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Standard Practice for Manufacturing Characterization of Digital Detector Arrays¹

This standard is issued under the fixed designation E2597/E2597M; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ε) indicates an editorial change since the last revision or reapproval.

1. Scope

1.1 This practice describes the evaluation of Digital Detector Arrays (DDAs), and assures that one common standard exists for quantitative comparison of DDAs so that an appropriate DDA is selected to meet NDT requirements.

1.2 This practice is intended for use by manufacturers or integrators of DDAs to provide quantitative results of DDA characteristics for NDT user or purchaser consumption. Some of these tests require specialized test phantoms to assure consistency among results among suppliers or manufacturers. These tests are not intended for users to complete, nor are they intended for long term stability tracking and lifetime measurements. However, they may be used for this purpose, if so desired.

NOTE 1-Further information on application of DDAs is contained in Guide E2736 and Practices E2698 and E2737.

1.3 The results reported based on this standard<u>practice</u> should be based on a group of at least three individual detectors for a particular model number.

1.4 <u>Units</u>—The values stated in either SI units or inch-pound units are to be regarded separately as standard. The values stated in each system are not necessarily exact equivalents; therefore, to ensure conformance with the standard, each system shall be used independently of the other, and values from the two systems shall not be combined.

1.5 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety safety, health, and health environmental practices and determine the applicability of regulatory limitations prior to use.

<u>1.6 This international standard was developed in accordance with internationally recognized principles on standardization</u> established in the Decision on Principles for the Development of International Standards, Guides and Recommendations issued by the World Trade Organization Technical Barriers to Trade (TBT) Committee.

2. Referenced Documents

2.1 ASTM Standards:²

E1316 Terminology for Nondestructive Examinations

E1815 Test Method for Classification of Film Systems for Industrial Radiography

E2002 Practice for Determining Total Image Unsharpness and Basic Spatial Resolution in Radiography and Radioscopy E2445 Practice for Performance Evaluation and Long-Term Stability of Computed Radiography Systems

¹ This practice is under the jurisdiction of ASTM Committee E07 on Nondestructive Testing and is the direct responsibility of Subcommittee E07.01 on Radiology (X and Gamma) Method.

Current edition approved Jan. 1, 2014Jan. 1, 2022. Published February 2014February 2022. Originally approved in 2007. Last previous edition approved in $\frac{20072014}{10.1520/E2597E2597M-14.10.1520/E2597M-22.}$

² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For Annual Book of ASTM Standards volume information, refer to the standard's Document Summary page on the ASTM website.



E2446 Practice for Manufacturing Characterization of Computed Radiography Systems

E2698 Practice for Radiographic Examination Using Digital Detector Arrays

E2736 Guide for Digital Detector Array Radiography

E2737 Practice for Digital Detector Array Performance Evaluation and Long-Term Stability

2.2 OtherISO Standards:³

ISO 7004 Photography—Industrial Radiographic Films—Determination of ISO Speed, ISO Average Gradient and ISO Gradients G2 and G4 When Exposed to X- and Gamma-Radiation

- <u>IEC 62220-1ISO 17636-2</u> <u>Medical Electrical Equipment Characteristics of Digital X-ray Imaging Devices Part 1: Determination</u> of the Detective Quantum Efficiency<u>Non-destructive Testing of Welds — Radiographic Testing — Part 2: X- and Gamma-ray</u> Techniques With Digital detectors
- ISO 10893-7 Non-destructive Testing of Steel Tubes Part 7: Digital Radiographic Testing of the Weld Seam of Welded Steel Tubes for the Detection of Imperfections

2.3 Other Standards:

EN 12681-2 Founding — Radiographic Testing — Part 2: Techniques With Digital Detectors⁴

IEC 62220-1 Medical Electrical Equipment Characteristics of Digital X-ray Imaging Devices Part 1: Determination of the Detective Quantum Efficiency⁵

3. Terminology

3.1 Definitions of Terms Specific to This Standard:

3.1.1 achievable contrast sensitivity (CSa)—(CSa), n—optimum contrast sensitivity (see Terminology E1316 for a definition of contrast sensitivity) obtainable using a standard phantom with an X-ray technique that has little contribution from scatter.

3.1.2 active DDA area-area, n-the size and location of the DDA, which is recommended by the manufacturer as usable.

