# INTERNATIONAL STANDARD 

ISO

## Steel castings for pressure purposes

Pièces moulées en acier pour service sous pression
iTeh STANDARI PREVIIEW (standards.iteh.ai)

## ISO 4991:1994

https://standards.iteh.ai/catalog/standards/sist/3e7d60bc-b370-4687-bba7-

## Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by atleast $75 \%$ of the member bodies casting VIEW
a vote. a vote.
International Standard ISO 4991 was prepared by Gechnical Committee ISO/TC 17, Steel, Subcommittee SC 11, Steel castings.

Annex A of this International Standard is for information onlys/sist/3e7d60bc-b370-4687-bba7-
d9fb9f1 69ec/iso-4991-1994

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## Introduction

The national standards comparable with this International Standard are different not only in details but also in their basic technical concept, because of different codal requirements. In particular this applies to the following points.
a) Some national standards only specify the verification of mechanical properties for a 28 mm thick standard test block which has been heat treated under the same conditions as the casting, independent of the actual casting thickness. In these cases, the tensile test only checks the quality of the steel and heat treatment and not the actual casting properties. The influence of thickness on mechanical properties or thickness limitations for the use of the steels are considered in the

## iTelh ST design codes. Otherpationat standards require the verification of me- 

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b) Some national standards specify an impact test for room temperature and elevated temperature grades. Others specify only the reduction https://standards.iteh of area determined by the tensile test. ba7-
c) Many national standards
precify minimum elevated temperature proof-stress values for the elevated temperature grades. Others consider the influence of the elevated temperature in the design rules.

In order to make this International Standard acceptable for a sufficient number of ISO member bodies, it was necessary to give supplementary or alternative requirements.

It is expected that the attempts to harmonize the codes for boilers and pressure vessels will make a future revision of this International Standard more consistent when considering the material requirements for steel castings.

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ISO 4991:1994
https://standards.iteh.ai/catalog/standards/sist/3e7d60bc-b370-4687-bba7-d9fb9fl69ec/iso-4991-1994

## Steel castings for pressure purposes

## 1 Scope

1.1 This International Standard covers steel castings used for pressure purposes. It includes materials which are used for the manufacture of components subject to pressure vessel codes (see ISO/R 831, ISO 2694 and ISO 5730) and for other pressure containing components not subject to codal requirements.
iTeh STAND ARDIDS 5730:1992. SStationary shell boilers of welded construction (other than water-tube boilers).
1.2 In cases where castings are produced byweld-ds.iteh.ai) ing together component parts, this International Standard does not cover the welding process orsthe properties of the weldments://standards.iteh ai/catalog/standards/sis Unildss otherwise specified in this International Stand9fb9fl 6f9ec/iso-49 dard, materials supplied according to this International Standard shall conform to the requirements of ISO 4990.
ISO 2605-2:1976, Steel products for pressure purposes - Derivation and verification of elevated temperature properties - Part 2: Proof stress of austenitic steel products.

ISO 2694:- ${ }^{11}$, Pressure vessels.
ISO 4990:1986, Steel castings - General technical delivery requirements.

## 3 General delivery requirements

The following standards contain provisions which, through reference in this text, constitute provisions of this International Standard. At the time of publication, the editions indicated were valid. All standards are subject to revision, and parties to agreements based on this International Standard are encouraged to investigate the possibility of applying the most recent editions of the standards indicated below. Members of IEC and ISO maintain registers of currently valid International Standards.

ISO 783:1989, Metallic materials - Tensile testing at elevated temperature.

ISO 831:1968, Rules for construction of stationary boilers.

ISO 2605-1:1976, Steel products for pressure purposes - Derivation and verification of elevated temperature properties - Part 1: Yield or proof stress of carbon and low alloy steel products.

## 4 Ordering

In addition to the indications for ordering given in ISO 4990, the following is to be observed.

Alternative delivery conditions are covered by 5.2 , 8.2, 9.1.2, 9.2.2.1 and 10.1. If the purchaser cannot $8.2,9.1 .2,9.2 .2 .1$ and 10.1. If the purchaser cannot
leave the choice between the different conditions to the manufacturer, he shall indicate the required conditions in the enquiry and order.

## 5 Conditions of manufacture

### 5.1 Steelmaking process

The steel shall be produced by the open hearth or electric process, or one of the basic oxygen processes and this may be followed by separate degassing or refining.

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### 5.2 Heat treatment

5.2.1 The type of heat treatment shall be as indicated in table 1. Where more than one type of heat treatment is given for the grade ordered, the choice is left to the discretion of the manufacturer, unless otherwise specified by the purchaser.
5.2.2 The heat-treatment temperatures shall be as indicated in table 1.

Unless otherwise agreed, alternative temperatures are permitted, provided that all specified property values are complied with.

### 5.3 Repairs

Cavities resulting from the removal of unacceptable discontinuities and repair welds (see note 1) shall be inspected according to the same non-destructive testing criteria as the relevant part of the casting.

NOTE 1 Within this International Standard, the term "repair welding" indicates welding operations which are carried out by the founder during the manufacturing process, in order to comply with the quality requirements of the casting.

