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Standard Test Method for Measurement of Computed Tomography (CT) System Performance¹

This standard is issued under the fixed designation E1695; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ε) indicates an editorial change since the last revision or reapproval.

This standard has been approved for use by agencies of the U.S. Department of Defense.

1. Scope

1.1 This test method provides instruction for determining the spatial resolution and contrast sensitivity in X-ray and γ -ray computed tomography (CT) images:volumes. The determination is based on examination of the CT imagevolume of a uniform diskcylinder of material. The spatial resolution measurement (Modulation Transfer Function) is derived from an image analysis of the sharpness at the edgeedges of the disk. reconstructed cylinder slices. The contrast sensitivity measurement (Contrast Discrimination Function) is derived from an image analysis of the contrast and the statistical noise at the center of the disk.cylinder slices.

1.2 This test method is more quantitative and less susceptible to interpretation than alternative approaches because the required diskcylinder is easy to fabricate and the analysis is immune to cupping artifacts. This test method may not yield meaningful results if the disk image occupies less than a significant fraction of the field of view.easy to perform.

1.3 This test method may also be used to evaluate other performance parameters. Among those characteristics of a CT system that are detectable with this test method are: the mid-frequency enhancement of the reconstruction kernel, the presence (or absence) of detector crosstalk, the undersampling of views, and the clipping of unphysical (that is, negative) CT numbers (see Air Force Technical Report WL-TR-94-4021 is not to predict the detectability of specific object features or flaws in a specific application. This). It is highly likely that other characteristics as well can be detected with this test method. is subject of IQI and RQI standards and standard practices.

1.4 This method tests and describes overall CT system performance. Performance tests of systems components such as X-ray tubes, gamma sources, and detectors are covered by separate documents, namely Guide E1000, Practice E2737, and Practice E2002; c.f. 2.1, which should be consulted for further system analysis.

1.5 <u>Units</u>—The values stated in SI units are to be regarded as the standard. Inch-pound standard. The values given in parentheses after SI units are provided for information only.only and are not considered standard.

1.6 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety safety, health, and health environmental practices and determine the applicability of regulatory limitations prior to use.

<u>1.7 This international standard was developed in accordance with internationally recognized principles on standardization established in the Decision on Principles for the Development of International Standards, Guides and Recommendations issued by the World Trade Organization Technical Barriers to Trade (TBT) Committee.</u>

¹ This test method is under the jurisdiction of ASTM Committee E07 on Nondestructive Testing and is the direct responsibility of Subcommittee E07.01 on Radiology (X and Gamma) Method.

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2. Referenced Documents

2.1 ASTM Standards:²

E177 Practice for Use of the Terms Precision and Bias in ASTM Test Methods

E691 Practice for Conducting an Interlaboratory Study to Determine the Precision of a Test Method

E1000 Guide for Radioscopy

E1316 Terminology for Nondestructive Examinations

E1441 Guide for Computed Tomography (CT)

E1570 Practice for Fan Beam Computed Tomographic (CT) Examination

E2002 Practice for Determining Total Image Unsharpness and Basic Spatial Resolution in Radiography and Radioscopy

E2737 Practice for Digital Detector Array Performance Evaluation and Long-Term Stability

2.2 ISO Standard:³

15708 NDT – Radiation Methods – Computed Tomography – Part 1: Terminology, Part 2: Principles, Equipment and Samples, Part 3: Operation and Interpretation, Part 4: Qualification

3. Terminology

3.1 *Definitions*—The definitions of terms relating to Gamma- and X-Radiology, which appear in Terminology E1316 and Guide E1441, shall apply to the terms used in this test method.

3.2 Definitions of Terms Specific to This Standard:

3.2.1 *phantom—examination object, n*—a part or itemspecimen being usedsubjected to quantify-CT system performance.examination.

3.2.2 *examinationphantom, object*—<u>n</u>_a part or specimenitem being subjectedused to <u>quantify</u> CT examination.system performance.

3.3 Acronyms:

3.3.1 CDD—contrast-detail-diagram; see Guide E1441 for details.

<u>3.3.2 *CDF*</u>—contrast discrimination function; describes the influence of image noise on the detectability of a feature in an elsewhere homogeneous material neighborhood as a function of the size of this feature in voxels.

<u>3.3.2.1 Discussion</u> It intentionally does not pay regard to unsharpness effects, as these are covered by the MTF. See Guide E1441 for details.

