



Designation: ~~C1832–22~~ C1832 – 23

# Standard Test Method for Determination of Uranium Isotopic Composition by Modified Total Evaporation (MTE) Method Using Thermal Ionization Mass Spectrometer<sup>1</sup>

This standard is issued under the fixed designation C1832; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reapproval.

## 1. Scope

1.1 This test method describes the determination of the isotope amount ratios of uranium material as nitrate solutions by the modified total evaporation (MTE) method using a thermal ionization mass spectrometer (TIMS) instrument.

1.2 The analytical performance in the determination of the  $^{235}\text{U}/^{238}\text{U}$  major isotope amount ratio by MTE is similar to the (“classical”) total evaporation (TE) method as described in [C1672](#). However, in the MTE method, the evaporation process is interrupted on a regular basis to allow measurements and subsequent corrections for background from peak tailing, perform internal calibration of a secondary electron multiplier (SEM) detector versus the Faraday cups, peak centering, and ion source refocusing. Performing these calibrations and corrections on a regular basis during the measurement, improves precision, and significantly reduces uncertainties for the minor isotope amount ratios  $^{234}\text{U}/^{238}\text{U}$  and  $^{236}\text{U}/^{238}\text{U}$  as compared to the TE method.

1.3 In principle, the MTE method may yield major isotope amount ratios without the need for mass fractionation correction. However, depending on the measurement conditions, small variations are observed between sample turrets. Therefore, a small correction based on measurements of a certified reference material is recommended to improve consistency. The uncertainty around the mass fractionation correction factor usually includes unity.

1.4 *Units*—The values stated in SI units are to be regarded as standard. The values given in parentheses after SI units are provided for information only and are not considered standard.

1.5 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety, health, and environmental practices and determine the applicability of regulatory limitations prior to use.*

1.6 *This international standard was developed in accordance with internationally recognized principles on standardization established in the Decision on Principles for the Development of International Standards, Guides and Recommendations issued by the World Trade Organization Technical Barriers to Trade (TBT) Committee.*

## 2. Referenced Documents

### 2.1 ASTM Standards:<sup>2</sup>

[C753](#) Specification for Nuclear-Grade, Sinterable Uranium Dioxide Powder

<sup>1</sup> This test method is under the jurisdiction of ASTM Committee [C26](#) on Nuclear Fuel Cycle and is the direct responsibility of Subcommittee [C26.05](#) on Methods of Test. Current edition approved Feb. 1, 2022/Jan. 1, 2023. Published March 2022/January 2023. Originally approved in 2016. Last previous edition approved in 2024/2022 as ~~C1832–24~~ C1832 – 22. DOI: [10.1520/C1832-22](#). [10.1520/C1832-23](#).

<sup>2</sup> For referenced ASTM standards, visit the ASTM website, [www.astm.org](#), or contact ASTM Customer Service at [service@astm.org](#). For *Annual Book of ASTM Standards* volume information, refer to the standard’s Document Summary page on the ASTM website.

[C776 Specification for Sintered Uranium Dioxide Pellets for Light Water Reactors](#)  
[C787 Specification for Uranium Hexafluoride for Enrichment](#)  
[C833 Specification for Sintered \(Uranium-Plutonium\) Dioxide Pellets for Light Water Reactors](#)  
[C859 Terminology Relating to Nuclear Materials](#)  
[C967 Specification for Uranium Ore Concentrate](#)  
[C996 Specification for Uranium Hexafluoride Enriched to Less Than 5 % <sup>235</sup>U](#)  
[C1008 Specification for Sintered \(Uranium-Plutonium\) Dioxide Pellets—Fast Reactor Fuel \(Withdrawn 2014\)<sup>3</sup>](#)  
[C1068 Guide for Qualification of Measurement Methods by a Laboratory Within the Nuclear Industry](#)  
[C1128 Guide for Preparation of Working Reference Materials for Use in Analysis of Nuclear Fuel Cycle Materials](#)  
[C1156 Guide for Establishing Calibration for a Measurement Method Used to Analyze Nuclear Fuel Cycle Materials](#)  
[C1347 Practice for Preparation and Dissolution of Uranium Materials for Analysis](#)  
[C1411 Practice for The Ion Exchange Separation of Uranium and Plutonium Prior to Isotopic Analysis](#)  
[C1625 Test Method for Uranium and Plutonium Concentrations and Isotopic Abundances by Thermal Ionization Mass Spectrometry](#)  
[C1672 Test Method for Determination of Uranium or Plutonium Isotopic Composition or Concentration by the Total Evaporation Method Using a Thermal Ionization Mass Spectrometer](#)  
[C1871 Test Method for Determination of Uranium Isotopic Composition by the Double Spike Method Using a Thermal Ionization Mass Spectrometer](#)  
[D1193 Specification for Reagent Water](#)  
[E2586 Practice for Calculating and Using Basic Statistics](#)  
[E2655 Guide for Reporting Uncertainty of Test Results and Use of the Term Measurement Uncertainty in ASTM Test Methods](#)

### 3. Terminology

3.1 Terminology [C859](#) contains terms, definitions, descriptions of terms, nomenclature, and explanations of acronyms and symbols specifically associated with standards under the jurisdiction of Committee C26 on Nuclear Fuel Cycle.

