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Standard Test Methods for Deep Foundation Elements Under Static Axial Tensile Load[1]

This standard is issued under the fixed designation D3689/D3689M; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ε) indicates an editorial change since the last revision or reapproval.

1. Scope

1.1 The test methods described in this standard measure the axial deflection of an individual vertical or inclined deep foundation element or group of elements when loaded in static axial tension. These methods apply to all types of deep foundations, or deep foundation systems, as they are practical to test. The individual components of which are referred to herein as elements that function as, or in a manner similar to, drilled shafts; cast-in-place piles (augered cast-in-place piles, barrettes, and slurry walls); driven piles, such as pre-cast concrete piles, timber piles or steel sections (steel pipes or wide flange beams); or any number of other element types, regardless of their method of installation. Although the test methods may be used for testing single elements or element groups, the test results may not represent the long-term performance of the entire deep foundation system. A summary of the test methods is contained in Section 4.

1.2 This standard provides minimum requirements for testing deep foundation elements under static axial tensile load. Project plans, specifications, provisions, or any combination thereof may provide additional requirements and procedures as needed to satisfy the objectives of a particular test program. The engineer in charge of the foundation design, referred to herein as the foundation engineer, shall approve any deviations, deletions, or additions to the requirements of this standard. (Exception: the test load applies to the testing apparatus shall not exceed the rated capacity established by the engineer who designed the testing apparatus.)

1.3 Apparatus and procedures herein designated "optional" may produce different test results and may be used only when approved by the foundation engineer. The word "shall" indicates a mandatory provision, and the word "should" indicates a recommended or advisory provision. Imperative sentences indicate mandatory provisions.

1.4 The foundation engineer should interpret the test results obtained from the procedures of this standard to predict the actual performance and adequacy of elements used in the constructed foundation.

1.5 An engineer qualified to perform such work shall design and approve all loading apparatus, loaded members, and support frames. The foundation engineer shall design or specify the test procedures. The text of this standard references notes and footnotes which provide explanatory material. These notes and footnotes (excluding those in tables and figures) shall not be considered requirements of the standard. This standard also includes illustrations and appendices intended only for explanatory or advisory use.

1.6 *Units*—The values stated in either SI units or inch-pound units are to be regarded separately as standard. The values stated in each system may not be exact equivalents; therefore, each system shall be used independently of the other. Combining values from the two systems may result in non-conformance with the standard.

1.7 The gravitational system of inch-pound units is used when dealing with inch-pound units. In this system, the pound [lbf] represents a unit of force [weight], while the unit for mass is slug. The rationalized slug unit is not given, unless dynamic [F=ma] calculations are involved.

1.8 All observed and calculated values shall conform to the guidelines for significant digits and rounding established in Practice D6026. The procedure used to specify how data are collected, recorded and calculated in this standard are regarded as the industry standard. In addition, they are representative of the significant digits that should generally be retained. The procedures used do not consider material variation, purpose for obtaining the data, special purpose studies, or any considerations for the user's objectives; and it is common practice to increase or reduce significant digits of reported data to be commensurate with these considerations. It is beyond the scope of this standard to consider significant digits used in analysis methods for engineering data.

1.9 The method used to specify how data are collected, calculated, or recorded in this standard is not directly related to the accuracy to which the data can be applied in design or other uses, or both. How one applies the results obtained using this standard is beyond its scope.

1.10 *This standard offers an organized collection of information or a series of options and does not recommend a*

[1] These test methods are under the jurisdiction of ASTM Committee D18 on Soil and Rock and are the direct responsibility of Subcommittee D18.11 on Deep Foundations.

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specific course of action. This document cannot replace education or experience and should be used in conjunction with professional judgment. Not all aspects of this standard may be applicable in all circumstances. This ASTM standard is not intended to represent or replace the standard of care by which the adequacy of a given professional service must be judged, nor should this document be applied without consideration of a project's many unique aspects. The word "Standard" in the title of this document means only that the document has been approved through the ASTM consensus process.