## 9 Testing and inspection

### 9.1 Certificates

9.1.1 Castings delivered according to this International Standard shall be supplied with an inspection rortifinato and chall ennconcoantlo, ho enonifinall, in spected and tested.
9.1.2 Unless an inspection certificate signed by the purchaser or the representative of a body named by him (ICP) is ordered, the inspection certificate signed by the representative of the qualified department of the works (IC) is to be delivered.

### 9.1.3 The inspection certificate shall include

a) the results of all elements specified in table 1 , provided by the manufacturer;
b) the results of the mechanical tests required by 9.2.2;
c) a statement of the results of the visual inspection and dimensional checks;
(standard ${ }_{d}$ if any additional tests and inspections were agreed upon, the results or statements of the results of these additional tests and inspections.
steel shall conform to the chemical composition requirements given in table 1. (For check-analysis see footnote 2 to table 1.)
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### 9.2 Mechanical tests

### 9.2.1 Formation of lots

9.2.1.1 In the case of castings weighing 1000 kg or less, the delivery shall be subdivided into lots covering castings of the same type from the same cast having undergone the same heat treatment. (See 9.1 of ISO 4990:1986.)

The weight of a test lot shall not be greater than 5000 kg .
9.2.1.2 In the case of castings weighing more than 1000 kg , each individual casting shall be regarded as

### 9.2.2 Test to be carried out

9.2.2.1 Steel used for castings shall conform to the mechanical property requirements given in table 1.
9.2.2.1.1 For the room temperature and elevated temperature grades, either area reduction or impact strength shall be determined and shall conform to the requirements prescribed for the grade in table 1. The
choice of test will be at the discretion of the manufacturer, unless the conditions of 11.3 or 11.5 are specified by the purchaser at the time of the order.
9.2.2.2 For the low temperature grades, three impact tests shall be carried out at the temperature indicated in table 1 and shall be evaluated in accordance with 6.2.2.3.2 of ISO 4990:1986.
9.2.2.3 If a verification of the elevated temperature proof-stress values is required, this may be carried out in accordance with supplementary requirements 11.6 or 11.7.

## 10 Marking

10.1 If not otherwise agreed at the time of inquiry and order, the castings shall be legibly marked to show
a) the symbols of the manufacturer;
b) symbols, letters or numbers which relate the certificated test, test pieces and products to each other.
use with the specification are listed below, by title only.

From ISO 4990:1986

### 9.1.2 Reporting of the steel making process

### 9.1.3 Agreed manufacturing procedure

### 9.1.4 Dividing up the cast

### 9.1.6 Mass and tolerance on mass

### 9.3 Chemical analysis for residual elements

### 9.4.4.2 Lateral expansion

### 9.4.4.3 Percentage of shear area

### 9.6.1 Test blocks representative of the castings

If test blocks with the ruling thickness $T$ of the casting are ordered, instead of the 28 mm thick standard test blocks, or if the test pieces are to be taken from the casting, and if in these cases heat-treatment conditions are, within the limits given in table 1, left to the discretion of the manufacturer, the mechanical properties given in table 1 shall apply up to the ruling thickness ogiven in table 2.
10.2 Except as indicated in 10.3, the Sidentification d. marks shall be stamped or cast on each piece in a location and a manner to be designated by thelpur- $991: 199$ chaser. https//standards.iteh.ai/catalog/standards/s d9fb9fl 6f9ec/iso-49
10.3 Small castings may be batched and the identification marks stamped on the label attached to each

## 11 Supplementary requirements

### 11.1 General

Additional supplementary requirements suitable for use with the specifications of this International Standard, at the option of the purchaser, are described below. One or more of the supplementary requirements indicated below may be included in the purchaser's order or contract. When so included, a supplementary requirement shall be as important as the body of the specification. Details of supplementary requirements which are not fully described shall be agreed upon by the purchaser and the supplier.

### 11.2 List of optional supplementary requirements

A list of standardized supplementary requirements to be used at the option of the purchaser is described in ISO 4990. Those which are considered suitable for

### 9.7.2 Details of the treatment

9.8.1 ${ }^{\text {Prior }}$ agreement relating to major repair welds

### 9.8.2 Weld maps (sketches)

### 9.9.2 Magnetic particle inspection

### 9.9.3 Radiographic inspection

### 9.9.4 Ultrasonic inspection

### 9.10.1 Intergranular corrosion test

### 9.10.3 Pressure-tightness

### 11.3 Measurement of the reduction in area

The minimum values for the reduction in area given in table 1 are mandatory.

### 11.4 Test on samples with additional heat treatment

One additional sample per test lot, selected and prepared as described in 9.2 , shall be subjected to an additional heat treatment and to the same tests as the samples which have not undergone the additional
heat treatment. The details of the additional heat treatment and the properties to be obtained shall be agreed upon by the parties concerned at the time of enquiry and order.

### 11.5 Measurement of the impact energy at rnnm tamnarat.irn

The minimum values for the impact energy at room temperature given in table 1 are mandatory.

### 11.6 Verification of the elevated temperature proof-stress properties by specific testing acceptance tests

The proof-stress properties shall be verified by specific tests to be carried out in accordance with

ISO 783 at one of the temperatures given in table 1 . The relevant temperature and, if 9.2.1 does not apply for these tests, the formation of lots shall be agreed upon by the interested parties.

