} —array of measured total irradiance values (Wm^{-2}).

3.3.7 $E(\lambda)$ —spectral irradiance ($\text{Wm}^{-2}\mu\text{m}^{-1}$ or $\text{Wm}^{-2}\text{nm}^{-1}$).

3.3.8 $E_S(\lambda)$ —measured solar spectral irradiance ($\text{Wm}^{-2}\mu\text{m}^{-1}$ or $\text{Wm}^{-2}\text{nm}^{-1}$).

3.3.9 $E_o(\lambda)$ —reference spectral irradiance distribution ($\text{Wm}^{-2}\mu\text{m}^{-1}$ or $\text{Wm}^{-2}\text{nm}^{-1}$).

3.3.10 F —spectral correction factor (dimensionless).

3.3.11 FOV —field-of-view ($^\circ$).

3.3.12 I —short-circuit current, reference cell (A).

3.3.13 \mathbf{I} —array of measured short-circuit currents, reference cell (A).

3.3.14 i —as a subscript, refers to the i th current and irradiance data point (dimensionless).

3.3.15 j —as a subscript, refers to the j th calibration value data point (dimensionless).

3.3.16 L —collimator length (m).

3.3.17 n —number of current and irradiance data points measured during calibration time period (dimensionless).

3.3.18 m —number of calibration value data points (dimensionless).

3.3.19 M —spectral mismatch parameter (dimensionless).

3.3.20 $O_D(\lambda, T)$ —quantum efficiency, reference cell (%).

3.3.21 r_x —collimator inner aperture radius (m).

3.3.22 R —collimator entrance aperture radius (m).

3.3.23 R_E —pyrheliometer to integrated spectral irradiance ratio (dimensionless).

3.3.24 RNG —as a subscript, refers to the minimum-to-maximum range of an array of values.

3.3.25 s —sample standard deviation, reference cell calibration value (Am^2W^{-1}).

3.3.26 T —temperature ($^\circ\text{C}$).

3.3.27 T_o —calibration temperature, reference cell (25°C).

3.3.28 $Z_P(\lambda)$ —pyrheliometer spectral transmittance function (dimensionless).

3.3.29 λ —wavelength (μm or nm).

3.3.30 θ_o —collimator opening angle ($^\circ$).

3.3.31 θ_s —collimator slope angle ($^\circ$).

3.3.32 $\Theta_D(\lambda)$ —partial derivative of quantum efficiency with respect to temperature ($\% \cdot ^\circ\text{C}^{-1}$).

4. Summary of Test Method

4.1 The calibration of a primary photovoltaic reference cell consists of measuring the short-circuit current of the cell when illuminated with natural sunlight, along with the direct solar irradiance using a pyrheliometer (see Terminology **E772**). The ratio of the short-circuit current of the cell to the irradiance is called the responsivity, which, when divided by a spectral correction factor similar to the spectral mismatch parameter defined in Test Method **E973**, is the calibration value for the reference cell. The spectral correction factor also corrects the calibration value to 25°C (see **4.2.2**).

4.1.1 The relative spectral irradiance of the sunlight is measured using a spectroradiometer as specified in Test Method **G138** and Test Method **E973**.

4.1.2 A pyrheliometer measures direct solar irradiance by restricting the field-of-view (FOV) to a narrow conical solid angle, typically 5° , that includes the 0.5° cone subtended by the sun. This calibration method requires that the same irradiance measured by the pyrheliometer also illuminate the primary reference cell to be calibrated and the spectroradiometer simultaneously. Thus, both are required to have collimators (see **6.2**).

4.1.3 Multiple calibration values determined from I , E , and $E(\lambda)$ measurements made on a minimum of three different days, are averaged to produce the final calibration result. Each data point corresponds to a single $E(\lambda)$ spectral irradiance.