#### 3.2 Definitions:

3.2.1 *abundance sensitivity, n*—in isotope amount ratio measurements, the ratio of the measured intensity of an ion beam at a mass  $m$ , to the measured intensity from the same isotope measured at one mass unit difference (for example,  $m \pm 1$ ).

##### 3.2.1.1 Discussion—

Abundance sensitivity is a measure of the magnitude of the peak tailing correction. For measuring uranium on thermal ionization mass spectrometer (TIMS) and inductively coupled plasma mass spectrometry (ICP-MS) instruments, the abundance sensitivity is typically calculated as the ratio of the measured signal intensities at masses 237 and 238 using a suitable uranium sample.

3.2.2 *dark noise, n*—observed count rate on an ion counting detector measured without incident ion beam

3.2.3 *total evaporation, TE, n*—analytical method for determination of isotope amount ratios of uranium or plutonium, as described in Test Method [C1672](#), also called “classical” total evaporation in this test method.

3.2.4 *turret, n*—holder for sample filaments.

##### 3.2.4.1 Discussion—

Alternate names for turret are carousel, magazine, wheel.

#### 3.3 Acronyms and Abbreviations:

3.3.1 *cpm*—counts per minute

3.3.2 *cps*—counts per second

3.3.3 *CRM*—Certified Reference Material

3.3.4 *DS*—Double Spike

3.3.5 *DU*—Depleted Uranium

<sup>3</sup> The last approved version of this historical standard is referenced on [www.astm.org](http://www.astm.org).

3.3.6 *FAR*—Faraday Cup

3.3.7 *HEU*—High Enriched Uranium

3.3.8 *IAEA*—International Atomic Energy Agency

3.3.9 *ICPMS*—Inductively Coupled Plasma Mass Spectrometry

3.3.10 *IRMM*—Institute for Reference Materials and Measurements

3.3.11 *ITU*—Institute for Transuranium Elements

3.3.12 *JRC*—Joint Research Centre of the European Union

3.3.13 *JRC-G.2*—Unit for Standards for Nuclear Safety, Security and Safeguards of JRC (new name for the nuclear part of the former IRMM)

3.3.14 *JRC-G.II.6*—Unit for Nuclear Safeguards and Forensics of JRC (part of the former ITU)

3.3.15 *LEU*—Low Enriched Uranium

3.3.16 *MTE*—Modified Total Evaporation

3.3.17 *NBL*—New Brunswick Laboratory

3.3.18 *RSD*—Relative Standard Deviation; SD (see below) divided by the mean value of the observations in repeated sampling

3.3.19 *RSE*—Relative Standard Error; SE (see below) divided by the mean value of the observations in repeated sampling

3.3.20 *SD*—Standard Deviation; according to Practice **E2586**, 3.1.30, the square root of the sum of the squared deviations of the observed values in the sample divided by the sample size minus one

3.3.21 *SE*—Standard Error; according to Practice **E2586**, 3.1.29, standard deviation of the population of values of a sample statistic (that is, the mean value) in repeated measurements, or an estimate of it.

3.3.21.1 *Discussion*—

According to Practice **E2586**, 3.1.30, if the standard error (SE, see above) of a statistic is estimated, it will itself be a statistic with some variance that depends on the sample size, that is, the number of observed values in the sample (Practice **E2586**, 3.1.26).

3.3.21.2 *Discussion*—

According to Guide **E2655**, 5.8.4.1, from statistical theory, a 95 % confidence interval for the mean of a normal distribution, given  $n$  independent observations  $x_1, x_2, \dots, x_n$  drawn from the distribution is,  $x_{mean} \pm t \times SD / \sqrt{n}$ , where  $x_{mean}$  is the sample mean, SD is the standard deviation of the observations (see above), and  $t$  is the 0.975 percentile of the Student's  $t$  distribution with  $n-1$  degrees of freedom. Because Student's  $t$  distribution approaches the Normal as  $n$  increases, the value of  $t$  approaches 1.96 as  $n$  increases. This is the basis for using the (coverage) factor 2 for expanded uncertainty. The standard error (SE) of the mean value of a series of  $n$  independent repeated measurements can be derived from that by using  $t = 1$ , so the standard error (SE) is given by  $SD/\sqrt{n}$ .