### 11.7 Verification of the elevated temperature proof-stress properties bv non-specitic tests

The elevated temperature proof-stress properties shall be verified by the presentation of statistical assistance, preferably in accordance with ISO 2605-1 or ISO 2605-2.

### 11.8 Individual testing

Each individual casting shall be regarded as a separate test lot.

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Table 1 - Chemical composition (cast analysis), mechanical properties at room temperature of the 28 mm thick reference test block in the heat-treated condition

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Heat treatment ${ }^{5}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | $(S$ | $\tan$ |  | $d s$ $1091 \cdot 19$ | iteh <br> 194 | ii) |  | $\sim$ | i |  | - | $\checkmark$ |  |  |  | $\checkmark$ |  |
| hittps://standards.iteh.ai/catalog/standards/sist/3e7d60bc-b370-Unalloyed steels |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| C23-45A | <0,25 | <0,60 | <1,20 | 0,035 | 0,035 | d9fb9 | fl 6f9e | /iso-4 | ¢91-199 | 240 | $\begin{gathered} 450 \\ \text { to } \\ \text { to } \end{gathered}$ | 22 | 35 | 27 | - |  | $\begin{gathered} A \\ N(+T) \\ (Q+T) \end{gathered}$ | 890 to 980 890 to 980 890 to 980 | f a i | 600 to 700 600 to 700 | - |
| C23-45AH | <0,25 | <0,60 | <1,20 | 0,035 | 0,035 | - | - | - | - | 240 | $\begin{aligned} & 450 \\ & \text { to } \\ & 600 \end{aligned}$ | 22 | 35 | 27 | - |  | N $\left(+T^{10)}\right.$ $0+T$ | $\begin{aligned} & 890 \text { to } 980 \\ & 890 \text { to } 980 \end{aligned}$ | $\stackrel{\text { a }}{ }$ | $\begin{aligned} & 600 \text { to } 700 \\ & 600 \text { to } 700 \end{aligned}$ | ${ }_{\text {a }}^{\text {a, }} \mathrm{f}$ |
| C23-45B | <0,20 | <0,60 | $\begin{gathered} 1,00 \\ \text { to } \\ 1,60 \end{gathered}$ | 0,035 | 0,035 | - | - | - | - | 240 | $\begin{aligned} & 450 \\ & \text { to } \\ & \text { to } \end{aligned}$ | 22 | 35 | 45 | - |  | $\begin{gathered} A \\ N(+T) \\ (Q+T) \end{gathered}$ | 890 to 980 890 to 980 890 to 980 | f a i | 600 to 700 600 to 700 |  |
| C23-45BH | <0,20 | <0,60 | $\begin{gathered} \begin{array}{c} 1,00 \\ \text { to } \\ 1,6 \end{array} \end{gathered}$ | 0,035 | 0,035 | - | - | - | - | 240 | $\begin{gathered} 450 \\ \text { to } \\ 60 \end{gathered}$ | 22 | 35 | 45 | - |  | $\mathrm{N}+\mathrm{T})$ $0+\mathrm{T}$ | $\begin{aligned} & 890 \text { to } 980 \\ & 890 \text { to } 980 \end{aligned}$ | ${ }^{\text {a }}$ | $\begin{aligned} & 600 \text { to } 700 \\ & 600 \text { to } 700 \end{aligned}$ |  |
| C23-45BL | <0,20 | <0,60 | $\begin{gathered} 1,00 \\ \text { to } \\ 1,60 \end{gathered}$ | 0,030 | 0,030 | - | - | - | - | 240 | $\begin{gathered} 450 \\ \text { to } \\ 600 \end{gathered}$ | 22 |  | - | -40 | 27 | $(N+T)$ $0+\mathrm{T}$ | $\begin{aligned} & 890 \text { to } 980 \\ & 890 \text { to } 980 \end{aligned}$ | a | $\begin{aligned} & 600 \text { to } 700 \\ & 600 \text { to } 700 \end{aligned}$ | $\stackrel{\mathrm{a}, \mathrm{f}}{\mathrm{a}} \mathrm{f}$ |