3.3.3 *ERF*—edge response function.

3.3.4 *PSF*—<u>*LSF*</u>—point<u>line</u> spread function.

3.3.5 *MTF*—modulation transfer function; function; describes the transfer of a spatial modulation in an image signal (relative intensity variation, here by a CT system) as function of the modulation's spatial frequency.

3.3.5.1 Discussion—

Intentionally, it does not include noise effects, as those strongly depend on scan parameters and sample materials. Noise effects are covered by the CDF. See Guide E1441 for details.

3.3.4 CDF—contrast discrimination function.

4. Significance and Use

4.1 <u>Two-The major factors affecting the quality of a CT image are geometrical total image unsharpness (U_T^{image}), contrast ($\Delta\mu$), and random noise. Geometrical unsharpness limits noise (σ). Geometrical and detector unsharpness limit the spatial resolution of</u>

² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

³ Available from International Organization for Standardization (ISO), ISO Central Secretariat, BIBC II, Chemin de Blandonnet 8, CP 401, 1214 Vernier, Geneva, Switzerland, http://www.iso.org.

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a CT system, that is, its ability to image fine structural detail in an object. Random noise <u>limits-and contrast response limit</u> the contrast sensitivity of a CT system, that is, its ability to detect the presence or absence of features in an object. Spatial resolution and contrast sensitivity may be measured in various ways. ASTM specifies In this test method, spatial resolution <u>beis</u> quantified in terms of the modulation transfer function (MTF)(MTF), and contrast sensitivity <u>beis</u> quantified in terms of the contrast discrimination function (CDF) (see (CDF). The relationship between contrast sensitivity and spatial resolution describing the resolving and detecting capabilities is given by the contrast-detail-diagram (CDD metric, see also Guide E1441 and Practice E1570). This test method allows the purchaser or the provider of CT systems or services, or both, to measure and specify spatial resolution and contrast sensitivity.sensitivity and is a measure for system stability over time and performance acceptability.

5. Apparatus

5.1 *DiskCylinder Phantom*—The diskcylinder phantom shall be a right <u>circular</u> cylinder of uniform material conforming to the design and material requirements in Table 1 and Fig. 1. Since spatial resolution and contrast sensitivity depend on the examination task (that is, the examination object and the specified CT parameters), the application requirements must be fixed before the phantom can be designed. In general, each examination task will require a separate phantom. The diameter of the disk relative to the field of view shall be such that the reconstructed image of the disk occupies a significant fraction of the image matrix. Recommended sizes are given in For fan beam CT apparatus with LDA, a disk-shaped Table 2. The diameter and opacity of the disk shall be such that the phantom approximates the attenuation range of the examination object. If possible, the phantom should be of the same material as the examination object, but the other requirements take precedence and may dictate the selection of another material. The design of the disk phantom is a matter of agreement between the purchaser and the supplier.phantom as described in the precedented version of this standard (cf. Test Method E1695-95) is sufficient. Standard ISO 15708-2, Table 1, provides recommendations for X-ray voltages depending on material and thickness.

6. Procedure of Measurement

6.1 The phantom shall be mounted on the CT system with the orientation of the axis of revolution of the disk normalcylinder <u>parallel</u> to the scan <u>plane.axis</u>. The alignment shall not compromise the measurement of geometrical unsharpness. Unless otherwise agreed upon between purchaser and supplier, the unsharpness. The phantom shall be placed at the center of the field of view used for the examination object. It may also be placed off center at defined and documented positions.

6.2 Unless otherwise agreed upon between purchaser and supplier, the <u>The</u> data acquisition parameters shall be <u>identicalsimilar</u> to those used for examination object scans. The slice plane shall intercept the phantom approximately midway between the flat faces of the disk.scans, whereas strong cupping artifacts near the surface shall be avoided by using enough pre-filter material (two half-value layers may be appropriate) or numeric corrections, or both, during the reconstruction.

6.2.1 For fan beam CT, one slice shall be acquired and analyzed.

6.2.2 The cylinder height shall be chosen according to Table 1.

6.2.3 For cone beam CT, three slice planes shall intercept the phantom cylinder at different positions of the detector. The first shall be positioned at the center of the reconstructed volume, the second and third at 15 % from the top and bottom of the reconstructed volume under investigation. MTF and CDF shall be computed on each plane individually. Additional slice locations may be added.

NOTE 1—The opening angle of the cone beam may contribute to lower MTF values, which in turn may result in lower spatial resolution in the object under examination at these opening angles.