3.3.22 *SEM*—Secondary Electron Multiplier

3.3.22.1 *Discussion*—

In the scientific literature the acronym SEM is also used for Scanning Electron Microscope, but within this document SEM represents Secondary Electron Multiplier.

3.3.23 *SGAS*—Safeguards Analytical Services Laboratory of the IAEA

### 3.3.24 TIMS—thermal ionization mass spectrometry

## 4. Summary of Test Method

4.1 The modified total evaporation method has been developed on the basis of the “classical” total evaporation technique (1-4),<sup>4</sup> also described in Test Method C1672. By using the total evaporation technique, the mass fractionation is minimized by evaporating the entire sample amount loaded on the filament, in contrast to the “conventional” technique as described in Test Method C1625. The MTE method has already been described in detail in Refs (5) and (6). If necessary, uranium is separated from plutonium and other elements (to eliminate isobaric interferences) by selective extraction, anion exchange (see Practice C1411), or extraction chromatography. The purified uranium fraction as nitrate solution is loaded onto a degassed filament (made of metals such as rhenium, zone-refined rhenium, or tungsten) with high evaporation temperature and converted to an oxide by controlled heating of the filament under atmospheric conditions. For the MTE method, the uranium load is in the range of about  $22\ \mu\text{g}$  to  $6\ \mu\text{g}$ , which is about one to two orders of magnitude higher than that typically used for the “classical” total evaporation method by TIMS. The sample filament is mounted on the sample turret using a double-filament configuration. This configuration consists of an evaporation filament (Re or W) on which the sample is loaded, and an ionization filament (Re filament with no sample). For a measurement in the mass spectrometer, the ionization filament is heated to a temperature of about  $1700\text{--}1900\text{ }^{\circ}\text{C}$ , sufficient to generate  $^{187}\text{Re}$  ion beam signals of  $150\text{--}400\ \text{mV}$  (corresponding to ion currents of  $1.5 \times 10^{-12}\ \text{A}$  to  $4 \times 10^{-12}\ \text{A}$  using an amplifier resistor of  $10^{11}\ \Omega$ ). The intensity of the optimized  $^{187}\text{Re}$  signal depends on the Re material (zone-refined or non-zone-refined), thickness and the measurement conditions, but it is expected to be similar for all filaments on the same sample turret. The  $^{187}\text{Re}$  ion current is also used for the initial ion beam focusing. The evaporation filament is heated next. After ion beam re-focusing and mass re-adjustment initially using a small sum intensity (sum of  $^{234}\text{U}$ ,  $^{235}\text{U}$ ,  $^{236}\text{U}$ , and  $^{238}\text{U}$ ) of about  $1\ \text{V}$  to  $4\ \text{V}$ , the data acquisition begins usually under computer control to yield a predefined target sum intensity of  $20\text{--}30\ \text{V}$  (corresponding to ion currents of  $2 \times 10^{-10}\ \text{A}$  to  $3 \times 10^{-10}\ \text{A}$  using an amplifier resistor of  $10^{11}\ \Omega$ ). This target value depends on the amount of uranium loaded on a filament. The MTE analysis takes between 2 and 5 h per sample filament and is about three to ten times longer than (“classical”) TE analyses in spite of the higher intensities at which the analyses are performed. To ensure that the whole sample is completely evaporated and analyzed before the ionization filament breaks as a result of overheating, the MTE analysis routine is programmed to increase the target sum intensity during the course of the analysis if necessary. The occurrences of outliers due to technical glitches, for example, as a result of termination before complete sample evaporation or because of early sample exhaustion, are minimized by a dynamic target intensity control feature through manipulation of the target sum intensity depending on the actual measurement conditions.