| C26-52 | $\begin{gathered} <0,25 \\ 111,121 \end{gathered}$ | < 0,60 | $\begin{gathered} <1,20 \\ 111,121 \end{gathered}$ | 0,035 | 0.035 | - | - | - | - | 280 | $\begin{gathered} 520{ }^{133} \\ \text { to } \\ 670 \\ \hline \end{gathered}$ | 18 | 30 | 35 | - | - | $\begin{gathered} \mathrm{A} \\ \mathrm{~N}+\mathrm{T}) \\ (\mathrm{Q}+\mathrm{T}) \end{gathered}$ | 890 to 980 890 to 980 890 to 980 | f a i | $\begin{aligned} & 600 \text { to } 700 \\ & 600 \text { to } 700 \end{aligned}$ |  |
| C26-52H | $\begin{gathered} <0,25 \\ 111,122 \end{gathered}$ | <0,60 | $\begin{gathered} \mid<1,20 \\ 111,12 \mid \end{gathered}$ | 0,035 | 0,035 | - | - | - | - | 280 | $\begin{gathered} 520^{131} \\ \text { to } \\ 670 \\ \hline \end{gathered}$ | 18 | 30 | 35 | - | - | $\begin{aligned} & \mathrm{N}+\mathrm{T})^{10)} \\ & \mathrm{O}+\mathrm{T} \end{aligned}$ | 890 to 980 890 to 980 | a | $\begin{aligned} & 600 \text { to } 700 \\ & 600 \text { to } 700 \end{aligned}$ | a, f $\mathrm{a}, \mathrm{f}$ |
| C26-52L | $\begin{gathered} <0,25 \\ 11) \end{gathered}$ | <0,60 | $\begin{gathered} <1,20 \\ 111 \end{gathered}$ | 0,030 | 0,030 | - | - | - | - | 280 | $\begin{gathered} \hline 5200^{131} \\ \text { to } \\ 670 \\ \hline \end{gathered}$ | 18 |  | - | -35 | 27 | $(N+T)$ $0+T$ | $\begin{aligned} & 890 \text { to } 980 \\ & 890 \text { to } 980 \end{aligned}$ | a | $\begin{aligned} & 600 \text { to } 700 \\ & 600 \text { to } 700 \end{aligned}$ | a, f $\mathrm{a}, \mathrm{f}$ |
| Alloyed ferritic and martensitic steels |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| C28H | $\begin{gathered} 0,15 \\ \text { to } \\ 0,2 \end{gathered}$ | $\begin{gathered} 0,30 \\ \text { to } \\ 0,60 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 0,50 \\ \text { to } \\ 1,00 \\ \hline \end{gathered}$ | 0,035 | 0,035 | <0,30 | $\begin{gathered} 0,40 \\ \text { to } \\ 0,60 \end{gathered}$ | - | - | 250 | $\begin{gathered} 450 \\ \text { to } \\ 600 \\ \hline \end{gathered}$ | 21 | 35 | 25 | - |  | $\begin{aligned} & N+T \\ & 0+T \end{aligned}$ | $\begin{aligned} & 900 \text { to } 960 \\ & 900 \text { to } 960 \end{aligned}$ | a | 630 to 710 630 to 710 | $\begin{aligned} & a, f \\ & a, f \end{aligned}$ |
| C31L | <0,29 | $\begin{gathered} 0,30 \\ \text { to } \\ 0,60 \end{gathered}$ | $\begin{gathered} 0,50 \\ \text { to } \\ 0,80 \end{gathered}$ | 0,030 | 0,030 | $\begin{gathered} 0,90 \\ \text { to } \\ 1.20 \end{gathered}$ | $\begin{gathered} 0,15 \\ \text { to } \\ 0.30 \end{gathered}$ | - | - | 370 | $\begin{aligned} & 550 \\ & \text { to } \\ & 70 \end{aligned}$ | 16 | 30 | - | -45 | 27 | ( $\mathrm{N}+\mathrm{T}$ ) | $\begin{aligned} & 850 \text { to } 910 \\ & 850 \text { to } 910 \end{aligned}$ | $\stackrel{\text { a }}{ }$ | $\begin{aligned} & 640 \text { to } 690 \\ & 640 \text { to } 690 \end{aligned}$ | a, ${ }_{\text {a }} \mathrm{f}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