1.11 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety, health, and environmental practices and determine the applicability of regulatory limitations prior to use.*

1.12 *This international standard was developed in accordance with internationally recognized principles on standardization established in the Decision on Principles for the Development of International Standards, Guides and Recommendations issued by the World Trade Organization Technical Barriers to Trade (TBT) Committee.*

2. Referenced Documents

2.1 *ASTM Standards:*[2]

D653 Terminology Relating to Soil, Rock, and Contained Fluids

D3740 Practice for Minimum Requirements for Agencies Engaged in Testing and/or Inspection of Soil and Rock as Used in Engineering Design and Construction

D5882 Test Method for Low Strain Impact Integrity Testing of Deep Foundations

D6026 Practice for Using Significant Digits and Data Records in Geotechnical Data

D6760 Test Method for Integrity Testing of Concrete Deep Foundations by Ultrasonic Crosshole Testing

D7949 Test Methods for Thermal Integrity Profiling of Concrete Deep Foundations

D8169/D8169M Test Methods for Deep Foundations Under Bi-Directional Static Axial Compressive Load

2.2 *ASME Standards:*[3]

ASME B30.1 Jacks

ASME B40.100 Pressure Gages and Gauge Attachments

ASME B89.1.10.M Dial Indicators (For Linear Measurements)

3. Terminology

3.1 *Definitions*—For definitions of common technical terms used in this standard, refer to Terminology D653.

3.2 *Definitions of Terms Specific to This Standard:*

3.2.1 *cast in-place pile, n*—a deep foundation element made of cement grout or concrete and constructed in its final location, for example, drilled shafts, bored piles, caissons, augered cast-in-place piles, pressure-injected footings, etc.

3.2.2 *deep foundation element, n*—a relatively slender structural element that transmits some or all of the load it supports to soil or rock well below the ground surface, such as a steel pipe or concrete-filled drilled shaft.

3.2.3 *driven pile, n*—a deep foundation element made of preformed material with a predetermined shape and size and typically installed by impact hammering, vibrating, or jacking.

3.2.4 *failure load, n*—the test load at which continuing, progressive movement occurs, or at which the total axial movement exceeds the value specified by the foundation engineer.

3.2.5 *gage or gauge, n*—an instrument used for measuring load, pressure, displacement, strain or such other physical properties associated with load testing as may be required.

3.2.6 *reaction, n*—a device or deep foundation element or elements designed to provide resistance in the opposite direction of the test load.

3.2.7 *telltale rod, n*—an unstrained metal rod extended through the test element from a specific point to be used as a reference from which to measure the change in the length of the loaded element.

3.2.8 *toe, n*—the bottom of a deep foundation element, sometimes referred to as tip or base.

3.2.9 *wireline, n*—a steel wire mounted with a constant tension force between two supports and used as a reference line to read a scale indicating movement of the test element.

4. Summary of Test Method

4.1 This standard provides minimum requirements for testing deep foundation elements under static axial tensile load. The test is a specific type of test, most commonly referred to as deep foundation load testing or static load testing. This standard is confined to test methods for loading a deep foundation element or elements from the top, in the upward direction. The loading requires devices or structural elements be constructed that resist downward movement, often referred to collectively as a reaction system. The principal measurements taken in addition to load are displacements.

4.2 This standard allows the following test procedures:

Method A	Quick Test	10.1.2
Method B	Maintained Test	10.1.3
Method C	Constant Rate of Uplift Test	10.1.4

5. Significance and Use

5.1 Field tests provide the most reliable relationship between the axial load applied to a deep foundation and the resulting axial movement. Test results may also provide information used to assess the distribution of side shear resistance along the element and the long-term load-deflection behavior. The foundation engineer may evaluate the test results to determine if, after applying appropriate factors of safety, the element or group of elements has a static capacity, load response and deflection at service load satisfactory to support the foundation. When performed as part of a multiple-element test program, the foundation engineer may also use the results

[2] For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

[3] Available from American Society of Mechanical Engineers (ASME), ASME International Headquarters, Two Park Ave., New York, NY 10016-5990, http://www.asme.org.

to assess the viability of different sizes and types of foundation elements and the variability of the test site.

5.2 If feasible and without exceeding the safe structural load on the element or element cap (hereinafter unless otherwise indicated, "element" and "element group" are interchangeable as appropriate), the maximum load applied should reach a failure load from which the foundation engineer may determine the axial static tensile load capacity of the element. Tests that achieve a failure load may help the foundation engineer improve the efficiency of the foundation design by reducing the foundation element length, quantity, and/or size.

5.3 If deemed impractical to apply axial test loads to an inclined element, the foundation engineer may elect to use axial test results from a nearby vertical element to evaluate the axial capacity of the inclined element. The foundation engineer may also elect to use a bi-directional axial test on an inclined element (D8169/D8169M).

5.4 Different loading test procedures may result in different load-displacement curves. The Quick Test (10.1.2) and Constant Rate of Uplift Test (10.1.4) typically can be completed in a few hours. Both are simple in concept, loading the element relatively quickly as load is increased. The Maintained Test (10.1.3) loads the element in larger increments and for longer intervals, which could cause the test duration to be significantly longer. Because of the larger load increments the determination of the failure load can be less precise, but the Maintained Test is thought to give more information on creep displacement. Although control of the Constant Rate of Uplift Test is somewhat more complicated (and uncommon for large diameter or capacity elements), the test may produce the best possible definition of capacity. The foundation engineer must weigh the complexity of the procedure and other limitations against any perceived benefit.