4.2 The sample amount to be loaded for MTE analyses is limited to a range of about  $22\ \mu\text{g}$  to  $6\ \mu\text{g}$  to achieve ion beam signals of about  $20\text{--}30\ \text{V}$  for the major isotope ( $^{238}\text{U}$  for DU, NU, and LEU samples and  $^{235}\text{U}$  for HEU samples) corresponding to a  $^{234}\text{U}$  intensity of  $1\ \text{mV}$  to  $10\ \text{mV}$ . This causes the  $^{234}\text{U}$  ion beam to be suitable for an internal cross calibration of the SEM versus the Faraday cups through the entire measurement time. This also allows the  $^{236}\text{U}/^{238}\text{U}$  isotope amount ratio to be measured in a wide dynamic range from  $10^{-2}$  down to  $10^{-10}$  using a Faraday cup or an SEM in combination with an energy filter for improved abundance sensitivity. For all samples with minor ratios  $^{234}\text{U}/^{238}\text{U}$  and  $^{236}\text{U}/^{238}\text{U}$  higher than  $3 \times 10^{-5}$ , which also includes HEU samples, the minor isotopes are only measured using Faraday cups, with amplifier resistors of  $10^{12}\ \Omega$  or  $10^{13}\ \Omega$  yielding a favorable signal-to-noise ratio.

4.3 Similar to the TE analysis, the isotope ion beams of the major isotopes  $^{235}\text{U}$  and  $^{238}\text{U}$  are integrated over the course of the analysis, and the summed intensity for  $^{235}\text{U}$  is divided by the summed intensity for  $^{238}\text{U}$  to yield the major isotope amount ratio. The result of the major isotope amount ratio is corrected for mass fractionation using the measurement of a CRM analyzed on the same sample turret.

4.4 The minor isotope amount ratios are corrected for mass fractionation for each integration step individually. This is accomplished in an internal manner; the magnitude of the mass fractionation for the minor ratios is calculated from the measured mass fractionation of the major ratio. The peak tailing contributions are determined at two positions, slightly below and slightly above the isotope masses of interest. If applicable, the SEM-versus-Faraday calibration is also performed for each integration step individually.

## 5. Significance and Use

5.1 Uranium material is used as a fuel in certain types of nuclear reactors. To be suitable for use as nuclear fuel, the starting

<sup>4</sup> The boldface numbers in parentheses refer to a list of references at the end of this standard.

material shall meet certain specifications such as those described in Specifications **C753**, **C776**, **C787**, **C833**, **C967**, **C996**, and **C1008**, or as specified by the purchaser. The isotope amount ratios of uranium material can be measured by mass spectrometry following this test method to ensure that they meet the specification.

5.2 The MTE method can be used for a wide range of sample sizes even in samples containing as low as 20  $\mu\text{g}$  of uranium. If the uranium sample is in the form of uranium hexafluoride, it has to be converted into a uranium nitrate solution for measurement by the MTE method. The concentration of the loading solution for MTE has to be in the range of 1 mg/g to 6 mg/g to allow a sample loading of  $22\ \mu\text{g}$  to 6  $\mu\text{g}$  of uranium. A minimum loading of 3  $\mu\text{g}$  uranium per filament is strongly recommended. This is needed to have a sufficient and stable ion signal especially for the two minor isotopes ( $^{234}\text{U}$  and  $^{236}\text{U}$ ) thus enabling the internal calibration of SEM versus the Faraday cups using the  $^{234}\text{U}$  ion beam signal during the measurement.

5.3 Until now, the instrument capabilities for the MTE method have only been implemented on the TRITON™ TIMS instrument.<sup>5</sup> Therefore, all recommendations for measurement parameters in this test method are specified for the TRITON instrument. The manufacturers of other TIMS instruments (for example, IsotopX and Nu Instruments) have indicated plans to implement the modifications needed in their instruments to use the MTE method.

5.4 The MTE method described here can also be extended to measurement of elements other than uranium. Note that the MTE method has already been implemented for plutonium and calcium.

## 6. Interferences

6.1 Isobaric nuclides such as  $^{238}\text{Pu}$  interfere in the uranium measurements. The removal of interferences is generally accomplished by chemical separation leading to ionization of uranium only and improved precision of measured isotope amount ratios.

6.2 It has to be ensured that samples are not contaminated by environmental uranium. The level of effort required to minimize contamination shall be based upon the sample size and the levels of contamination present in the analytical facility. For extremely small samples or extremely low  $^{236}\text{U}$  abundances, residual uranium from chemicals used for sample dissolution and sample preparation are possible sources for bias in the isotopic data.

6.3 Samples shall be chemically purified to assure reliable analyses by TIMS. Impurities, especially alkali elements, produce unstable ion emission leading to poor precision in the isotope amount ratios. Organic contaminants or oxide layers on the filaments also adversely influence TIMS analyses. Isobaric interferences, if not removed, will bias the isotope amount ratios. Contaminants in reagents, lab ware, or filament material are also sources for bias in the isotope amount ratios.

6.4 The performance of the instrument can be adversely affected by changes in the environmental conditions of the laboratory, that is, temperature and humidity. For this reason, controlled laboratory environmental conditions should be maintained (within the manufacturer's specifications) during instrument operation.