3.1.3 *bad pixel—pixel, n*_a pixel identified with a performance outside of the specification range for a pixel of a DDA <u>DDA pixel</u> that does not conform to a specified performance as defined in 6.2.

3.1.4 *burn-in*—*burn-in*, *n*—change in gain of the scintillator that persists well beyond the exposure.

3.1.5 *calibration*—correction applied for the offset signal, and the non-uniformity of response of any or all of the X-ray beam, scintillator and the read-out structure.

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3.1.6 *contrast-to-noise ratio (CNR)*—quotient of the difference of the mean signal levels between two image areas and the standard deviation of the signal levels. As applied here, the two image areas are the step-wedge groove and base material. The standard deviation of the intensity of the base material is a measure of the noise. The CNR depends on the radiation dose and the DDA system properties.

3.1.7 *detector signal-to-noise ratio–normalized (dSNRn)*—the SNR is normalized for basic spatial resolution SRb as measured directly on the detector without any object other than beam filters in the beam path.

3.1.5 digital detector <u>DDA correction</u>, array <u>n</u>_(DDA) system—an electronic device that converts ionizing or penetrating radiation into a discrete array of analog signals which are subsequently digitized and transferred to a computer for display as a digital image corresponding to the radiologic energy pattern imparted upon the input region of the device. The conversion of the ionizing or penetrating radiation into an electronic signal may transpire by first converting the ionizing or penetrating radiation into visible light through the use of a scintillating material. These devices can range in speed from many seconds per image to many images per second, up to and in excess of real-time radioscopy rates (usually 30 frames per seconds). the process of subtracting the response of each pixel in absence of ionizing radiation (DDA offset image) and normalization of the gain of each pixel in the presence of ionizing radiation and the absence of a specimen (DDA gain image) and finally the replacement of the bad pixels by corrected values (bad pixel correction). The result is a corrected digital radiograph.

³ Available from American National Standards Institute (ANSI), 25 W. 43rd St., 4th Floor, New York, NY 10036, http://www.ansi.org.International Organization for Standardization (ISO), ISO Central Secretariat, Chemin de Blandonnet 8, CP 401, 1214 Vernier, Geneva, Switzerland, https://www.iso.org.

⁴ Available from https://www.en-standard.eu/.

⁵ Available from International Electrotechnical Commission (IEC), 3, rue de Varembé, Case postale-<u>1st floor, P.O. Box</u> 131, CH-1211, Geneva 20, Switzerland, http://www.iec.ch. https://www.iec.ch.

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- 3.1.6 *DDA gain <u>image</u>—<u>image</u>, <u>n</u>—image obtained with no structured object in the X-ray beam to <u>calibrate correct the pixel</u> response in a DDA.*
- 3.1.7 DDA offset image—image, n—image of the DDA in the absence of X-rays providing the background signal of all pixels.

3.1.8 <u>efficiency</u>—<u>efficiency</u>, <u>n</u>—<u>dSNRn</u><u>SNR</u>_N (see 3.1.73.1.16</u>) divided by the square root of the dose (in mGy) and mGy), this is used to measure the response of the detector at different beam energies and qualities.

3.1.9 frame rate-rate, n-number of frames acquired per second.

3.1.10 *GlobalLag1f* (*global lag 1st frame*)—*frame*), *n*—the ratio of mean signal value of the first frame of the DDA where the X-rays are completely off to the mean signal value of an image where the X-rays are fully on. This parameter is specifically for the integration time used during data acquisition.

3.1.11 GlobalLag1s (global lag 1 s)—s), n—the projected value of GlobalLag1f for an integration time of $\frac{1 \text{ se. 1 s.}}{1 \text{ se. 1 s.}}$

3.1.12 *GlobalLag60s (global lag 60 s)—s), n*—the ratio between mean graypixel value of an image acquired with the DDA after $60 \pm 60 \text{ s}$ where the X-rays are completely off, to same of an image where the X-rays are fully on.

3.1.16 gray value—the numeric value of a pixel in a DDA image. This is typically interchangeable with the terms pixel value, detector response, Analog-to-Digital Unit, and detector signal.

3.1.13 internal scatter radiation (ISR)—ratio (ISR), n—ratio of external primary radiation to scattered radiation within the detector.