5.5 The scope of this standard does not include analysis for foundation capacity in tension, but in order to analyze the test data appropriately it is important that information on factors that affect the derived mobilized static axial tensile capacity are properly documented. These factors may include, but are not limited to, the following:

5.5.1 Potential residual loads in the element which could influence the interpreted distribution of load along the element shaft.

5.5.2 Possible interaction of friction loads from test element with downward friction transferred to the soil from reaction elements obtaining part or all of their support in soil at levels above the tip level of the test element.

5.5.3 Changes in pore water pressure in the soil caused by element driving, construction fill, and other construction operations which may influence the test results for frictional support in relatively impervious soils such as clay and silt.

5.5.4 Differences between conditions at time of testing and after final construction such as changes in grade or groundwater level.

5.5.5 Potential loss of soil supporting the test element from such activities as excavation and scour.

5.5.6 Possible differences in the performance of an element in a group or of an element group from that of a single isolated element.

5.5.7 Effect on long-term element performance of factors such as creep, environmental effects on element material, negative friction loads not previously accounted for, and strength losses.

5.5.8 Type of structure to be supported, including sensitivity of structure to settlements and relation between live and dead loads.

5.5.9 Special testing procedures which may be required for the application of certain acceptance criteria or methods of interpretation.

5.5.10 Requirement that non-tested element(s) have essentially identical conditions to those for tested element(s) including, but not limited to, subsurface conditions, element type, length, size and stiffness, and element installation methods and equipment, so that application or extrapolation of the test results to such other elements is valid. For concrete elements, it is sometimes necessary to use higher amounts of reinforcement in the test elements in order to safely conduct the test to the predetermined required test load. In such cases, the foundation engineer shall account for the difference in stiffness between the test elements and non-tested elements.

5.5.11 Tension tests are sometimes used to validate element compression capacity in addition to tension capacity. When subjected to tension loads, elements may have different stiffness and structural capacity compared to elements subjected to compression loads.

NOTE 1—The quality of the result produced by these test methods is dependent on the competence of the personnel performing it, and the suitability of the equipment and facilities used. Agencies that meet the criteria of Practice D3740 are generally considered capable of competent and objective testing/sampling/inspection/etc. Users of these test methods are cautioned that compliance with Practice D3740 does not in itself assure reliable results. Reliable results depend on many factors; Practice D3740 provides a means of evaluating some of those factors.

6. Test Foundation Preparation

6.1 Excavate or add fill to the ground surface around the test element to the final design elevation unless otherwise approved by the foundation engineer. Type of fill and compaction requirements shall be as specified by the foundation engineer.

6.2 Design and construct the test element so that any location along the depth of the element will safely sustain the maximum anticipated loads to be developed at that location. Cut off or build up the test element as necessary to permit construction of the load-application apparatus, placement of the necessary testing and instrumentation equipment, and observation of the instrumentation. Remove any damaged or unsound material from the element top as necessary to properly install the apparatus for measuring movement, for applying load, and for measuring load.

6.3 For tests on element groups, cap the element group with steel-reinforced concrete or a steel load frame designed for the anticipated loads by the structural engineer.

6.4 Install structural tension connectors extending from the test element or element cap, constructed of steel straps, bars, cables, and/or other devices bolted, welded, cast into, or otherwise firmly affixed to the test element or element cap to safely apply the maximum required test load without slippage, rupture, or excessive elongation. Carefully inspect these tension members for any damage that may reduce their tensile capacity. Tension members with a cross-sectional area reduced by corrosion or damage, or material properties compromised by fatigue, bending, or excessive heat, may rupture suddenly under load. Do not use brittle materials for tension connections.

NOTE 2—Deep foundations sometimes include hidden defects that may go unnoticed prior to static testing. Low strain integrity tests as described in Test Method D5882, ultrasonic crosshole integrity tests as described in Test Method D6760, and thermal integrity profiling as described in Test Methods D7949 may provide a useful pre-test evaluation of the test foundation. While the former two methods can be done at any time, including after the load test, thermal integrity profiling must be done relatively soon after the concrete element is cast.

NOTE 3—When testing a cast-in-place concrete element such as a drilled shaft, the size, shape, material composition and properties of the element can influence the element capacity and the interpretation of strain measurements described in Section 8.