## 7. Apparatus

7.1 The suitability of the mass spectrometer for carrying out measurements by the MTE method shall be evaluated by means of performance tests. The relevant instrument characteristics are as follows:

7.1.1 A thermal ionization source for using double filament assemblies with rhenium or tungsten filaments, or both.

7.1.2 A mass analyzer sufficient to resolve adjacent masses in the mass-to-charge range being studied,  $m/z = 233$  to 238 for  $\text{U}^+$ . Resolution shall be greater than 350 (full width at 1 % of peak height) and the abundance sensitivity at mass 237 for ions of  $^{238}\text{U}$  less than  $5 \times 10^{-6}$ .

7.1.3 A multiple Faraday collector system to allow simultaneous detection of isotope beams from  $m/z = 233$  to 238 for  $\text{U}^+$  ions.

7.1.4 For the Faraday cups used to measure the major ion beams of  $^{235}\text{U}$  and  $^{238}\text{U}$ , there shall be current amplifiers equipped with  $10^{11}\ \Omega$  resistors and, for the minor ion beams of  $^{234}\text{U}$  and  $^{236}\text{U}$ , there shall be current amplifiers equipped with at least  $10^{11}\ \Omega$ , and preferably  $10^{12}\ \Omega$  (or even  $10^{13}\ \Omega$ ) resistors to improve the signal-to-noise ratio.

<sup>5</sup> The TRITON™ (Plus) Multicollector Thermal Ionization Mass Spectrometer is a trademark product of Thermo Fisher Scientific, <http://www.thermoscientific.com>.

7.1.5 The detection system shall include at least one secondary electron multiplier (SEM) operated in ion counting mode or a Daly detector, or similar detector, with a dark noise  $<0.2$  cps. The SEM shall be equipped with an energy filter to improve the abundance sensitivity, which shall be better than  $2 \times 10^{-8}$  at mass 237 for ions from  $^{238}\text{U}^+$  with the energy filter in operation.

7.1.6 A sample turret with at least ten filament positions to allow automatic measurement sequences of at least five replicate filament loadings per sample and at least five replicate filament loadings for a calibration standard (preferentially a CRM).

7.1.7 A pumping system that is able to attain a vacuum of  $<4.0 \times 10^{-5}$  Pa ( $3 \times 10^{-7}$  torr) in the ion source, the analyzer, and the detector is required. Tailing corrections are dependent on the vacuum levels inside the mass spectrometer. Analyzer pressures below  $7.0 \times 10^{-7}$  Pa ( $5 \times 10^{-9}$  torr) are preferred.

7.1.8 A mechanism to scan masses by varying the magnetic field or the accelerating voltage, or both.

7.1.9 An optical pyrometer for determining the temperatures of the filaments.

7.1.10 A computer for control of the data acquisition according to a predefined sequence.

7.2 *Special MTE Capabilities*—The mass spectrometer software must be flexible enough to implement a user-defined filament-heating program for MTE.<sup>6</sup>

7.3 A separate filament degassing device for cleaning of the filaments before sample loading is recommended.

7.4 *Microsyringe or Micropipette*—Syringe to transfer microlitre volumes of solutions.

## 8. Reagents and Materials

8.1 *Purity of Reagents*—Reagent-grade chemicals shall be used in all sample preparations. Unless otherwise indicated, it is intended that all reagents conform to the specifications of the Committee on Analytical Reagents of the American Chemical Society where such specifications are available.<sup>7</sup> Other grades may be used, provided it is first ascertained that the reagent is of sufficiently high purity and low uranium concentration to permit its use without lessening the accuracy of the MTE measurements.

8.2 Ultra-high purity reagents are necessary for processing small sample amounts or samples with extremely small isotope amount ratios. The level of uranium contamination from chemicals, water, and the sample handling environments shall be determined to ensure that the materials and the environment are sufficiently pure for the samples being analyzed.

8.3 *Nitric Acid* ( $\text{HNO}_3$ , 15.8 M)—Concentrated nitric acid.

8.4 *Nitric Acid* ( $\text{HNO}_3$ , 1 M)—One volume of concentrated nitric acid ( $\text{HNO}_3$ , 15.8 M) brought to 15.8 volumes with water.

8.5 *Purity of Water*—Unless otherwise indicated, references to water shall be understood to mean laboratory accepted demineralized or deionized water as described by Type I of Specification **D1193**.