3.1.14 $iSRbISO^{detector}$ material thickness limit (ISO-MTL), n—the interpolated basic spatial resolution of the detector indicates the limit determined similar to SMTR, but using as thicker wall thickness limit the value where the normalized SNR (SNR_N smallest geometric detail, which can be resolved spatially using a digital detector array with no geometric magnification.) is above 70 (basic technique) or 100 (enhanced technique).

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Note 1—It is equal to 1/2 of the measured detector unsharpness and it is determined from a digital image of the duplex wire IQI (Practice E2002), directly placed on the DDA without object. The *iSRb*^{detector} value is determined from the interpolated or approximated modulation depth of two, or several, neighbor wire pairs at 20 % modulation depth.

3.1.15 *lag-lag, n*-residual signal in the DDA that occurs shortly after the exposure is completed.

3.1.16 normalized signal-to-noise ratio of the detector- (SNR_N) , n—the SNR is normalized by the interpolated basic spatial resolution iSR_b^{detector} as measured directly on the detector without any object other than beam filters in the beam path.

3.1.17 *pixel value*, *n*—the numeric value of a pixel in the DDA image; this is typically interchangeable with the terms *gray value*, *detector response*, *Analog-to-Digital Unit*, or *detector signal*.

3.1.18 *phantom—phantom, n*_a part or item being used to quantify DDA characterization metrics.

3.1.21 *pixel value*—the numeric value of a pixel in a DDA image. This is typically interchangeable with the term gray value.

3.1.19 saturation gray value-pixel value, n-the maximum possible graypixel value of the DDA after offset correction.

3.1.23 *signal-to-noise ratio (SNR)*—quotient of mean value of the intensity (signal) and standard deviation of the intensity (noise). The SNR depends on the radiation dose and the DDA system properties.

3.1.20 specific material thickness range (SMTR)—(SMTR), n—the penetrated material thickness range within which a given image quality is achieved. As applied here, the minimum SNR in the image is achieved. The wall thickness range of a DDA, whereby

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DDA is limited for the thinner wall thickness is limited by 80 % of the maximum gray value of the DDAsaturation pixel value at this thickness and the thicker wall thickness by a SNR of 130:1 for 2 % contrast sensitivity and SNR of 250:1 for 1 % contrast sensitivity. Note that SNR values of 130:1 and 250:1 do not guarantee that 2 % and 1 % contrast sensitivity values will be achieved, but are being used to designate a moderate quality image, and a higher quality image respectively.130 (basic contrast sensitivity) or 250 for (enhanced contrast sensitivity).

NOTE 2-This is not related to the image quality requirement of 1-2T or 2-2T, because the spatial resolution is not considered.

3.1.21 *step-wedge—total image acquisition time, n*<u>a stepped block of a single metallic alloy with a thickness range that is to be manufactured in accordance with complete acquisition time of a DDA image, consisting of the effective exposure time of the integrated frames and the image transfer time between detector and computer including the detector read-out time, that is, from start of the exposure until 5.2. storage of the final image on the computer.</u>

4. Significance and Use

4.1 This practice provides a means to compare DDAs on a common set of technical measurements, realizing that in practice, adjustments can be made to achieve similar results even with disparate DDAs, given geometric magnification, or other industrial radiologic settings that may compensate for one shortcoming of a device.

4.2 A user <u>mustshould</u> understand the definitions and corresponding performance parameters used in this practice in order to make an informed decision on how a given DDA can be used in the target application.

4.3 The <u>factorsparameters</u> that will be evaluated for each DDA are: interpolated basic spatial resolution ($iSR_b^{detector}$), efficiency (Detector (normalized Detector SNR-normalized ($dSNRnSNR_N$) at 1 mGy, for different energies and beam qualities), achievable contrast sensitivity (CSa), specific material thickness range (SMTR), and ISO-MTL, image lag, burn-in, bad pixels distribution and <u>statistics and</u> internal scatter radiationratio (ISR).