7. Safety Requirements

7.1 All operations in connection with element load testing shall be carried out in such a manner to minimize, avoid, or eliminate the exposure of people to hazard. The following safety rules are in addition to general safety requirements applicable to construction operations:

7.1.1 Keep all test and adjacent work areas, walkways, platforms, etc. clear of scrap, debris, small tools, and accumulations of snow, ice, mud, grease, oil, or other slippery substances.

7.1.2 Provide timbers, blocking and cribbing materials made of quality material and in good serviceable condition with flat surfaces and without rounded edges.

7.1.3 Hydraulic jacks shall be equipped with hemispherical bearings or shall be in complete and firm contact with the bearing surfaces and shall be aligned with axis of loading to avoid eccentric loading.

7.1.4 Loads shall not be hoisted, swung, or suspended over any person and shall be controlled by tag lines.

7.1.5 For tests on inclined elements, all inclined jacks, bearing plates, test beam(s), or frame members shall be firmly fixed into place or adequately blocked to prevent slippage upon release of load.

7.1.6 All test beams, reaction frames, platforms, and boxes shall be adequately supported at all times.

7.1.7 Only authorized personnel shall be permitted within the immediate test area, and only as necessary to monitor test equipment. The overall load test plan should include all provisions and systems necessary to minimize or eliminate the need for personnel within the immediate test area. All reasonable effort shall be made to locate pumps, load cell readouts, data loggers, and test monitoring equipment at a safe distance away from jacks, loaded beams, weighted boxes, dead weights, and their supports and connections.

7.1.8 The requirements in this section have been developed to assist in the preparations for the testing process, but should not be considered completely comprehensive of all safety issues. Safety matters should be carefully considered with the list above being a starting point for any safety planning.

8. Apparatus for Applying and Measuring Loads

8.1 *General:*

8.1.1 The apparatus for applying tensile loads to a test element shall conform to one of the methods described in 8.3 – 8.6. The apparatus for applying and measuring loads described in this section shall be designed in accordance with recognized standards by a qualified engineer who shall clearly define the maximum allowable load that can be safely applied. The method in 8.3 is recommended. The method in 8.5 can develop high tensile loads with relatively low jacking capacity, but does not perform well for tests to failure or for large upward movements. All described methods require careful setup to ensure a safe test environment.

8.1.2 Reaction elements, if used, shall be of sufficient number and installed to safely provide adequate reaction capacity without excessive movement. When using two or more reaction elements at each end of the test beam(s), cap them with reaction beams (Fig. 1). Locate reaction elements so that resultant test beam load supported by them acts at the center of the reaction element group. Cribbing, if used as a reaction, shall be of sufficient plan dimensions to transfer the reaction loads to the soil without settling at a rate that would prevent maintaining the applied loads.

8.1.3 Cut off or build up reaction elements as necessary to place the reaction or test beam(s). Remove any damaged or unsound material from the top of the reaction elements, and provide a smooth bearing surface parallel to the reaction or test beam(s). To minimize stress concentrations due to minor surface irregularities, set steel bearing plates on the top of precast or cast-in-place concrete reaction elements in a thin layer of quick-setting, non-shrink grout, less than 6 mm [0.25 in.] thick and having a compressive strength greater than the reaction element at the time of the test. For steel reaction

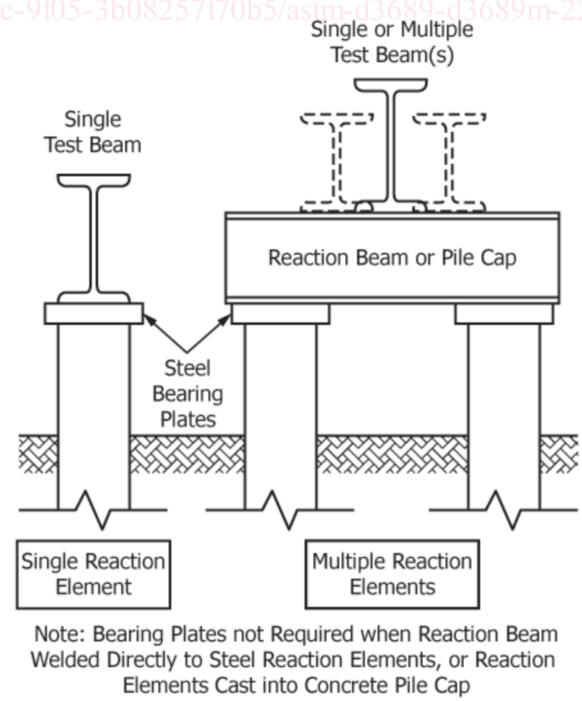

FIG. 1 Typical End Views of Test Beam(s) and Reaction Pile(s)

elements, weld a bearing plate to each element, or weld the cap or test beam(s) directly to each element. For timber reaction elements, set the bearing plate(s) directly on the cleanly cut top of the element, or in grout as described for concrete elements.