4.2 The following is a list of measurements that are used to characterize reference cells and are reported with the calibration data:

4.2.1 The relative quantum efficiency of the cell is determined in accordance with Test Methods **E1021**.

4.2.2 Temperature sensitivity of the cell's short-circuit current is determined experimentally by measuring the partial derivative of quantum efficiency with respect to temperature, as specified in Test Method **E973**.

³ Available from World Meteorological Organization (WMO), 7bis, avenue de la Paix, Case Postale No. 2300, CH-1211 Geneva 2, Switzerland, <http://www.wmo.int>.

4.2.3 Linearity of short-circuit current versus irradiance is determined in accordance with Test Method [E1143](#).

4.2.4 The fill factor of the reference cell is determined using Test Method [E948](#). Providing the fill factor with the calibration data allows the reference cell to be checked in the future for electrical degradation or damage.

5. Significance and Use

5.1 The electrical output of a photovoltaic device is dependent on the spectral content of the illumination source, its intensity, and the device temperature. To make standardized, accurate measurements of the performance of photovoltaic devices under a variety of light sources when the intensity is measured with a calibrated reference cell, it is necessary to account for the error in the short-circuit current that occurs if the relative quantum efficiency of the reference cell is not identical to the quantum efficiency of the device to be tested. A similar error occurs if the spectral irradiance distribution of the test light source is not identical to the desired reference spectral irradiance distribution. These errors are accounted for by the spectral mismatch parameter (described in Test Method [E973](#)), which is a quantitative measure of the error in the short-circuit current measurement. It is the intent of this test method to provide a recognized procedure for calibrating, characterizing, and reporting the calibration data for primary photovoltaic reference cells using a tabular reference spectrum.

5.2 The calibration of a reference cell is specific to a particular spectral irradiance distribution. It is the responsibility of the user to specify the applicable irradiance distribution, for example Tables [G173](#). This test method allows calibration with respect to any tabular spectrum.

5.2.1 Tables [G173](#) do not provide spectral irradiance data for wavelengths longer than 4 μm , yet pyrheliometers (see [6.1](#)) typically have response in the 4–10 μm region. To mitigate this discrepancy, the Tables [G173](#) spectra must be extended with the data provided in [Annex A2](#).

5.3 A reference cell should be recalibrated at yearly intervals, or every six months if the cell is in continuous use outdoors.

5.4 Recommended physical characteristics of reference cells can be found in Specification [E1040](#).

5.5 High-quality silicon primary reference cells are expected to be stable devices by nature, and as such can be considered control samples. Thus, the calibration value data points (see [9.3](#)) can be monitored with control chart techniques according to Practice [E2554](#), and the test result uncertainty estimated. The control charts can also be extended with data points from previous calibrations to detect changes to the reference cell or the calibration procedures.

6. Apparatus

6.1 *Pyrheliometer*—A secondary reference pyrheliometer that is calibrated in accordance with Test Method [E816](#), or an absolute cavity radiometer. See also World Radiometric Reference in Terminology [E772](#) and the World Meteorological Organization (WMO) guide WMO-No.8, Chapter 7. Practice

[G183](#) provides guidance to the use of pyrheliometers for direct solar irradiance measurements.

6.1.1 Because secondary reference pyrheliometers are calibrated against an absolute cavity radiometer, the total uncertainty in the primary reference cell calibration value will be reduced if an absolute cavity radiometer is used.

6.1.2 The spectral transmittance function of the pyrheliometer must be considered. For an absolute cavity radiometer without a window, $Z_p(\lambda)$ can be assumed to be one over a very wide wavelength range. Secondary reference pyrheliometers typically have a window at the entrance aperture, so $Z_p(\lambda)$ can be assumed to be the spectral transmittance of the window material.

6.1.2.1 Test Method [E816](#) requires absolute cavity radiometers to be “nonselective over the range from 0.3 to 10 μm ”, and secondary reference pyrheliometers to be “nonselective over the range from 0.3 to 4 μm .”