|  | Chemical composition [\% (m/m) ${ }^{11,}$, 2) |  |  |  |  |  |  |  |  | Mechanical properties at room temperature ${ }^{3 /}$ |  |  |  |  |  |  | Heat treatment ${ }^{5 /}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| designation | C | Si | $\mathbf{M n}$ |  | S max. | Cr | Mo | $\mathrm{Ni}$ | Others | $\begin{gathered} R_{\mathrm{e}}{ }^{6)} \\ \text { min. } \\ \mathrm{N} / \mathrm{mm}^{2} \end{gathered}$ | $\begin{gathered} R_{\mathrm{m}} \\ \mathrm{~N} / \mathrm{mm}^{2} \end{gathered}$ |  | $\begin{gathered} Z^{71} \\ \text { min. } \\ \% \end{gathered}$ | $\left\|\begin{array}{c} K V^{71,41} \\ \min . \\ J \end{array}\right\|$ | $\begin{aligned} & \mathrm{KL} \\ & \text { at } \\ & { }^{\circ} \mathrm{C} \end{aligned}$ | 4) min. J | Symbol ${ }^{\text {8 }}$ | Austenitizing temperature ${ }^{\circ} \mathrm{C}$ | Cooling condition ${ }^{9}$ | Tempering temperature ${ }^{\circ} \mathrm{C}$ | Cooling condition ${ }^{91}$ |
| H-CIN Alloyed ferritic and martensitic steels |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| C 32 H | $\begin{array}{\|c} 0,10 \\ \text { to } \\ 0,20^{10)} \end{array}$ | $\begin{gathered} 0,30 \\ \text { to } \\ 0,60 \end{gathered}$ | $\begin{gathered} 0,50 \\ \text { to } \\ 0,80 \end{gathered}$ | 0,035 | $0,035$ | $\begin{gathered} 2,00 \\ \text { to } \\ 1,50 \end{gathered}$ | $\begin{gathered} \hline 0,45 \\ \text { to } \\ 0,65 \end{gathered}$ | CS. | tel | $2_{290}$ | $\begin{gathered} 490 \\ \text { to } \\ 640 \end{gathered}$ | 18 | 35 | 27 | - | - | $\begin{aligned} & N+T \\ & 0+T \end{aligned}$ | $\begin{aligned} & 900 \text { to } 960 \\ & 900 \text { to } 960 \end{aligned}$ | $\begin{aligned} & \text { a } \\ & \text { i } \end{aligned}$ | $\begin{aligned} & 650 \text { to } 720 \\ & 650 \text { to } 720 \end{aligned}$ | $\begin{aligned} & a, f \\ & a, f \end{aligned}$ |
| C33H | $\begin{gathered} 0,10 \\ \text { to } \\ 0,17 \end{gathered}$ | $\begin{gathered} 0,30 \\ \text { to } \\ 0,60 \\ \hline \end{gathered}$ | $\begin{array}{\|c\|} \hline 0,40 \\ \text { to. } \\ \hline 0,70 \\ \hline \end{array}$ | 0,035 | 0,035 | $\begin{array}{\|c\|} \hline 0,30 \\ \text { ito } \\ \text { to } 60 \\ 0,60 \end{array}$ | $I 0,404$ 0 to 0,60 | $991: 19$ $<0,40$ | $\begin{aligned} & \mathrm{v}: 0,22 \\ & \mathrm{st} / 3 \mathrm{e} \text { to } \\ & 0,32 \end{aligned}$ | $\mathrm{pbc}^{320} 37$ | $\begin{gathered} 500 \\ 0-40 \\ 650 \end{gathered}$ | pba ${ }^{17}$ | 30 | 13 | - | - | $N+T$ | 950 to 1000 | a | 680 to 750 | a, f |
| C34AH | $\begin{gathered} 0,08 \\ \text { to } \\ 0,15 \end{gathered}$ | $\begin{gathered} 0,30 \\ \text { to } \\ 0,60 \end{gathered}$ | $\begin{gathered} 0,50 \\ \text { to } \\ 0,80 \\ \hline \end{gathered}$ | 0,035 | 0,035 | $\begin{gathered} 2,00 \\ \text { to } \\ 2,50 \end{gathered}$ | $\begin{gathered} 0,90 \\ \text { to } \\ 1,20 \end{gathered}$ | $\begin{gathered} 1 \mathrm{SO}=-4 \\ - \end{gathered}$ | $\begin{gathered} -1994 \\ - \end{gathered}$ | 280 | $\begin{gathered} 510 \\ \text { to } \\ 660 \\ \hline \end{gathered}$ | 18 | 35 | 25 | - | - | $N+T$ | 930 to 970 | a | 680 to 750 | a, f |
| C34BH | $\begin{gathered} 0,13 \\ \text { to } \\ 0,20 \end{gathered}$ | $\begin{gathered} 0,30 \\ \text { to } \\ 0,60 \end{gathered}$ | $\begin{gathered} 0,50 \\ \text { to } \\ 0,80 \end{gathered}$ | 0,035 | 0,035 | $\begin{gathered} 2,00 \\ \text { to } \\ 2,50 \end{gathered}$ | $\begin{gathered} 0,90 \\ \text { to } \\ 1,20 \end{gathered}$ | - | - | 390 | $\begin{gathered} 600 \\ \text { to } \\ 750 \end{gathered}$ | 18 | 35 | 40 | - | - | $\begin{gathered} (\mathrm{N}+\mathrm{T}) \\ \mathrm{Nac}_{\mathrm{ac}}+\mathrm{T} \\ \mathrm{Q}+\mathrm{T} \end{gathered}$ | $\begin{aligned} & 930 \text { to } 970 \\ & 930 \text { to } 970 \\ & 930 \text { to } 970 \end{aligned}$ | $\begin{gathered} \mathrm{a} \\ \mathrm{ac} \\ \text { । } \end{gathered}$ | $\begin{aligned} & 680 \text { to } 750 \\ & 680 \text { to } 750 \\ & 680 \text { to } 750 \end{aligned}$ | $\begin{aligned} & a, f \\ & a, f \\ & a, f \end{aligned}$ |