6.3 Unless otherwise agreed upon between purchaser and supplier, the reconstruction parameters shall be identical to those used for examination object reconstructions.

6.4 Unless otherwise agreed upon between purchaser and supplier, the display parameters shall be identical to those used for examination object display. It shall be verified by examination that the disk image occupies an image at least two-thirds of the image matrix. Recommended guidelines are given in Table 2.

7. Procedure of Analysis

7.1 Spatial Resolution—From the CT image data, generate the composite profile of the edge of each individual cylinder slice to obtain the edge response function (ERF), as discussed below in this section. Calculate the first derivative of the ERF to obtain the



TABLE 1 Disk Phantom Design Requirements

The material, in conjunction with the diameter of the disk,
shall be such that the phantom approximates the
attenuation range of the examination object. The material
should preferably be the same as that of the examination
object.
The diameter shall be such that the reconstruction of the disk
occupies a significant fraction of the resulting image. In
conjunction with the material, the diameter shall be such
that the phantom approximates the attenuation range of the
examination object.
The thickness of the disk shall be greater than the slice
thickness used to inspect the examination object.
The perpendicularity of the axis of revolution with respect to
the surface used to mount the phantom on the CT system
shall not compromise the measurement of geometrical
unsharpness.
The surface texture roughness of the curved surface shall not
compromise the measurement of geometrical unsharpness.

TABLE 1 a Disk Phantom Design Requirements

NOTE 1—The cupping effect due to beam hardening should be reduced by prefilters in front of the X-ray tube or in front of the detector or by numeric corrections in the reconstruction algorithm, or both.

Material	The material, in conjunction with the diameter of the cylinder,
	shall be such that the phantom approximates the attenua-
	tion range of the examination object. The material should
	preferably be the same as that of the examination object.
Diameter	The diameter shall be such that the reconstruction of the cyl-
	inder occupies at least 250 voxels in diameter of the result-
	ing image. In conjunction with the material, the diameter
	shall be such that the phantom approximates the attenua-
	tion range of the examination object provided the beam
	hardening effects are acceptable
Height	The height of the cylinder should cover 80 % the detector
Teight	height of model in the middle line at the magnification
	used to inspect the examination object. It may be shorter if
	there are means to may be field of view
Shape	The percention of the axis of revolution with respect to
	the performance to me and the mean the performance to
	the surface used to mount the prianton on the CT system
	shall not compromise the measurement of geometrical un-
	ASTM E sharpness. The reconstructed image may be realigned by
1 // 🛶 1 1	software for evaluation.
https://stanc <u>Finish</u> s.itel	The surface texture roughness of the curved surface shall not
	affect the measurement of geometrical unsharpness.

TABLE 1 b Cylinder Phantom Suggestions

NOTE 1—The circularity is recommended, assuming the diameter covers up to 1000 voxels.

Cylinder Diameter [mm]	Circularity [mm]
<u>1</u>	0.001
3	0.003
10	0.010
30	0.030
100	<u>0.10</u>
Materials	Diameters [mm]
Plastic (for example, Delrin)	1-100
Aluminum	1-100
Steel	1-30
Inconel	<u>1-30</u>

line spread function (LSF). Calculate the magnitude of the Fourier Transform⁴ of the LSF and normalize the results to unity at zero frequency to obtain the modulation transfer function (MTF). In detail:

7.1.1 The ERF shall be generated as follows; cf. Fig. 2:

⁴ The Fourier Transform and Its Applications, Ronald M. Bracewell, McGraw-Hill, NY, ISBN 0-07-007013-X. Bracewell, R. M., *The Fourier Transform and Its Applications*, McGraw-Hill, NY, ISBN 0-07-007013-X.



FIG. 1 Disk PhantomPrinciple Drawing of the Cylinder Phantom, Not to Scale

iTeh Standards

7.1.1.1 Find the 50 % iso-surface of the disk and fit a circle to it. Its radius is r_c . Other, more advanced methods of surface detection are permitted and shall be documented.

7.1.1.2 Select the inner and outer radii, r_i and r_o of the evaluation annulus with respect to the center of the circle resulting from 7.1.1.1 that comfortably bracket the edge, that is, it should extend from top plateau level to background level.

7.1.1.3 Compute the distance to the center of mass for all voxels between the inner and outer radii.

7.1.1.4 Generate a table of voxel values in order of their voxel distance from the circle center.

7.1.1.5 Segregate the values into equal bins sized to a small fraction of one voxel. The bin size should be as small as practical without causing some bins to be empty. Recommended sizes are given in Table 2.