4.4 Given that each of these parameters are discussed together in many of the following sections, the following list will be helpful in selecting the key sections for a given test as follows. It should be noted that other sections of the document are needed to establish the appropriate technique for the parameter under test. Note that for each parameter (test), the first section listed is typically an apparatus or gauge (if required), the second section listed are the standardized measurements, and the third section listed involves the analysis or computations:

4.4.1 For iSR_b detector, see 5.1, 7.7, 8.2 dards/sist/d17c7428-9450-47c3-9b35-f1289895585f/astm-e2597-e2597m-22

4.4.2 For Detector Efficiency, see 5.3, 7.8, 8.3.

4.4.3 For CSa, see 5.2, 7.9, 8.4.

4.4.4 For SMTR, see 5.2 (or 7.9, if already completed), 7.10, 8.5.

4.4.5 For ISO-MTL, see 5.2 (or 7.9, if already completed), 7.10, 8.6.

4.4.6 For Image Lag, see 7.11.1, 8.7.1.

4.4.7 For Burn-in, see 5.4, 7.11.2, 8.7.2.

4.4.8 For Bad Pixel Tests, see 6.2, 7.12, 8.8.

4.4.9 For ISR, see 5.4, 7.13, 8.9.

5. Apparatus

5.1 Duplex Wire Image Quality Indicator for $iSRb iSR_b^{detector}$ —The duplex wire quality indicator corresponds to the design specified in Practice E2002 for the measurement of $iSRb iSR_b^{detector}$, and not unsharpness.

5.2 Step-Wedge Image Quality Indicator—The wedge has six steps in accordance with the drawing provided in Fig. 1. The wedge



may be formed with built-in masking to avoid X-ray scatter and undercut. In lieu of built-in masking, the step-wedge may be inserted into a lead frame. The lead frame eanshould then extend another 25.4 mm [1 in.] about approximately 25 mm [1 in.] around the perimeter of the step-wedge, beyond the support. The A slight overlap of the lead support with the edges of the step-wedge (no more than 6 mm [-0.25 in.] approximately 6 mm [-0.25 in.]) assures a significantly reduced number of X-rays to leak-through of X-ray dose will leak through under the step-wedge that and will contaminate influence the data acquired on each step. The step-wedges shall be formed of threetwo different materials: Aluminum 6061, Titanium Ti-6A1-4V, and Inconel 718-7022 or Stainless Steel 316L, with a center groove in each step, as shown in Fig. 1. The dimensions of the wedges for the different materials are shown in Table 1.

- 5.3 *Filters for Measuring Efficiency of the DDA*—The following filter thicknesses ($\frac{5.3.1 5.3.75.3.1 5.3.7}{5.3.1 5.3.7}$) and alloys (5.3.8) shall be used to obtain different radiation beam qualities and are to be placed at the output of the beam. The tolerance for these thicknesses shall be $\pm 0.1 \text{ mm} [\pm 0.004 \text{ in.}]$.
 - 5.3.1 No external filter (50 kV).

- 5.3.2 30 mm [1.2 in.] aluminum (90 kV).
- 5.3.3 40 mm [1.6 in.] aluminum (120 kV).
- 5.3.4 3 mm [0.12 in.] copper (120 kV).
- 5.3.5 10 mm [0.4 in.] iron (160 kV).
- 5.3.6 8 mm [0.3 in.] copper (220 kV).
- 5.3.7 16 mm [0.6 in.] copper (420 kV].kV).

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TABLE 1 Dimension of the ThreeTwo Step-Wedges for ThreeTwo Different Materials Used as Image Quality Indicators in thisIn This