| C34BL | <0,20 | $\begin{gathered} 0,30 \\ \text { to } \\ 0,60 \end{gathered}$ | $\begin{gathered} 0,50 \\ \text { to } \\ 0,80 \end{gathered}$ | 0,030 | 0,030 | $\begin{gathered} 2,00 \\ \text { to } \\ 2,50 \end{gathered}$ | $\begin{gathered} 0,90 \\ \text { to } \\ 1,20 \end{gathered}$ | - | - | 390 | $\begin{gathered} 600 \\ \text { to } \\ 750 \end{gathered}$ | 18 | - | - | 50 | 27 | $\begin{gathered} (N+T) \\ \left(N_{a c}+T\right) \\ Q+T \end{gathered}$ | $\begin{aligned} & 930 \text { to } 970 \\ & 930 \text { to } 970 \\ & 930 \text { to } 970 \end{aligned}$ | $\begin{gathered} \mathrm{a} \\ \mathrm{ac} \\ \text { । } \end{gathered}$ | 680 to 750 680 to 750 680 to 750 | $\begin{aligned} & \mathrm{a}, \mathrm{f} \\ & \mathrm{a}, \mathrm{f} \\ & \mathrm{a}, \mathrm{f} \\ & \hline \end{aligned}$ |
| C35BH | $\begin{gathered} 0,13 \\ \text { to } \\ 0,20 \\ \hline \end{gathered}$ | $\begin{gathered} 0,30 \\ \text { to } \\ 0,60 \\ \hline \end{gathered}$ | $\begin{gathered} 0,50 \\ \text { to } \\ 0,80 \\ \hline \end{gathered}$ | 0,035 | 0,035 | $\left\|\begin{array}{c} 1,20 \\ \text { to } \\ 1,60^{14)} \end{array}\right\|$ | $\begin{gathered} 0,90 \\ \text { to } \\ 1,20 \\ \hline \end{gathered}$ | 15) | $\begin{gathered} V: 0,15 \\ \text { to } \\ 0,35 \end{gathered}$ | 420 | $\begin{gathered} 590 \\ \text { to } \\ 740 \\ \hline \end{gathered}$ | 15 | 35 | 24 | - | - | $\begin{gathered} \mathrm{N}_{\mathrm{ac}}+\mathrm{T} \\ \mathrm{Q}+\mathrm{T} \end{gathered}$ | $\begin{aligned} & 940 \text { to } 980 \\ & 940 \text { to } 980 \end{aligned}$ | ac | $\begin{aligned} & 680 \text { to } 750 \\ & 680 \text { to } 750 \end{aligned}$ | $\begin{aligned} & a, f \\ & a, f \end{aligned}$ |
| C37H | $\begin{gathered} 0,12 \\ \text { to } \\ 0,19 \\ \hline \end{gathered}$ | <0,80 | $\begin{gathered} 0,50 \\ \text { to } \\ 0,80 \\ \hline \end{gathered}$ | 0,035 | 0,035 | $\begin{gathered} 4,00 \\ \text { to } \\ 6,00 \end{gathered}$ | $\begin{gathered} 0,45 \\ \text { to } \\ 0,65 \\ \hline \end{gathered}$ | - | - | 420 | $\begin{gathered} 630 \\ \text { to } \\ 780 \\ \hline \end{gathered}$ | 16 | 35 | 25 | - | - | $N+T$ | 930 to 990 | a | 620 to 750 | a, ${ }^{\dagger}$ |
| C 38 H | $\begin{gathered} 0,10 \\ \text { to } \\ 0,17 \end{gathered}$ | <0,80 | $\begin{gathered} 0,50 \\ \text { to } \\ 0,80 \end{gathered}$ | 0,035 | 0,035 | $\begin{gathered} 8,00 \\ \text { to } \\ 10,0 \\ \hline \end{gathered}$ | $\begin{gathered} 1,00 \\ \text { to } \\ 1,30 \end{gathered}$ | - | - | 420 | $\begin{gathered} 630 \\ \text { to } \\ 780 \end{gathered}$ | 16 | 35 | 20 | - | - | $N+T$ | 930 to 990 | a | 620 to 750 | a, f |
| C 39 CH | $\begin{gathered} 0,10 \\ \text { to } \\ 0,17 \end{gathered}$ | <0,80 | <1,00 | 0,035 | 0,035 | $\begin{gathered} 11,5 \\ \text { to } \\ 13,5 \\ \hline \end{gathered}$ | <0,50 | <1,00 | - | 450 | $\begin{gathered} 620 \\ \text { to } \\ 770 \\ \hline \end{gathered}$ | 14 | 30 | 20 | - | - | $N+T$ | 950 to 1050 | a | 620 to 750 | a |
| C39CNiH | $\begin{gathered} 0,05 \\ \text { to } \\ 0,10 \end{gathered}$ | <0,80 | $\begin{gathered} 0,40 \\ \text { to } \\ 0,80 \\ \hline \end{gathered}$ | 0,035 | 0,035 | $\begin{gathered} 11,5 \\ \text { to } \\ 13,0 \end{gathered}$ | $\begin{gathered} 0,20 \\ \text { to } \\ 0,50 \\ \hline \end{gathered}$ | $\begin{gathered} 0,80 \\ \text { to } \\ 1,80 \\ \hline \end{gathered}$ | - | 360 | $\begin{gathered} 540 \\ \text { to } \\ 690 \end{gathered}$ | 18 | 35 | 35 | - | - | $N+T$ | 1000 to $1050^{16)}$ | a | 650 to 720 | a, $\dagger$ |
| C39NiH | <0,08 | <1,00 | <1,50 | 0,035 | 0,035 | $\begin{gathered} 11,5 \\ \text { to } \\ 13,5 \end{gathered}$ | <1,00 | $\begin{gathered} 3,50 \\ \text { to } \\ 5,00 \end{gathered}$ | - | 550 | $\begin{gathered} 750 \\ \text { to } \\ 900 \end{gathered}$ | 15 | 35 | 45 | - | - | $N+T$ | 950 to 1050 | a | 570 to 620 | a, $\dagger$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| Steel type designation | Chemical composition [\% (m/m)] ${ }^{1), 2)}$ |  |  |  |  |  |  |  |  | Mechanical properties at room temperature ${ }^{3 /}$ |  |  |  |  |  |  | Heat treatment ${ }^{\text {5 }}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | C | Si | Mn |  |  | Cr | Mo | Ni | Others | $\begin{gathered} R_{\mathrm{e}}{ }^{61} \\ \mathrm{~min} . \\ {\mathrm{N} / \mathrm{mm}^{2}}^{2} \end{gathered}$ |  | $\begin{gathered} A \\ \min . \\ \% \end{gathered}$ | $\begin{gathered} Z^{7)} \\ \min . \\ \% \end{gathered}$ | $\begin{gathered} K V^{7,4)} \\ \min . \\ J \end{gathered}$ | K at ${ }^{\circ} \mathrm{C}$ | 4) <br> min. <br> J | Symbol ${ }^{\text {8) }}$ | Austenitizing temperature ${ }^{\circ} \mathrm{C}$ | Cooling condition ${ }^{9)}$ | Tempering temperature <br> ${ }^{\circ} \mathrm{C}$ | Cooling condition ${ }^{9)}$ |