6.1.2.2 Commercially available secondary pyrheliometers use a variety of different window materials, and many do not meet the 0.3 to 4 μm requirement of Test Method [E816](#). The transmittance of fused silica (SiO_2), for example, has significant variations in the 2 to 4 μm region that depend on the grade of the material (ultraviolet or infrared grade). Sapphire (Al_2O_3) transmits beyond 4 μm , but its transmittance is not entirely flat over 0.4 to 4 μm . Crystalline quartz (SiO_2) is very flat over 0.25 to 2.5 μm , but the transmittance falls to zero by 4 μm . The pyrheliometer manufacturer should be consulted to obtain the window transmittance data.

6.1.2.3 The calibration procedure in Test Method [E816](#) places restrictions on allowable atmospheric conditions and does not adjust calibration results with spectral information: all pyrheliometers are calibrated with the same procedure regardless of the window material.

6.2 *Collimators*—Tubes with internal baffles, intended for pointing toward the sun, that restrict the FOV and are fitted to the reference cell to be calibrated and the spectroradiometer (see [6.3](#)); an acceptable collimator design is provided in [Annex A1](#). The collimators must match the FOV of the pyrheliometer (see [A1.4.1](#)).

6.2.1 Eliminate or minimize any stray light entering the collimators at the bottoms of the tubes.

6.2.2 The receiving aperture of the reference cell collimator shall be sized such that the entire optical surface of the primary reference cell to be calibrated is completely illuminated, including the window (see Specification [E1040](#)). Thus, for a reference cell with a 50 mm square window, the collimator would require a receiving aperture radius equal to:

$$\sqrt{50^2 + 50^2} / 2 = 35.4 \text{ mm}$$

6.3 *Spectroradiometer*, as required by Test Methods [G138](#) and [E973](#) for direct normal solar spectral irradiance measurements.

6.3.1 The wavelength range of the spectral irradiance measurement shall be wide enough to span the wavelength range of the quantum efficiency of the cell to be calibrated (see [6.7.3](#)) and the spectral sensitivity function of the pyrheliometer (see [6.1.2](#)).

6.3.2 If the spectral irradiance measurement is unable to measure the entire wavelength range required by 6.3.1 and 6.3.2, it is acceptable to use a reference spectrum, such as Tables G173, to supply the missing wavelengths. The reference spectrum is scaled to match the measured spectral irradiance data over a convenient wavelength interval within the wavelength range of the spectral irradiance measurement equipment. It is also acceptable to calculate the missing spectral irradiance data using a numerical spectral irradiance model.

6.3.2.1 Note that the reference spectrum is also required to include the wavelengths specified by 6.3.1: see 5.2.1.

6.4 *Normal Incidence Tracking Platforms*—A platform or platforms that hold the reference cell to be calibrated, the pyrheliometer, and the spectroradiometer during the calibration procedure. Using two orthogonal axes, such as azimuth and elevation (that is, altazimuthal mount), the platforms must follow the apparent motion of the sun such that the angle between the sun vector and the normal vector is less than 0.1° (that is, the tracking error). The collimators (including that of the pyrheliometer) define the normal vector and shall be parallel to each other within $\pm 0.25^\circ$.

6.4.1 The tracking error tolerance is dependent on the FOV and slope angle of the pyrheliometer and the collimators (see A1.4.1); WMO-No. 8 states that 0.1° is acceptable for the recommended FOV of 5° and slope angle of 1° .

6.5 *Temperature Measurement Equipment*—The instrument or instruments used to measure the temperature of the reference cell to be calibrated must have a resolution of at least 0.1°C , and a total uncertainty of less than $\pm 1^\circ\text{C}$ of reading when such uncertainty is combined with the uncertainty of the sensors themselves.

6.5.1 Sensors such as thermocouples or thermistors used for the temperature measurements must be located in a position that minimizes any temperature gradients between the sensor and the photovoltaic device junction.