8.1.4 Provide a clear distance between the test element(s) and the reaction elements or cribbing of at least five times the maximum diameter of the largest test or reaction element(s), but not less than 2.5 m [8 ft]. The engineer may increase or decrease this minimum clear distance based on factors such as the type and depth of reaction, soil conditions, and magnitude of loads so that reaction forces do not significantly affect the test results.

NOTE 4—Excessive vibrations during reaction element installation in non-cohesive soils may affect test results. Reaction elements that penetrate deeper than the test element may affect test results. Reaction elements nearest to the test element should be installed first to help reduce installation effects. A clear distance of five (5) times the maximum element diameter may be impractical for larger elements.

8.1.5 Each jack shall include a lubricated hemispherical bearing or similar device to minimize lateral loading of the test element. The hemispherical bearing(s) should include a locking mechanism for safe handling and setup.

8.1.6 Provide bearing stiffeners as needed between the flanges of test and reaction beams.

8.1.7 Provide steel bearing plates to spread the load to and between the jack(s), load cell(s), hemispherical bearing(s), test beam(s), reaction beam(s), and reaction element(s). Unless otherwise specified by the engineer, the size of the bearing plates shall be not less than the outer perimeter of the jack(s), load cell(s), or hemispherical bearing(s), nor less than the total width of the test beam(s), reaction beam(s), reaction elements to provide full bearing and distribution of the load. Bearing plates supporting the jack(s), test beam(s), or reaction beams on timber or concrete cribbing shall have an area adequate for safe bearing on the cribbing.

8.1.8 Unless otherwise specified, where using steel bearing plates, provide a total plate thickness adequate to spread the bearing load between the outer perimeters of loaded surfaces at a maximum angle of 45 degrees to the loaded axis. For center hole jacks and center hole load cells, also provide steel plates adequate to spread the load from their inner diameter to the central axis at a maximum angle of 45 degrees, or per manufacturer recommendations.

8.1.9 Align the test load apparatus with the longitudinal axis of the test element to minimize eccentric loading. Align bearing plate(s), jack(s), load cell(s), and hemispherical bearing(s) on the same longitudinal axis. Place jacks to center the load on the test beam(s). Place test beam(s) to center the load on reaction beams or cribbing, and reaction beams to center the load on reaction piles or cribbing. These plates, beams, and devices shall have flat, parallel bearing surfaces. Set bearing plates on cribbing in the horizontal plane.

8.1.10 When testing inclined elements, align the test apparatus and reaction elements parallel to the inclined longitudinal axis of the test element(s) and orient the test beam(s) perpendicular to the direction of incline.

8.1.11 Qualified engineers shall design and approve all aspects of the loading apparatus, including loaded members, support frames, tension connections (material, diameter, weld or embedment length, etc.), reaction elements, instruments and loading procedures. The apparatus for applying and measuring loads (except for hydraulic jacks and load cells), including all structural members, shall have sufficient size, strength, and stiffness to safely prevent excessive deflection and instability up to the maximum anticipated test load.

NOTE 5—Rotations and lateral displacements of the test element, reaction elements, cribbing support(s), or element cap may occur during loading, especially for elements extending above the soil surface or through weak soils. Support reactions, loading apparatus and equipment should be designed and constructed to resist any undesirable or possibly dangerous rotations or lateral displacements. These displacements should be monitored during the test so the test can be immediately halted if undesirable rotations or lateral displacements occur.

8.2 *Hydraulic Jacks, Gages, Transducers, and Load Cells:*

8.2.1 The hydraulic jack(s) and their operation shall conform to ASME B30.1. Jack(s) and load cell(s) shall have a nominal load capacity exceeding the maximum anticipated test load by at least 20 %. The jack, pump, and any hoses, pipes, fittings, gages, or transducers used to pressurize it shall be rated to a safe pressure corresponding to the nominal jack capacity.

8.2.2 The hydraulic jack(s) shall have a ram (piston, rod) travel greater than the sum of the anticipated maximum axial movement of the element plus the deflection of the reaction system and the elongation of the tension connection, but not less than 15 % of the average element diameter or width (or any other specified and approved displacement requirement). Use a single high capacity jack when possible. When using a multiple jack system, provide jacks of the same make, model, and capacity, and supply the jack pressure through a common manifold with a master pressure gage, and operated by a single hydraulic pump. Fit the manifold and each jack with a pressure gage to detect malfunctions and imbalances.