8.6 *Filaments*—High-purity filaments, for example, zone refined Re, are required. The size and configuration of the filament is instrument dependent. Tungsten might be used with minor modifications to the heating script. All filaments must be degassed before use. For measurement of uranium present only at the trace levels in the sample, contamination of the samples by interferences from elemental or molecular species within the  $m/z = 233$  to 238 range need to be determined to ensure that biases due to contributions from the filament material will not bias the analysis results. In case a significant count rate  $>1$  cps is determined at  $m/z = 236$ , a correction has to be applied for  $^{236}\text{U}/^{238}\text{U}$  ratios  $< 10^{-6}$  (**6, 7**).

<sup>6</sup> The sole source of supply of the apparatus known to the committee at this time is Thermo Fisher Scientific Inc., 81 Wyman St., Waltham, MA 02451. If you are aware of alternative suppliers, please provide this information to ASTM International Headquarters. Your comments will receive careful consideration at a meeting of the responsible technical committee,<sup>1</sup> which you may attend.

<sup>7</sup> *ACS Reagent Chemicals, Specifications and Procedures for Reagents and Standard-Grade Reference Materials*, American Chemical Society, Washington, DC. For suggestions on the testing of reagents not listed by the American Chemical Society, see *Analar Standards for Laboratory Chemicals*, BDH Ltd., Poole, Dorset, U.K., and the *United States Pharmacopeia and National Formulary*, U.S. Pharmacopeial Convention, Inc. (USPC), Rockville, MD.

## 9. Hazards

9.1 TIMS instruments operate at 8 to 10 kV electrical potential. Ensure that the high-voltage is switched off before insertion or removal of the sample turret into/from the instrument, and working with the ion source, or accessing other electronic components.

9.2 The filaments reach temperatures in excess of 2000 °C. The filament holders, sample wheel, and ion source parts are expected to be hot. Ensure that a sufficient time has lapsed since the last filament heating before accessing the filaments, sample turrets, and ion source.

9.3 Wear eye protection and suitable gloves when filling cold traps with liquid nitrogen. Protect hands, torso, and feet in the event of splashing or spilling of the liquid nitrogen.

9.4 Handle radioactive materials with appropriate attention to radiological safety.

## 10. Sampling, Test Specimens, and Test Units

10.1 *Isotope Reference Materials*—Uranium reference materials used in the analysis should be prepared from certified reference materials (CRMs) traceable to SI units. Examples include the NBL U-Series CRMs (for example, U010 and U500), IRMM uranium standards IRMM 184-187, IRMM 019-029 (to be converted from UF<sub>6</sub>), IRMM-074, IRMM-075, and IRMM-3100. See Guide [C1128](#) for additional guidance on preparation of traceable working reference materials.

10.2 Uranium samples to be measured and isotope reference materials used for estimation of the mass fractionation correction factor (*K*-factor) or for quality control purposes shall be in the same medium and in the same oxidation state. The solutions for loading onto the filaments are 1 *M* nitric acid solutions. The uranium concentrations of these solutions shall be similar. The loading and drying sequence of the filaments shall also be similar.

10.3 In the case of characterization studies of test materials, possible inhomogeneity between test units shall be evaluated statistically and included in the uncertainty calculations of the isotope amount ratios assigned.

## 11. Preparation of Apparatus

11.1 *Filament Degassing*—Degass all filaments before using them for MTE measurements. It is recommended to use a separate apparatus (see [7.3](#)) for performing this. Start the degassing procedure when a vacuum pressure of  $<4.0 \times 10^{-4}$  Pa ( $3 \times 10^{-6}$  torr) is reached. Recommended filament currents for degassing are in the range of ~~4.0~~4.0 A to 5.0 A, corresponding to temperatures in the range of ~~1700~~1700 °C to 2000 °C. Perform the degassing for a duration of at least 30 min.

11.2 *“Initialization” of Sample Turret*—Adjust, if needed, the position of the sample turret in the ion source and verify proper electrical connections for both the evaporation and ionization filament for each sample loading position. It shall be ensured that the electrical contact is not interrupted in case the turret is slightly moved for the purpose of ion beam focusing.

11.3 *Amplifier Signal Decay Adjustment*—Adjust the signal decay characteristics of the current amplifiers of the Faraday cups. This is important for measuring isotope amount ratios with a large dynamic range, especially for the minor isotope amount ratios of uranium. Depending on the combination of the capacitance and resistance of the current amplifier, the response time for a sudden change in the ion beam signal to the Faraday cup can reach up to 5 s. For resistances higher than the  $10^{11}$  Ω, for example,  $10^{12}$  Ω, and in particular  $10^{13}$  Ω, longer response times of about 15 s can be expected. The MTE method is designed by taking into consideration the required response times. The amplifier response can be checked either using a custom-made software module within the operating software (when available) or “manually” by means of a large ion beam that is abruptly directed into a Faraday cup to check the signal ingrowth time, or away from a Faraday cup (for example, by closing a valve between ion source and analyzer) to check the signal decay time.