6.6 *Electrical Measurement Equipment*—Voltsmeters, ammeters, or other suitable electrical measurement instruments, used to measure the short-circuit current, I , of the cell to be calibrated and the pyrheliometer output, E , must have a resolution of at least 0.02 % of the maximum current or voltage encountered, and a total uncertainty of less than 0.1 % of the maximum current or voltage encountered.

6.6.1 The electrical measurement equipment should be able to record a minimum of 50 to 100 data points during the calibration time period (see 8.1).

6.7 *Quantum Efficiency Measurement Equipment*, as required by Test Method E1021 for spectral responsivity measurements and the following additional requirements:

6.7.1 The wavelength interval between successive quantum efficiency data points shall be 10 nm or less.

6.7.2 For reference cells made with direct bandgap semiconductors such as GaAs, it is recommended that the wavelength interval be no greater than 5 nm.

6.7.3 The low- and high-wavelength endpoints of the quantum efficiency measurement shall span all wavelengths for which the measured quantum efficiency are greater than 1 % of the maximum quantum efficiency.

6.7.4 The full-width-at-half maximum bandwidth for the monochromatic light source shall be 10 nm or less.

6.8 *Temperature Control Block (Optional)*—A device to maintain the temperature of the reference cell at $25 \pm 1^\circ\text{C}$ for the duration of the calibration.

7. Characterization

7.1 Because some silicon solar cells are susceptible to a loss of short-circuit current upon initial exposure to light, newly manufactured reference cells shall be light soaked prior to initial characterization, as follows:

7.1.1 Measure the short-circuit current and the cell area of the reference cell to be calibrated according to Test Method E948, with respect to standard reporting conditions corresponding to the reference spectral irradiance distribution (see 5.2 and Table 1 of Test Method E948).

7.1.2 Connect the reference cell to the electrical measurement equipment (see 6.6) and prepare to record short-circuit current versus time.

7.1.3 Illuminate the reference cell with either natural sunlight or a solar simulator (see Specification E927); the spectral irradiance is not critical, nor is the cell temperature.

7.1.4 Record the short-circuit current of the reference cell when the current is greater than 85 % of the current measured in 7.1.1.

7.1.5 Integrate the short-circuit currents recorded in 7.1.4 with time to calculate the total charge generated.

7.1.6 Discontinue the illumination when 22 MCm^{-2} have been generated. For an Si solar cell with a short-circuit current density of 300 Am^{-2} at 1000 Wm^{-2} , this amount of charge requires approximately 20 h of illumination.

7.2 Characterize the reference cell to be calibrated by the following methods:

7.2.1 *Quantum Efficiency*—Determine the relative quantum efficiency (optionally the absolute quantum efficiency) of the reference cell to be calibrated at 25°C in accordance with Test Methods E1021 and the requirements of 6.7.

7.2.1.1 Repetition of 7.2.1 is optional if the quantum efficiency has been previously measured in accordance with 7.2.1.

7.2.2 *Partial Derivative of Quantum Efficiency with Respect to Temperature*—Determine the working temperature range of the reference cell to be calibrated and measure its $\theta_D(\lambda)$ according to Annex A1 of Test Methods E973.

NOTE 1—Test Method E973 requires all quantum efficiency measurements needed for $Q_D(\lambda, T_0)$ and $\theta_D(\lambda)$ be measured with the same multiplicative calibration or scaling factors.

7.2.2.1 Repetition of 7.2.2 is optional if $\theta_D(\lambda)$ has been previously measured in accordance with 7.2.2.

7.2.3 *Linearity*—Determine the short-circuit current versus irradiance linearity of the cell being calibrated in accordance with Test Method E1143 for the irradiance range 750 to 1100 Wm^{-2} .

7.2.3.1 For reference cells that use single-crystal silicon solar cells, or for reference cells that have been previously characterized, the short-circuit current versus irradiance linearity determination is optional.

7.2.4 *Fill Factor*— Determine the fill factor of the cell to be calibrated from the I-V curve of the device, as measured in accordance with Test Methods E948.