8.2.3 Unless otherwise specified, the hydraulic jack(s), pressure gage(s), and pressure transducer(s) shall each be calibrated to at least the maximum anticipated jack load performed within the six months prior to each test or series of tests. Furnish the calibration report(s) prior to performing a test. Each report shall include the ambient temperature and individual calibrations shall be performed for multiple discrete ram strokes up to the maximum stroke of the jack.

8.2.4 Each complete jacking and pressure measurement system, including the hydraulic pump, should be calibrated as a unit when practicable. The hydraulic jack(s) shall be calibrated over the complete range of ram travel for increasing and decreasing applied loads. The calibrated jacking system(s) shall have accuracy within 5 % of the maximum applied load. When not feasible to calibrate a jacking system as a unit, calibrate the jack, pressure gages, and pressure transducers separately, and each of these components shall have accuracy within 2 % of the applied load.

8.2.5 Pressure gages and pressure transducers shall have minimum resolutions less than or equal to 1 % of the maximum applied load and shall conform to ASME B40.100 with an accuracy grade 1A having a permissible error ±1 % of the span. When used for control of the test, pressure transducers shall include a real-time display.

8.2.6 Place a properly positioned load cell or equivalent device in series with each hydraulic jack. Unless otherwise specified the load cell shall have a calibration to at least the maximum anticipated jack load performed within the six months prior to each test or series of tests. The calibrated load cell shall have accuracy within 1 % of the applied load, including an eccentric loading of up to 1 % applied at an eccentric distance of 25 mm [1 in.]. After calibration, load cells shall not be subjected to impact loads.

8.2.7 Do not leave the hydraulic jack pump unattended at any time during the test. Automated jacking systems shall include a clearly marked mechanical override to safely reduce hydraulic pressure in an emergency.

8.3 *Load Applied by Hydraulic Jack(s) Supported on Test Beam(s) (Figs. 2 and 3)*—Support the ends of the test beam(s) on reaction elements or cribbing, using reaction beams as needed to cap multiple reaction elements as shown in Fig. 1. Place the hydraulic jack(s), load cell(s), hemispherical bearing(s), and bearing plates on top of the test beam(s). Center a reaction frame over the jack(s), and anchor it to the tension connections (see 6.4) extending from the test element. Design and construct the test beam(s), reaction frame, and reaction elements or cribbing, and arrange the jack(s) symmetrically to apply the resultant tensile load at, and parallel to, to the longitudinal axis of the test element. Leave adequate clear space beneath the bottom flange(s) of the test beam(s) to allow for the maximum anticipated upward movement of the test element plus the deflection of the test beam(s).

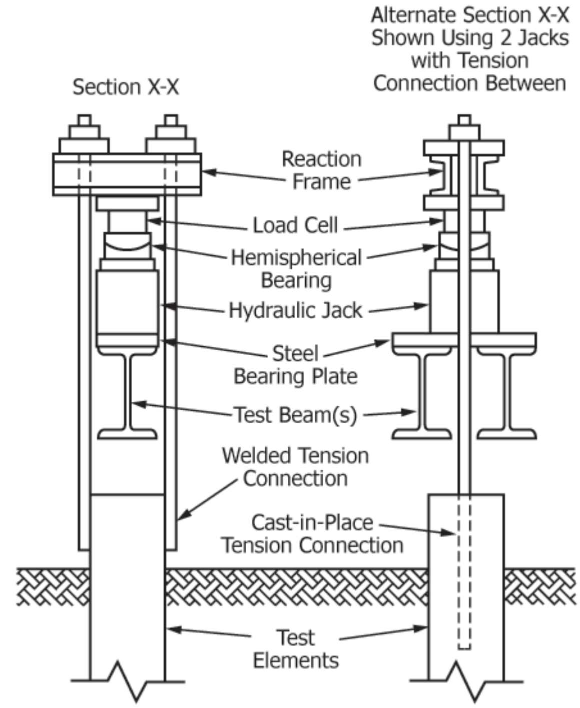

FIG. 3 Typical Section X-X (Fig. 2) of Test Beam(s) at Test Element(s)

8.4 *Load Applied by Hydraulic Jacks Acting Upward at Both Ends of Test Beam(s) (Figs. 4 and 5)*—Support each end of the test beam(s) on hydraulic jack(s) centered beneath the beam web(s) and placed equidistant from the longitudinal axis of the test element. Support the jacks on reaction elements or cribbing, using reaction beams as needed to cap multiple reaction elements. Center a reaction frame over the test beam(s) and anchor it to the tension connections (see 6.4) extending from the test element. Place a single load cell and hemispherical bearing between the reaction frame and the test beam(s) (preferred), or alternatively, place a load cell and hemispherical bearing with each jack beneath the test beam(s). Design and construct the test beam(s), reaction frame, and reaction elements or cribbing, and arrange the jack(s) symmetrically to apply the resultant tensile load at, and parallel to, the longitudinal axis of the test element.