11.4 *SEM Plateau Voltage*—The SEM plateau voltage, that is, the dependency of the count rate on the applied high voltage to the SEM, shall be measured on a regular basis, as recommended by the manufacturer of the SEM or the operator’s quality system. Typical SEM plateau voltages range between ~~1700~~1700 V to 3000 V. The SEM plateau voltage drifts to higher values with use and shall be readjusted to restore the original efficiency. The efficiency should be higher than 90 %.

11.5 *SEM Dark Noise*—SEM detectors are usually operated in ion counting rather than analogue mode to avoid the resistor noise of the current amplifier. The ion counting mode results in much smaller uncertainties encountered for measurements of very low intensity ion beams ( $10^{-19}$  A to  $10^{-16}$  A, equivalent to 0.60.6 cps to 600 cps). However, the dark noise, that is, the observed count rate measured without incident ion beam, shall be measured before an automated MTE measurement sequence to enable corrections to the isotope amount ratios and their uncertainties (7). The dark noise shall be below 0.5 cps.

11.6 *Ion Source and Analyzer Pressure*—It is important to achieve a certain level of vacuum before the isotope amount ratio measurements can begin. See 7.1.7 for the recommended pressure. The peak tailing depends strongly on the vacuum pressure in the detector system since the number of ion collisions with gas molecules inside the mass spectrometer is a direct function of the ambient pressure. Increase in the pressure within the ion source caused by the heating of the ionization and evaporation filaments can be subdued, to a certain extent, by using a cold trap filled with liquid nitrogen.

## 12. Calibration and Standardization

NOTE 1—The measurement method may be qualified following Guide C1068 and calibrated following Guide C1156. Additional information regarding mass spectrometer calibrations with regard to the MTE method may be found in Refs (5, 6).

12.1 *Mass Calibration*—The relationship between the known atomic masses and the magnetic field necessary to direct the isotope beams into the detectors shall be updated on a regular basis. Mass calibration shall be performed at intervals specified by the manufacturer or the user's quality assurance program.

12.2 *Peak Centering*—The peak centering routine is used as a fine adjustment to ensure that the ion beam is centered within the detector. Peak centering usually occurs by means of fine adjustments of the accelerating voltage, and any difference between the value optimized during peak centering from the default accelerating voltage requires a readjustment of the mass calibration curve. Peak centering shall be performed for at least three uranium masses as part of the mass calibration and also before the start of each MTE measurement sequence. During the MTE measurement, peak centering is performed on a regular basis.

12.3 *Amplifier Baseline Calibration*—The baselines of the Faraday cup amplifiers, that is, the amplifier responses without incoming ion beam to the cup, shall be measured on a regular basis and checked for stability. During the MTE measurements, baseline measurements are performed on a regular basis. Note that the integration time for the baseline measurement has a significant influence on the uncertainty of Faraday cup measurements, particularly at lower ion beam intensities. Therefore, the integration time of the baseline (within a measurement) shall be comparable to the integration time of the actual ion beam signal integration. The long-term historical baseline data shall be regularly reviewed by the user to assure that the system performance is within manufacturer specifications and quality system requirements.

12.4 *Amplifier Gain Calibration*—The stability and response of individual Faraday detector amplifiers shall be measured and differences between amplifiers corrected by means of the amplifier gain calibration. Gain calibration is normally performed by sequentially applying a stable calibration current to the input of each Faraday cup amplifier and the output is then normalized to a reference value to generate a gain calibration factor for each amplifier. A gain calibration shall be performed prior to each automatic MTE sequence. Historical gain calibration data can be used to evaluate the stability of the amplifiers.

12.5 *Faraday Cup Efficiency Test*—The response of individual Faraday cups depends on several factors, for example, extent of usage, manufacturing variability, and can also be affected by an insufficient electron suppression voltage. The relative response of the Faraday cups, therefore, shall be determined periodically. Usually, the Faraday cups of a multi-collector system are only intercalibrated for the current amplifiers connected to them (see 12.4) but not for the differences in the efficiencies of the Faraday cups themselves. The efficiencies of the Faraday cups are expected to be similar to each other, which means that the relative efficiencies (relative to one reference cup) are normally close to unity. Note that an (electronic) amplifier gain calibration (see 12.4) shall be performed prior to the Faraday cup efficiency test. The Faraday cup efficiency test can be performed in several ways, as described in 12.5.1 – 12.5.4.