| C39NiL | <0,08 | < 1,00 | < 1,50 | 0,030 | $0,030$ | $\begin{gathered} a_{11,5} \\ \text { to } \\ 13,5 \\ \hline \end{gathered}$ | $<1,00$ | $\begin{gathered} 3,50 \\ \text { to } \\ 500 \end{gathered}$ |  | 550 | $\begin{gathered} 750 \\ \text { to } \\ 900 \end{gathered}$ | 15 | - | - | -80 | 27 | $\begin{aligned} & \mathrm{Nac}_{\mathrm{ac}}+\mathrm{T} \\ & (\mathrm{~N}+\mathrm{T}) \end{aligned}$ | $\begin{aligned} & 950 \text { to } 1050 \\ & 950 \text { to } 1050 \end{aligned}$ | $\begin{gathered} \text { ac } \\ \text { a } \end{gathered}$ | $\begin{aligned} & 570 \text { to } 620 \\ & 570 \text { to } 620 \end{aligned}$ | $\begin{aligned} & a, f \\ & a, f \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{C4OH}$ | $\begin{gathered} 0,20 \\ \text { to } \\ 0,26 \end{gathered}$ | $\begin{gathered} 0,20 \\ \text { to } \\ 0,40 \end{gathered}$ | $\begin{gathered} 0,50 \\ \text { to } \\ 0,70 \end{gathered}$ | 0,035 | S0,035 | $\begin{aligned} & 11,3 \\ & \text { cta } \\ & \text { di2, } 39 \end{aligned}$ | $\begin{gathered} 1,00 \\ \text { to } \\ 10,200 \end{gathered}$ | 0,70 ar, 10 ist,00 | $\begin{aligned} & v=0,25 \\ & \text { to } \\ & 91-0,35 \end{aligned}$ | $b_{540} 37$ | 740 -40 880 | pa, $5^{-}$ | 20 | $21^{171}$ | - | - | $N+T$ | 1020 to 1070 | a | 680 to 750 | a, f |
| C43L | <0,14 | $\begin{gathered} 0,30 \\ \text { to } \\ 0,60 \end{gathered}$ | $\begin{gathered} 0,50 \\ \text { to } \\ 0,80 \end{gathered}$ | 0,030 | 0,030 | - | - | $\begin{gathered} 3,00 \\ \text { to } \\ 4,00 \end{gathered}$ | - | 300 | $\begin{gathered} 460 \\ \text { to } \\ 610 \end{gathered}$ | 20 | - | - | -70 | 27 | $Q+T$ | 820 to 870 | 1 | 590 to 660 | $a^{18)}$ |
| C43C1L | <0,24 | $\begin{gathered} 0,30 \\ \text { to } \\ 0,60 \end{gathered}$ | $\begin{gathered} 0,80 \\ \text { to } \\ 1,20 \end{gathered}$ | 0,030 | 0,030 | - | $\begin{gathered} 0,15 \\ \text { to } \\ 0,30 \end{gathered}$ | $\begin{gathered} 1,50 \\ \text { to } \\ 2,00 \end{gathered}$ | - | 380 | $\begin{gathered} 520 \\ \text { to } \\ 670 \end{gathered}$ | 20 | - | - | -35 | 27 | Q+T | 900 to 950 | 1 | 600 to 670 | $\mathrm{a}^{18)}$ |
| C43E2aL | <0,22 | <0,60 | $\begin{gathered} 0,40 \\ \text { to } \\ 0,80 \end{gathered}$ | 0,030 | 0,030 | $\begin{gathered} 1,35 \\ \text { to } \\ 2,00 \\ \hline \end{gathered}$ | $\begin{gathered} 0,35 \\ \text { to } \\ 0,60 \\ \hline \end{gathered}$ | $\begin{gathered} 2,50 \\ \text { to } \\ 3,50 \\ \hline \end{gathered}$ | - | 450 | $\begin{gathered} 620 \\ \text { to } \\ 800 \\ \hline \end{gathered}$ | 16 | - | - | -80 | 27 | $\begin{gathered} (N+T) \\ N_{a c}+T \\ Q+T \end{gathered}$ | 900 to 950 <br> 900 to 950 <br> 900 to 950 | $\begin{gathered} a \\ \mathrm{ac} \\ \mathrm{l} \end{gathered}$ | 580 to 650 <br> 580 to 650 <br> 580 to 650 | $\begin{aligned} & a^{18)} \\ & a^{18)} \\ & a^{18)} \end{aligned}$ |
| C43E2bL | <0,22 | <0,60 | $\begin{gathered} 0,40 \\ \text { to } \\ 0,80 \end{gathered}$ | 0,030 | 0,030 | $\begin{gathered} 1,50 \\ \text { to } \\ 2,00 \end{gathered}$ | $\begin{gathered} 0,35 \\ \text { to } \\ 0,60 \end{gathered}$ | $\begin{gathered} 2,75 \\ \text { to } \\ 3,90 \end{gathered}$ | - | 655 | $\begin{gathered} 800 \\ \text { to } \\ 950 \end{gathered}$ | 13 | - | - | -60 | 27 | $\begin{gathered} (N+T) \\ N_{a c}+T \\ Q+T \end{gathered}$ | $\begin{aligned} & 900 \text { to } 950 \\ & 900 \text { to } 950 \\ & 900 \text { to } 950 \end{aligned}$ | $\begin{gathered} \mathrm{a} \\ \mathrm{ac} \\ \mathrm{I} \end{gathered}$ | $\begin{aligned} & 580 \text { to } 650 \\ & 580 \text { to } 650 \\ & 580 \text { to } 650 \end{aligned}$ | $\begin{aligned} & a^{18)} \\ & a^{18!} \\ & a^{18)} \end{aligned}$ |