8. Procedure

8.1 Select the time period for a single calibration data point. Two factors must be considered: (1) the response time of the pyrheliometer, and (2) the time required for the spectroradiometer to measure a single spectral irradiance.

8.1.1 Pyrheliometers have response times (defined as the time required for the instrument to indicate 95 % of a step change of input irradiance) on the order of 1 to 30 s. It is recommended that the calibration time period span the manufacturer's specified response time by a factor of at least five.

8.1.1.1 Absolute cavity radiometers are self-calibrating instruments that rely on periodically blocking all light with shutters; the blocked periods must be considered when selecting the calibration time period.

8.1.2 Spectroradiometers that use mechanically rotated diffraction gratings can require as much as 60 s to scan a single spectral irradiance, while those that employ photodiode arrays can reduce the measurement time to tens of milliseconds.

8.1.3 Use the larger of either 8.1.1 or 8.1.2 as the calibration time period.

8.2 Mount the reference cell to be calibrated, the pyrheliometer, and the spectroradiometer on the tracking platforms, and orient the collimating tubes parallel to the sun vector within the tracking limits of the platforms (see 6.4).

8.3 Collect data for a single calibration data point during the calibration time period as follows:

8.3.1 Measure an array of reference cell short-circuit current values, where n is the number of current values:

$$\mathbf{I} = [I_1 \ I_2 \ \dots \ I_n] \quad (1)$$

8.3.2 Measure an array of the pyrheliometer output values, where n is the number of irradiance values:

$$\mathbf{E} = [E_1 \ E_2 \ \dots \ E_n] \quad (2)$$

8.3.3 Depending on the speed of the electrical measurement equipment (see 6.6), the numbers of current and irradiance values obtained in 8.3.1 and 8.3.2 might not be identical, and they are not required to be identical. However, the time periods over which the values are obtained must be identical.

8.3.4 Measure the spectral irradiance for the calibration time period using the spectroradiometer.

8.3.4.1 If the spectroradiometer measurement time is less than the calibration time period, collect multiple spectra and average them to obtain a single spectral irradiance.

8.3.5 Measure the reference cell temperature, T_D .

8.4 Perform a minimum of six replications of 8.3 on at least three separate days; more repetitions are recommended.

9. Calculation of Results

9.1 Each spectral irradiance measurement obtained in 8.3 defines one data point; denote the total number of these points as m .

9.2 For each data point, where $j=1\dots m$:

9.2.1 Compute the mean short-circuit current, where n is the number of current values measured in each repetition of 8.3.1:

$$I_j = \langle \mathbf{I}_j \rangle = \frac{1}{n} \sum_{i=1}^n I_i \quad (3)$$

9.2.2 Compute the mean irradiance, where n is the number of current values measured in each repetition of 8.3.2:

$$E_j = \langle \mathbf{E}_j \rangle \quad (4)$$

9.2.3 Compute the short-circuit current range in percent:

$$I_{RNGj} = 200 \frac{\max \mathbf{I}_j - \min \mathbf{I}_j}{\max \mathbf{I}_j + \min \mathbf{I}_j} \quad (5)$$

9.2.4 Compute the irradiance range in percent:

$$E_{RNGj} = 200 \frac{\max \mathbf{E}_j - \min \mathbf{E}_j}{\max \mathbf{E}_j + \min \mathbf{E}_j} \quad (6)$$

9.2.5 Discard any data points for which E_j is $<750 \text{ Wm}^{-2}$ or $>1100 \text{ Wm}^{-2}$.

9.2.6 Discard any data points for which I_{RNGj} is $>1 \%$.

9.2.7 Discard any data points for which E_{RNGj} is $>0.5 \%$.

9.2.8 The range limits in 9.2.5, 9.2.6, and 9.2.7 have been found useful for rejecting questionable data points and may be adjusted as needed. The smaller limit for E_{RNGj} reflects the difference between the time constant of the pyrheliometer and the nearly instantaneous response time of a solar cell; if the irradiance changes by more than 0.5 % during the calibration time period, then it is likely that the pyrheliometer is not in thermal equilibrium.