					Practice	•					
Material	Unit	А	B1	B2	B3	B4	B5	B6	С	D	E
Step-wedge (Inconel 718)	mm	35.0	1.25	2.5	5.0	7.5	10.0	12.5	175.0	70.0	35.0
Step-wedge (Steel SS 316L)	mm	35	1.5	3	6	9	12	15	175	70	35
Tolerance (±)	microns	200	25	25	38	38	38	38	200	200	200
5 % Groove	microns		63	125	250	375	500	625			
Tolerance (±)	microns		10	10	10	10	10	10			
Material	Unit	A	B1	B2	B3	B4	B5	B6	e	Ð	E
Step-wedge (Ti-6AI-4V)	mm	35.0	2.5	5.0	7.5	10.0	20.0	30.0	175.0	70.0	35.0
Tolerance (±)	microns	200	50	50	50	50	50	50	200	200	200
Tolerance (±)	μm	200	50	50	50	50	50	50	200	200	200
5 % Groove	microns		125	250	375	500	1000	1500			
5 % Groove	μm		75	150	300	450	600	750			
$\overline{\text{Tolerance } (\pm)}$	microns		10	10	10	10	10	10			
Tolerance (±)	μm		10	10	10	10	10	10			
Material	Unit	A	B1	B2	B3	B4	B5	B6	С	D	E
Step-wedge (Al-6061)	mm	35.0	10.0	20.0	40.0	60.0	80.0	100.0	175.0	70.0	35.0
Step-wedge (AI-7022)	mm	35	10	20	40	60	80	100	175	70	35
Tolerance (±)	microns	200	100	100	300	300	300	300	200	200	200
Tolerance (±)	um	200	100	100	300	300	300	300	200	200	200
5 % Groove	microns		500	1000	2000	3000	4000	5000			
5 % Groove	um		500	1000	2000	3000	4000	5000			
Tolerance (±)	microns		13	25	50	50	50	50			
Tolerance (±)	um		13	25	50	50	50	50			
The	values stated in	n SI units	above and	d inch-pou	ind units I	below are to be	regarded sepa	rately as stand	dard.		
Material	Unit	Α	B1	B2	B3	B4	B5	B6	С	D	E
Step-wedge (Inconel 718)	inch	1.4	0.05	0.1	0.2	0.3	0.4	0.5	6.9	2.8	1.4
Step-wedge (Steel SS 316L)	inch	1.40	0.06	0.12	0.24	0.36	0.48	0.60	6.9	2.8	1.4
Tolerance (±)	mils	8.0	1.0	1.0	1.5	1.5	1.5	1.5	8.0	8.0	8.0
Tolerance (±)	mils	8	2	2	2	2	2	2	8	8	8
5 % Groove	mils	-	2.5	4.9	9.8	14.8	19.7	24.6	_	_	-
5 % Groove	mils		6	12	24	36	48	60			
Tolerance (±)	mils		0.5	0.5	0.5	0.5	0.5	0.5			
Material	Unit	A	B1 /	B2	B3	B4	B5	• B6	С	D	E
Step-wedge (Ti-6AI-4V)	inch	1.4	0.1	0.2	0.3	0.4	0.8	1.2	6.9	2.8	1.4
Tolerance (±)	mils	8.0	2.0	2.0	2.0	2.0	2.0	2.0	8.0	8.0	8.0
5 % Groove	mils		4.9	9.8	14.8	19.7	39.4	59.1			
Tolerance (±)	mils		0.5	0.5	0.5	0.5	0.5	0.5			
Material	Unit	A	B1	B2	B3	B4	B5	B6	e	Ð	E
Step-wedge (AI-6061)	inch	1.4	0.4	0.8	1.6	2.4	3.1	3.9	6.9	2.8	1.4
Step-wedge (AI-7022)	inch	1.4	0.4	0.8	1.6	2.4	3.1	3.9	6.9	2.8	1.4
Tolerance (±)	mils	8.0	4.0	4.0	12.0	12.0	12.0	12.0	8.0	8.0	8.0
Tolerance (\pm)	mils	8	45	LIVI ₄ E2	39 12 E	259/12-22	12	12	8	8	8
5% Groove	mils/	ndarda	19.7	7,39.40	78.7	17 118.1 01	25 (157.50)	2054196.9%	$atm = 250^{\circ}$	7 - 250	17m 77
5 % Groove	mils		20	40	80	120	155	195			
Tolerance (±)	mils		0.5	1.0	2.0	2.0	2.0	2.0			
Tolerance (\pm)	mils		0.5	1	2	2	2	2			

5.3.8 The filters shall be placed directly at the tube window. The aluminum filter shall be composed of aAluminum 6061. 97 % purity or better. The copper shall be composed of 99.9 % purity or better. The iron filter shall be composed of Stainless Steel 304.316L. At minimum 3 of the above radiation qualities shall be used for the detector characterization.

NOTE 3—Radiation qualities in 5.3.2 and 5.3.3 are in accordance with DQE standard IEC62220-1, and radiation quality in 5.3.4 and 5.3.5 are in accordance with ISO 7004. Radiation qualityqualities in 5.3.6 isare used also in Test Method E1815, Practice E2445, and Practice E2446.