7.1.1.6 Average the members of each bin to obtain a table of values at constant increments from the inner r_i to outer radius r_o .

7.1.1.7 Starting at one end of the table and iterating until the entire table has been processed, smooth the voxel values by performing a piece-wise, least-squares cubic fit to an odd number of table values and replacing the center value with that predicted by the fit. The number of values to include in the fit should be large compared to the order of the polynomial and small compared to the fine ERF structure. Recommended guidelines for the number of values to use in the fit are given in Table 2.

7.1.1.8 Determine how much of the table is needed to be included in the analysis and delete the unwanted portions of the leading and trailing tails to obtain the ERF.

7.1.2 The LSF shall be generated as follows:

7.1.2.1 Starting at one end of the table and iterating until the entire table has been processed, perform a piece-wise, least-squares cubic fit to the ERF using for the fit the same number of values as were used to smooth the data (see 7.1.1).

7.1.2.2 For each fit, calculate the analytical derivative of the resultant polynomial and determine its numerical value at the center of the piece-wise window.

7.1.2.3 Generate a table of derivative values as a function of distance from the center of the cylinder.



FIG. 2 Typical Tile PatternAreas for Evaluation

TABLE 2 Suggested Measurement Parameters



7.1.2.4 Normalize the peak value of the resulting curve to unity to obtain the LSF.

7.1.3 The MTF shall be generated as follows:

7.1.3.1 Calculate the Fourier Transform⁴ of the LSF. The maximum frequency of the resultant transform should be at least four times the cut-off frequency of the matrix, which is 0.5 line-pairs per voxel. The sampling frequency in the Fourier domain should be small enough that the transform is smooth within the frequency range of interest. A sampling frequency of 0.01 lp/mm or smaller is recommended.

7.1.3.2 Calculate the magnitude of the transform by taking the square root of the product of the transform and its conjugate (Magnitude spectrum).

7.1.3.3 Normalize the magnitude at zero frequency to unity (100 % at MTF for zero spatial frequency) to obtain the MTF.

7.1.4 The MTF shall be visually displayed or plotted, or both, and the frequency at 10 % modulation (MTF₁₀) quantitatively indicated for each evaluated slice indicating its distance to the detector center (in direction to the rotation axis). Although not mandatory, the ERF and the LSF should also be graphically presented, with the full width at half maximum of the LSF quantitatively indicated. (The LSF, in particular, may indicate distortions of the X-ray source.)

7.2 Contrast Sensitivity:

<u>7.2.1</u> Background Correction—Define a second annulus (see Fig. 2) which will be used to determine the background level (air) μ_{air} by averaging all *n* voxel values within this annulus. Let d(x) be the distance of a voxel *x* to the center of the cylinder slice, $R = \{x \mid r_a < d \ (x) \le r_b\}$ the voxels in the annulus, and n = #R the respective number of voxels.

$$\mu_{air} = \frac{1}{n} \sum_{x \in \mathbb{R}} x \tag{1}$$

Subtract the average background μ_{air} from all voxel values x in the region of interest defined in 7.2.2.

7.2.2 *Contrast Discrimination Function*—From the CT image data, generate a sequence of tile patterns of tiles T_i of size D^* (=1,2,3,...), so that T_i contains $n = D^* \cdot D^*$ numbers of voxels, n being the number voxels in a single tile; see Fig. 3. The tile pattern shall fit within the central regions of the individual cylinder slices. For each pattern, calculate the mean voxel value μ_i of all now background corrected voxel values x (cf. 7.2.1) within each tile



NOTE 1—For tiles ranging in size D^* from a single voxel to $n = D^{*2}$ voxels, generate a sequence of patterns that tessellate the selected central region of the cylinder with a checkerboard of non-overlapping squares of size D^* . Terminate the sequence of patterns when the size of the tiles becomes too large to obtain a statistically significant number of tiles. It is recommended that the minimum number of tiles is about 25. See Table 2 for suggested maximum tile sizes. The tile pattern covers about one third of the cylinder slice in diameter. In each tile there is an average voxel value μ_i (D^*). NOTE 2—In this specific example, there are k = 24 tiles T_i of size $D^* = 3$, containing n = 9 voxels.

FIG. 3 Creating Tile Pattern for the CDF Determination