9.2.9 Calculate the spectral correction factor, F_j , using the following equation:

$$F_j = \frac{\int_{\lambda_1}^{\lambda_2} \lambda Q_D(\lambda, T_0) E_{Sj}(\lambda) d\lambda + (T_{Dj} - T_0) \int_{\lambda_1}^{\lambda_2} \lambda \Theta_D(\lambda) E_{Sj}(\lambda) d\lambda}{\int_{\lambda_3}^{\lambda_4} Z_P(\lambda) E_{Sj}(\lambda) d\lambda} \times \frac{\int_{\lambda_3}^{\lambda_4} Z_P(\lambda) E_0(\lambda) d\lambda}{\int_{\lambda_1}^{\lambda_2} \lambda Q_D(\lambda, T_0) E_0(\lambda) d\lambda} \quad (7)$$

where:

$$T_0 = 25^\circ,$$

$$Q_D(\lambda, T_0) = \text{the quantum efficiency of the reference cell to be calibrated (see 7.2.1),}$$

$$E_{Sj}(\lambda) = \text{spectral irradiance,}$$

$$T_{Dj} = \text{the measured cell temperature (see 8.3.4),}$$

$$\Theta_D(\lambda) = \text{the partial derivative of quantum efficiency with respect to temperature (see 7.2.2), and}$$

$$Z_P(\lambda) = \text{the spectral transmittance of the pyrheliometer (see 6.2.1).}$$

9.2.9.1 Eq 7 is similar to the spectral mismatch parameter, M , as expressed in Eq 1 of Test Method E973. Rather than an expression of four short-circuit current densities (see Appendix X1 of Test Method E973), Eq 7 is instead the ratio of two responsivities.

9.2.9.2 The wavelength integration limits λ_1 and λ_2 shall correspond to the spectral response limits of the photovoltaic device (see 6.7.1).

9.2.9.3 The wavelength integration limits λ_3 and λ_4 shall correspond to those of the spectral transmittance function of the pyrheliometer, $Z_P(\lambda)$ (see 6.1.2).

9.2.9.4 If necessary (see 5.2.1), extend the reference spectral irradiance distribution with the data provided in Annex A2.

9.2.9.5 If $|T_{Dj} - T_0| \leq 1^\circ\text{C}$, the temperature correction integral containing $\Theta_D(\lambda)$ may be assumed to be zero and eliminated from the calculation of F_j .

9.2.10 Calculate the calibration value:

$$C_j = \frac{I_j}{E_j} \cdot \frac{1}{F_j} \quad (8)$$

9.2.11 Calculate the pyrheliometer to integrated spectral irradiance ratio:

$$R_{Ej} = \frac{E_j}{\int_{\lambda_3}^{\lambda_4} Z_p(\lambda) E_{sj}(\lambda) d\lambda} \quad (9)$$

9.2.11.1 The irradiance ratio, R_{Ej} , will depend on the spectroradiometer's calibration and thus is not necessarily equal to one; this is not an error in the reference cell calibration value because the spectral correction factor does not require absolute spectral quantities (see Test Method E973). However, the R_{Ej} values should be used as rejection criteria through comparison and monitoring to detect possible problems with individual data points.

9.3 Construct an array of calibration values using the results obtained in 9.2.10.

$$\mathbf{C} = [C_1 \ C_2 \ \dots \ C_m] \quad (10)$$

9.4 Compute the mean calibration value:

$$C = \langle \mathbf{C} \rangle \quad (11)$$

9.5 Compute the sample standard deviation of the calibration value:

$$s = \sqrt{\frac{\mathbf{C} \cdot \mathbf{C} - mC^2}{m - 1}} \quad (12)$$

9.6 Compute the range of the calibration value:

$$C_{RNG} = 2 \frac{\max \mathbf{C} - \min \mathbf{C}}{\max \mathbf{C} + \min \mathbf{C}} \quad (13)$$

9.7 *Optional*—If the number of data points collected on any one day is greater than those from the other days (see 8.4), separate the data points according to day and compute the mean calibration value using Eq 10 for each day. Then compute the final mean calibration value using the daily mean values. This prevents coloration of the results by the atmospheric conditions on a single day.