5.4 *Filters for Measuring, Burn-In and Internal Scatter <u>Radiation—Ratio—</u>The filters for measuring burn-in and ISR shall consist of a minimum 16 mm [0.6 in.] thick copper plate (5.3.7) 100 by 75 mm [4 by 3 in.] 100 mm by 75 mm [4 in. by 3 in.] with a minimum of one sharp edge. If the DDA is smaller than \frac{1515 \text{ cm}}{15 \text{ cm}} by \frac{15 \text{ cm}}{15 \text{ cm}} [5.9 in.] by 5.9 in.] use a plate that is dimensionally 25 % of the active DDA area.*

6. Calibration Detector Correction and Bad Pixel Standardization Classification

6.1 DDA <u>CalibrationCorrection</u> Method—Prior to qualification testing, the DDA shall be <u>calibratedcorrected</u> for offset, or <u>gain</u>, or <u>both</u>, <u>gain</u>, and <u>bad pixels</u> (see $\frac{3.1.103.1.7}{3.1.8}$) to generate corrected images per manufacturer's recommendation.

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It is important that the calibration<u>this correction</u> procedure be completed as would be done in practice during routine calibration<u>correction</u> procedures. This is to assure that data collected by manufacturers will closely match that collected when the system is entered into service.

6.2 *Bad Pixel <u>Standardization</u> <u>Classification</u> for DDAs—Manufacturers typically have different methods for correcting bad pixels. Images collected for qualification testing shall be corrected for bad pixels as per manufacturer's bad pixel correction procedure wherever required. In this section, a standardized nomenclature is presented. The following definitions enable classification of pixels in a DDA as bad or good types. The manufacturers are to use these definitions on a statistical set of detectors in a given detector type to arrive at "typical" results for bad pixels for that model. The identification and correction of bad pixels in a delivered DDA remains in the purview of agreement between the purchaser and the supplier.*

6.2.1 Definition and Test of Bad Pixels:

6.2.1.1 *Dead Pixel*—Pixels that have no response, or that give a constant response independent of radiation dose on the detector.

6.2.1.2 Over Responding Pixel—Pixels whose gray-values are greater than 1.3 times the median graypixel value of an area of a minimum of 21×21 pixels. This test is done on an offset corrected image.

6.2.1.3 Under Responding Pixel—Pixels whose gray-values are less than 0.6 times the median graypixel value of an area of a minimum of 21×21 pixels. This test is done on an offset corrected image.

6.2.1.4 *Noisy Pixel*—Pixels whose standard deviation in a sequence of 30 to 100 images without radiation is more than six times the median pixel standard deviation for the complete DDA.

6.2.1.5 Non-Uniform Pixel—Pixel whose value exceeds a deviation of more than ± 1 % of the median value of its 9×9 neighbor pixel. pixel in the corrected digital radiograph. The test should be performed on an image where the average graypixel value is at or above 75 % 80 % of the DDA's linear range. This test is done on an offset and gain corrected image.

6.2.1.6 *Persistence/Lag Pixel*—Pixel whose value exceeds a deviation of more than a factor of two of the median value of its 9×9 neighbors in the first image after X-ray shut down and are or exceeds six times the median noise value in the dark image (refer to 7.11.1).

6.2.1.7 Bad Neighborhood Pixel-Pixel, where all eight neighboring pixels are bad pixels, is also considered a bad pixel.

6.2.2 Types or Groups of Bad Pixels:

6.2.2.1 *Single Bad Pixel*—A single bad pixel is a bad pixel with only good neighborhood pixels.

6.2.2.2 *Cluster of Bad Pixels*—Two or more connected bad pixels are called a cluster. Pixels are called connected if they are connected by a side or a corner (eight-neighborhood possibilities). Pixels which do not have five or more good neighborhood pixels are called cluster kernel pixel (CKP) (Fig. 2). A pixel direct at the detector rim is not called CKP if it has three or more good neighbors, but a pixel in a detector corner with less than 2 good neighbors is called a CKP.

6.2.2.3 A cluster without any CKP is well correctable and is labeled an irrelevant cluster. The name of the cluster is the size of a rectangle around the cluster and number of bad pixels in the irrelevant cluster, for example, " 2×3 cluster4" (Fig. 2).

6.2.2.4 A cluster (excluding a bad line segment defined in 6.2.2.5) with CKP is labeled a relevant cluster. A line cluster with CKP is classified differently (example given below and demonstrated in Fig. 2). The name of the cluster is similar to the irrelevant cluster; with the exception that the prefix "rel" is added and the number of CKPs is provided as a suffix, for example, "rel3×4 cluster7-2", cluster7-2" (Fig. 2), where 7 is the total number of bad pixels and two are those in this group that are CKPs.