8.5 *Load Applied by Hydraulic Jack(s) Acting Upward at One End of Test Beam(s) (Figs. 5 and 6)*—Support one end of the test beam(s) on hydraulic jack(s) centered beneath the beam

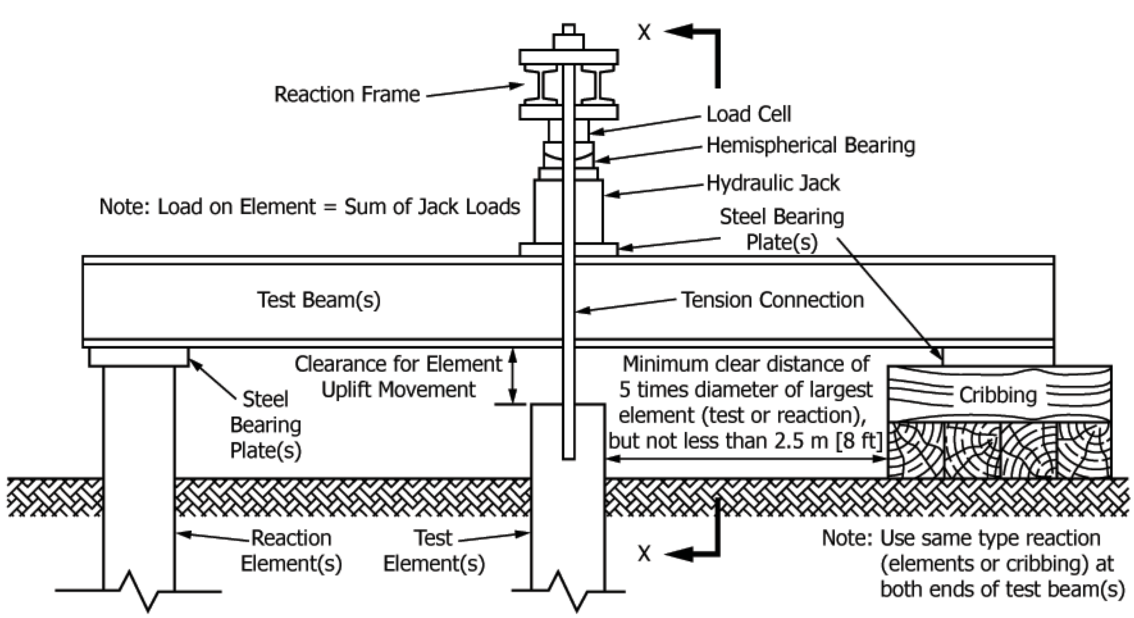

FIG. 2 Typical Setup for Load Test Using Hydraulic Jack(s) Supported on Test Beam(s)