|  | 1 | 1 | 1 | 1 | 1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 1 | 1 | 1 | 1 |  |  |
|  | 흔 | ํ | 흔 | 흔 | 훌 | 후 |  |
|  | 8 <br>  <br>  <br> 0 <br> 0 |  | $\begin{aligned} & 8 \\ & \frac{8}{6} \\ & \vdots \\ & \text { g } \\ & \hline \end{aligned}$ | $\begin{aligned} & 8 \\ & \hline \frac{8}{2} \\ & 0 \\ & 0 \\ & \hline 8 \end{aligned}$ | $\begin{aligned} & 8 \\ & \hline \\ & 0 \\ & 0 \\ & \hline 8 \end{aligned}$ | $\frac{8}{8}$ |  |
|  | 0 | $\infty$ | $\infty$ | $\infty$ | $\infty$ | $\infty$ |  |
|  | 1 | 1 | 1 | ¢8 | 1 | 1 |  |
|  | 1 | 1 | 1 | $\begin{aligned} & \overline{\bar{N}} \\ & \stackrel{O}{8} \\ & \hline \end{aligned}$ | 1 | 1 |  |
|  | б | Ф | б | 1 | б | Ф |  |
|  | 1 | 1 | 1 | 1 | 1 | 1 |  |
|  | ¢ | - | ¢ | - | セึ | ¢ |  |
|  | 욱의 | 윤융 | 안ㄹ | ㄱ7ㄴㅇㅢ | 완웅 | \% ¢ 응 |  |
|  | $\stackrel{\circ}{\sim}$ | 은 | \% | 은 | 은 | $\stackrel{\circ}{\text { N }}$ |  |
|  | 1 | 1 | 1 | 1 |  | 1 |  |
|  |  | $0_{\infty}^{0} 9$ | 으의 |  | ¢운 | 운을 |  |
|  | 1 | 1 | 1 | 1 | 1 | $\stackrel{\mathrm{O}}{\mathrm{N}} \mathrm{P}$ ¢ |  |
|  | $\stackrel{0}{ }+\underset{\circ}{\circ}$ |  | $0$ | $\stackrel{0}{ }:+ \text { ì }$ | $\stackrel{0}{\infty} \circ \frac{0}{N}$ | $\stackrel{0}{ㅇ}$ |  |
|  | ¢ | 응 | ¢ | $\begin{aligned} & \text { 응 } \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { 응 } \\ & 0 \end{aligned}$ | - |  |
|  | - | \% | 20 | $\begin{aligned} & \text { O8 } \\ & 0 \end{aligned}$ | $\mathbf{L}_{0}^{2}$ | -180 |  |
|  | 8 N v | 8 V V | 8 N V | 8 N V | 8 N V | 8 N V |  |
|  | 8 N V | $\begin{aligned} & 8 \\ & \underset{N}{N} \\ & \text { v } \end{aligned}$ | 8 N v | 8 N V | $\xrightarrow{8}$ | 8 N V |  |
|  | O | - | 岕: | - | $\begin{aligned} & 8 \\ & 8 \\ & 0 \\ & 0 \end{aligned}$ | O-8 |  |
|  | \% | ¢ | - | $\stackrel{\rightharpoonup}{\text { G }}$ | 웅 | $\stackrel{5}{3}$ |  |


[^0]:    (C) ISO 1994

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[^1]:    1) To be published.