6.2.2.5 A bad line segment is a special cluster with ten or more bad pixels connected in a line (row or eolumn)<u>column</u>), where no more than 10 % of this line has adjacent bad pixels. If there are CKPs in the line segment, then the following rule is to be followed: As shown in Fig. 2b, a relevant cluster is located at the end of a bad line segment. The bad line segment is then separated from the relevant cluster. In this example, the bad line segment is a $\frac{1\times51 \text{ Line51}1\times24 \text{ line24}}{1\times24 \text{ line34}}$ and attached with a relevant cluster Rel4×3 cluster 8-5. rel3x3 cluster7-7 directly at the detector rim (at bottom of Fig. 2). Crossing bad lines are reported like two single separated lines with a C at the end as, for example, 1x24 line24C. There may be configurations where a single CKP exists for two connected line segments, which is considered as non-relevant.

											4																			
	sin	gle	ba	d pi	ixel			2×.	2 c	ust	er2		2×3			cluster4			rel3×4 cluster7-				-2				L			
		С	С	C				C	С	С				C	С	С	С				С	С	С	С	С	С				
		С	D	С				С	D	ΓĒ	C			С	D	D	C	С			С	D	C	С	D	С				Γ
		С	С	С				С	С	D	С			С	C	D	D	С			С	D	К	к	С	С				T
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FIG. 2 (2) Different Types of Bad Pixel Groups: Cluster, Relevant Cluster, and Bad Line. (b) Example of a Small Clusters, A Relevant Cluster And Bad Lines; At Bottom An Example of A Bad Line Segment Separated from aAttached To A Relevant Cluster at the End. The line Segment is a 1x51 Line51 and Attached to a Relevant Cluster rel 4x4 cluster 8-5. At The Detector Rim is Shown; The Line Segment Is A 1x24 line24 (Not Relevant), But Connected To A Relevant Cluster rel3x3 cluster7-7

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NOTE 4—The positions of finally detected bad pixels as described before are a snapshot, which represents the current state of the detector. Some pixels could behave only temporarily like bad pixels. Therefore, at a later bad pixel analysis, the positions of bad pixels may vary from the snapshot before. The agreed thresholds for bad pixels shall always relate only to the number and region and not to the specific position during a snapshot.

7. Procedure

7.1 Beam filtration shall be defined by the test procedure for each individual test. It is to be noted that intrinsic beam filters may be installed in the X-ray tube head. Where possible, those values should be obtained and listed.

7.2 For all measurements, the X-ray source to detector distance (SDD) shall be $\geq 1000 \text{ mm} [\sim 40 \text{ in.}], \geq 1000 \text{ mm} [\sim 40 \text{ in.}], unless specifically mentioned. The beam shall not interact with any other interfering object other than that intended, and shall not be considerably larger than the detector area through the use of collimation at the source.$

Note 3—The exposure times listed in this procedure can be obtained by any combination of extended exposures or multiple frames as available from the DDA. However, whichever is used, that information shall be recorded in the test report and the same DDA integration time (per frame) shall be used for all tests. In the following sections, where an image is required, this image shall be stored in a format that contains the full bit depth of the acquisition for later analysis.

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7.3 The geometric unsharpness shall be less than or equal to 5 % of the total unsharpness for the $iSR_b^{detector}$ measurements. This avoids additional unsharpness due to the finite size of the X-ray focal spot on the measurement of $iSR_b^{detector}$. See example below. e.g. 100 µm pixel size \rightarrow (equal to $iSR_b^{detector}$) and focal spot size maximum size: 2 mm

Duplex wire to active sensor area distance : distance: 2.5 mm

Source to Object distance : 1 000 Source-to-Object distance: 1000 mm

Maximum expected unsharpness: $2 mm / 1 000 mm \times 2.5 mm = 0.005 mm = 5 \mu m$

Maximum unsharpness due to the limited focal spot size in percent relative to $iSR_b^{detector}$: 5 %

7.4 Measurement parameters for each test shall be recorded using the data-sheet template provided in Appendix X1, Data Sheet (Input).

NOTE 5—The effective exposure times listed in this procedure can be obtained by any combination of extended single exposures or multiple frames as available from the DDA. However, whichever is used, that information shall be recorded in the test report and the same DDA integration time (per frame) shall be used for all tests, the total image acquisition time (including the read-out and image transfer time) should be noted too. In the following sections, where an image is required, this image shall be stored in a format that contains the full bit depth of the acquisition for later analysis.