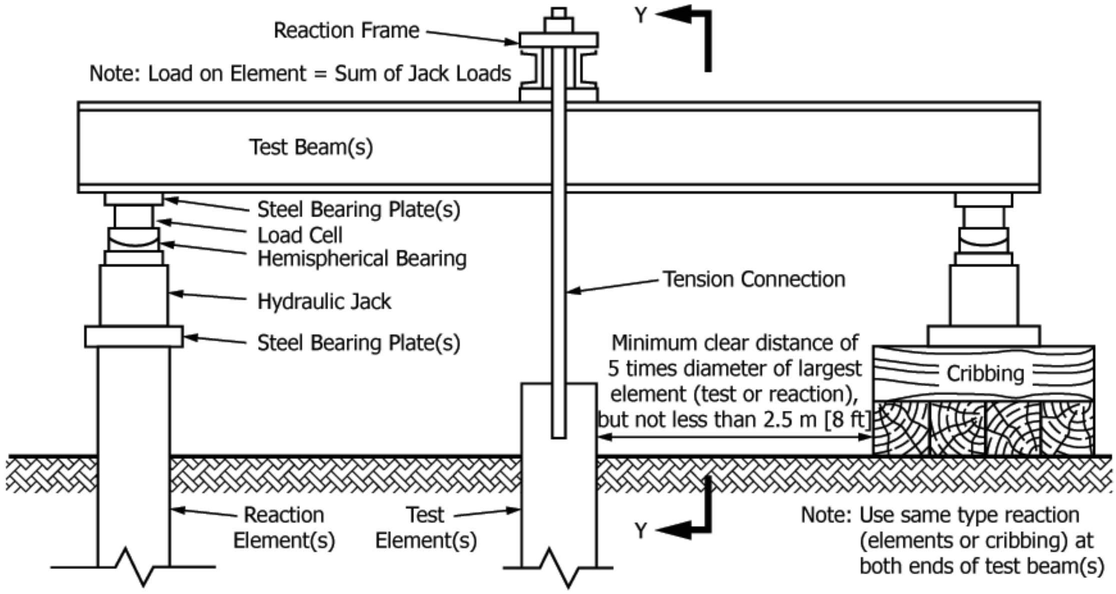

FIG. 4 Typical Setup for Load Test Using Hydraulic Jacks Acting Upward on Both Ends of Test Beam(s)

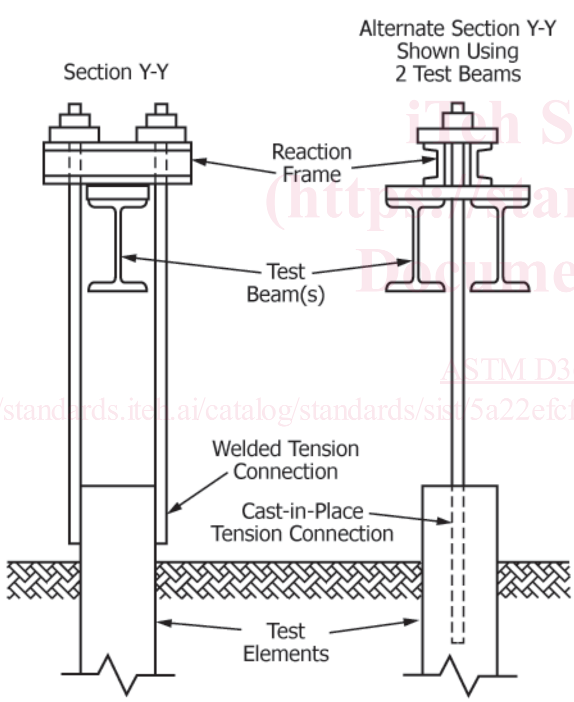

FIG. 5 Typical Section Y-Y (Fig. 4, Fig. 6) of Test Beam(s) at Test Element(s)

web(s). Support the jacks on reaction piles or cribbing, using reaction beams as needed to cap multiple reaction elements. Support the other end of the test beam(s) on a steel fulcrum or similar device placed on a steel plate supported on a reaction element(s) or cribbing, using reaction beams as needed to cap multiple reaction elements. Center a reaction frame over the test beam(s) and anchor it to the tension connections (see 6.4) extending from the test element. Place a single load cell and hemispherical bearing between the reaction frame and the test beam(s) (preferred), or alternatively, place a load cell and hemispherical bearing with each jack beneath the test beam(s). If using the latter arrangement, obtain accurate measurements of the plan locations of the jack(s), test element, and the fulcrum to determine the magnification factor to apply to the measured loads to determine the resultant tensile load. Design and construct the test beam(s), reaction frame, and reaction elements or cribbing, and arrange the jack(s) symmetrically to apply the resultant tensile load at, and parallel to, the longitudinal axis of the test element.

8.6 *Load Applied by Hydraulic Jack(s) Acting at Top of an A-Frame or a Tripod (Fig. 7) (optional)*—Support an A frame or tripod centered over the test element on concrete footings, reaction elements, or cribbing, using reaction beams as needed to cap multiple reaction elements. Using tension members, tie together the bottoms or supports of the A frame or tripod legs to prevent them from spreading apart under load. Secure the top of an A frame against lateral movement with not less than four guy cables anchored firmly to the ground. Place the hydraulic jack(s), load cell(s), hemispherical bearing(s), and bearing plates on top of the A frame or tripod. Center a reaction frame over the jack(s), and anchor it to the tension connections (see 6.4) extending from the test element. Design and construct the A frame or tripod, reaction frame, and footings, reaction elements or cribbing, and arrange the jack(s) symmetrically to apply the resultant tensile load at, and parallel to, the longitudinal axis of the test element. Leave adequate clear space beneath the A frame or tripod members to allow for the maximum anticipated upward movement of the test element or element cap plus the deflection of the A frame or tripod.

8.7 *Other Types of Loading Apparatus (optional)*—The engineer may specify another type of loading apparatus satisfying the basic requirements of 8.3 – 8.6.