10. Report

10.1 Report, as a minimum, the following information:

10.1.1 Reference cell serial number.

10.1.2 Date of calibration.

10.1.3 Reference spectral irradiance distribution, $E_0(\lambda)$.

10.1.4 *Reference Cell*:

10.1.4.1 Quantum efficiency, $Q_D(\lambda, T_0)$, as required by Test Method E973.

10.1.4.2 Partial derivative of quantum efficiency with respect to temperature, $\Theta_D(\lambda)$ as required by Test Method E973.

10.1.4.3 Fill factor.

10.1.4.4 Linearity verification, as required by Test Method E1143.

10.1.4.5 Calibration value, C .

10.1.4.6 Calibration value standard deviation, s .

10.1.4.7 Calibration range, C_{RNG} .

10.1.5 Pyrheliometer type, manufacturer, serial number, calibration value, data last calibrated.

10.1.6 Complete description of measurement system.

10.1.7 Any deviations from the standard calibration procedure.

10.1.8 Any unusual occurrences during calibration.

10.1.9 Data for each point in calibration, that shall include the following:

10.1.9.1 Cell temperature, T_{Dj} ,

10.1.9.2 Irradiance, E_j ,

10.1.9.3 Irradiance range, E_{RNGj} ,

10.1.9.4 Short-circuit current, I_j ,

10.1.9.5 Short-circuit current range, I_{RNG} ,

10.1.9.6 Pyrheliometer to integrated spectral irradiance ratio, R_{Ej} , and

10.1.9.7 Spectral correction factor, F_j .

11. Precision and Bias

11.1 *Precision*—It is not possible to specify the precision of the reference cell calibration test method using the results of an interlaboratory study because no laboratories were willing to participate in such a study. The restrictions placed on the apparatus and the calibration conditions have been selected to minimize precision errors in the reference cell calibration value. Factors that contribute to the total precision error include:

11.1.1 Temporal variations of the solar spectral and total irradiance during the calibration time periods (see 8.3) will introduce errors.

11.1.2 The discussion of precision of spectral measurements in 9.1 of Test Method E973 is applicable to the reference cell calibration test method.

11.1.3 Temperature variations of the reference cell being calibrated within the $25 \pm 1^\circ\text{C}$ band will introduce small errors in the calibration value if the temperature corrections are not employed (see 9.2.9.5). The partial derivative of quantum efficiency with respect to temperature (see 7.2.1) controls the magnitude of these errors.

11.1.4 Electronic instrumentation used to measure the reference cell short-circuit current, the total irradiance, and the cell temperature will contribute precision errors to the calibration value.

11.2 *Bias*—The contribution of bias to the total error will depend upon the bias of each individual factor used for the determination of the calibration value. Possible individual contributions of bias include:

11.2.1 The slope of the cell's I-V curve near zero volts, and loading of the cell by the current measurement instrument due to nonzero input impedance can result in somewhat smaller values of the short-circuit current. This situation can be minimized by forcing the reference cell voltage as close to zero as possible during the short-circuit current measurement.

11.2.2 Measurement of the cell temperature at the back of the device will give a value that is lower than the junction temperature during exposure of the cell to sunlight. This may

result in slightly too high a value for short-circuit current. Because the short-circuit current temperature coefficient is usually small, this source of bias tends to be small.

11.2.3 Each measurement instrument will introduce bias into the final calibration in varying amounts. It is assumed that all instruments are calibrated at regular intervals. However, bias will still affect any instrumentation even after careful calibration.