7.5 All images shall be <u>calibrated_corrected</u> for offset and gain variations of the DDAs unless otherwise mentioned. Bad pixel correction using the manufacturer's correction algorithms also needs to be completed for all tests with the exclusion of the bad pixel identification testing (see 7.12 and 8.7).

7.6 All tests specified for a given DDA type need to be performed at the same internal detector settings such as gain and analog-digital conversion.

7.7 Measurement Procedure for Interpolated Basic Spatial Resolution (iSR_b^{detector}):

7.7.1 The test object to measure the $iSR_b^{detector}$ is the duplex wire gage (Practice E2002). It should be placed directly on the detector with an angle between 2° and 5° to the rows/columns of the detector. If a DDA has a non-isotropic pixel, two images shall be made, one with the duplex wire near parallel to the columns and one near parallel to the rows. No image processing shall be used other than gain/offset and bad pixel corrections.

Note 4—For the extended quality numbers (>15) listed in Table 2 as discussed in Section 9 there are no duplex wires defined in Practice E2002. A special gage will be needed with wire pairs smaller than 50 µm to report in this extended quality regime. Any other gages used to perform the measurement shall be documented along with the test results

7.7.2 The exposure shall be performed at a distance of $\ge \underline{of} \ge 1$ m [≥ 40 in.] using geometric unsharpness levels as specified in 7.3.

7.7.3 The measurement of the interpolated basic spatial resolution of the detector may depend on the radiation quality. For DDAs that can operate above 160 kV, the test shall be performed with 220 kV. A filter of up to 0.5 mm Copper in front of the tube port shall be used. For all other DDAs, the test shall be completed at 90 kV (no pre-filtering or a filter of up to 0.5 mm Copper in front of the tube port). (with no added pre-filter). The mA of the X-ray tube shall be selected such that the graypixel value of the object (the duplex wire gage) is between 50 % and 80 % of full saturation for that DDA. If this cannot be achieved, a SNR of \geq 100 shall be obtained. Frame integration is recommended to achieve the required SNR. If the graypixel value of 80 % of full saturation is exceeded, the source to DDA distance shall be increased until the required grey levelpixel value is reached.

NOTE 6—The intent of this test is to determine the achievable $iSR_b^{detector}$ obtainable from the DDA under test. In this regard, it is important that the quantum noise of the measurement be significantly reduced. This may involve capturing multiple frames at the graypixel values listed above to fall within the procedure listed in provide robust measurements.^{7.7}

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mGy Efficiency = SNR _N @ 1 mGv	- 120	00 200	@ 160 kV, 10 mm Fe	200	240 2	280 3	3	60	8 4	40	22	IS IS	00	0 64	0	<u>0</u> 720	260	800	840	880	920	096	1000	1040	1080	1120	1160	1200
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TABLE 2 Continued	0.8 0.63 0.5 0.4 0.32 0.25 0.16 0.13 0.1 0080 0.063 0.050 0.040 0.025 0.016 0.013 0.010	0,8 0,63 0,5 0,4 0,32 0,25 0,2 0,16 0,13 0,1 0,080 0,053 0,050 0,040 0,032 0,025 0,016 0,015 0,013 0,010	<u>0.8</u> 0.63 0.5 0.4 0.32 0.25 0.2 0.16 0.13 0.1 0.080 0.063 0.050 0.040 0.032 0.026 0.016 0.013 0.010	0 550 600 650 700 750 800 850 900 950 1000 1050 1100 1150 1200 1250 1300 1350 1400 1450 1500	<u>0 550 600 650 700 750 800 850 900 950 1000 1050 1100 1150 1200 1250 1300 1350 1400 1450 1500</u>	55 60 65 70 75 80 85 90 95 100 105 110 115 120 125 130 135 140 145 150	2 25 60 65 70 75 80 85 90 95 100 105 110 115 120 125 130 135 140 145 150	edge-step-wedge shall be used for measurement of Specific Material Thickness Range. edge-step-wedge shall be used for measurement of Specific Material Thickness Range. tess of the freenel plate shall be 7.5 mm to extend the wedge for the scale by 10 quality values. It to extend the wedge for the scale by 10 quality values. mm to extend the wedge for the scale by 10 quality values. It to extend the wedge for the scale
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