11.2.4 An absolute accuracy of 0.25 % for terrestrial solar radiometric measurements has been established for absolute cavity radiometers that have been compared with the World Radiometric Reference. If a secondary reference pyrheliometer

is used, a 1 % transfer error from the cavity radiometer should be expected when utilizing the procedures of Test Method E816.

11.2.5 The discussion of bias in spectral measurements in 9.2 of Test Method E973 is applicable to the reference cell calibration test method.

12. Keywords

12.1 calibration; electrical performance; photovoltaic devices; primary terrestrial photovoltaic reference cells; spectral irradiance; spectral response; terrestrial photovoltaic reference cells

ANNEXES

(Mandatory Information)

A1. COLLIMATOR DESIGN

A1.1 Fig. A1.1 shows a cross section through the center of the tubular collimator assembly. Five apertures are used: A₁ is the entrance aperture, and A₂, A₃, A₄, and A₅ are the inner apertures, with their respective radii being R and r₂ through r₅. The apertures block light from outside the conical solid angle of the field-of-view (FOV).

A1.2 Three parameters determine the dimensions of the collimator; these are the FOV, the receiving aperture radius, r, and the slope angle, θ_s.

A1.2.1 The FOV and θ_s are selected to be the same as those of the pyrheliometer.

A1.2.2 The receiving aperture radius, r, defines the circular illumination area, which needs to encompass the size of the largest reference cell that will be calibrated, or the entrance optics of the spectroradiometer.

A1.2.3 Note that D is the distance to the top surface of the reference cell (or the spectroradiometer entrance optics) and not the distance to the final inner aperture, L₅. As a result, if the reference cell is positioned away from A₅, that is, D > L₅, the illumination area will be smaller than the area of the final inner aperture, and the FOV will be reduced. To ensure that all reference cells are calibrated with the same FOV, it is recommended that the collimator and test fixture be designed to allow adjustment of D–L₅ for difference reference cell package geometries.

A1.3 With the FOV, θ_s, and r known, the design dimensions are calculated using geometry.

A1.3.1 Opening angle:

$$\theta_o = \frac{1}{2} \text{FOV} \tag{A1.1}$$

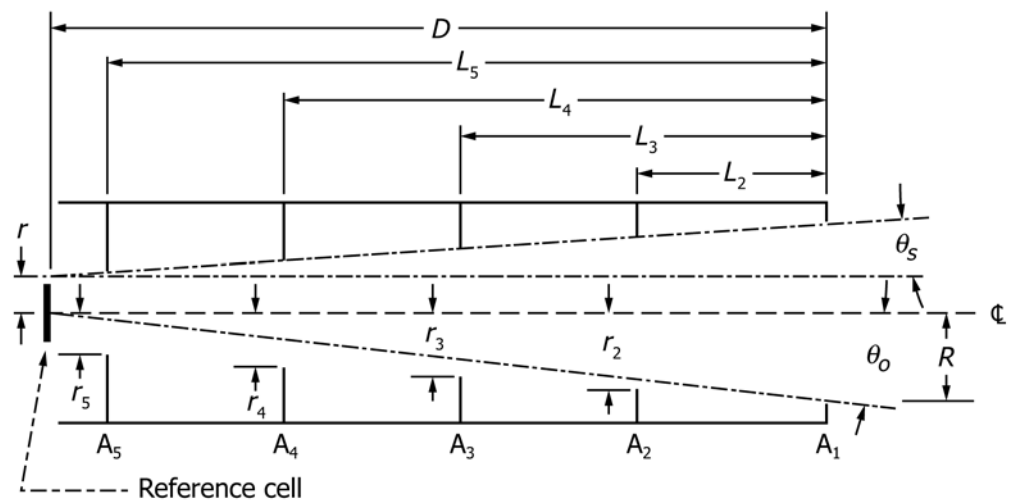


FIG. A1.1 Collimator Design Cross Section