12.5.1 The calibration may be performed by switching a stable ion beam of  $^{187}\text{Re}$  (from a blank filament) between each Faraday cup and a reference Faraday cup. In case a relative efficiency between the detectors is significantly different from unity, this result can be used to correct for differences in the detector response. This procedure can be performed with a relative uncertainty at the level of <0.1 %.

12.5.2 A series of peak-jumping measurements between all Faraday cups and a reference cup to be checked can also be performed



using a sufficiently large uranium sample and one large stable ion beam, for example, a  $\pm 10$  V to 20 V ion beam of  $^{238}\text{U}$  from an LEU or natural uranium sample. The drift of the signal intensity shall be corrected for using the operating software. This procedure can be performed with a relative uncertainty at the level of  $<0.01\%$ .

12.5.3 A series of comparative neodymium (Nd) isotope amount ratio measurements can be performed in two different modes such as the multi-dynamic mode and the static mode with “amplifier rotation” (only for TRITON TIMS, also called “virtual amplifier”: each Faraday cup is connected to each amplifier for regular time intervals during the measurement). This procedure can be performed with a relative uncertainty at the level of few ppm (5). It shall be repeated until all Faraday cups of interest for MTE measurements have been included.

12.5.4 A series of static measurements can be performed using special “multi-isotope” reference materials, such as IRMM-3100a ( $^{233}\text{U}/^{235}\text{U}/^{236}\text{U}/^{238}\text{U} = 1/1/1/1$ ) (8), IRMM-072/1, IRMM-074/1, or IRMM-199 ( $^{233}\text{U}/^{235}\text{U}/^{238}\text{U} = 1/1/1$ ) (9), to include all Faraday cups. This procedure can be performed with relative uncertainties of about  $0.03\%$ .

12.6 *Linearity Test*—There are various procedures to check the linearity of an isotope mass spectrometer detection system. The procedures described in 12.6.1 and 12.6.2 are mainly applicable for Faraday multi-collector systems (for SEM calibration and linearity, see 12.8 and 12.9).

12.6.1 The linearity of the mass spectrometer is determined over the working range of the Faraday cups by measuring the  $^{235}\text{U}/^{238}\text{U}$  ratios of various reference materials under identical conditions. The mass spectrometer system is linear if the *K*-factor, that is, the ratio of the certified  $^{235}\text{U}/^{238}\text{U}$  ratio to the measured  $^{235}\text{U}/^{238}\text{U}$  ratio, is independent of the isotopic composition of the material. For this procedure, the NBL U-series of reference materials (U005a to U970,  $0.50.5\%$  to  $97\%$  of  $^{235}\text{U}$ ) is ideal and can be combined with the IRMM-183-187 series ( $0.3(0.3\%$  to  $5\%$  of  $^{235}\text{U}$ ) and the IRMM 019-029 ( $0.17(0.17\%$  to  $5\%$  of  $^{235}\text{U}$ ). This procedure shall be performed sequentially for all Faraday cups of the multi-collector system needed for the MTE analyses.

12.6.2 The IRMM-072 and IRMM-074 series of reference materials are characterized by  $^{238}\text{U}/^{235}\text{U}$  ratios of  $\approx 1$  and  $^{233}\text{U}/^{235}\text{U}$  ratios ranging from  $\approx 1$  down to  $\approx 10^{-6}$  for the 15 or 10 units, respectively, of the used series. For each unit, the bias of the measured  $^{238}\text{U}/^{235}\text{U}$  ratios from the certified ones can be used for internal mass fractionation correction of the measured  $^{233}\text{U}/^{235}\text{U}$  ratios. The comparison of the corrected  $^{233}\text{U}/^{235}\text{U}$  ratios with the certified ones allows the linearity of the detection system to be checked over a dynamic range of six orders of magnitude for the ion beam intensity. A detailed description of the procedure is given in Ref (9). This procedure shall be performed sequentially for all Faraday cups needed for the MTE analyses.

12.7 *Peak Overlap*—When a Faraday multi-collector system for the simultaneous detection of several masses is used, it needs to be ensured that the peak overlap is acceptable. A mass scan, usually by scanning the magnetic field, shall be performed by which all ion beams are simultaneously moved through the respective cups. The measured intensities for all detectors shall be plotted versus the mass of a reference detector to make the peak overlap visible. All peaks shall have a symmetric shape with a common flat region in the center, with the peak centers reasonably close together, as specified by the manufacturer or the user quality system. After a satisfactory peak overlap is realized (by moving cups relative to one another if necessary), the positions of all detectors shall be saved, for example, as a Faraday cup configuration file. The positions shall be checked and possibly readjusted, manually or using stepping motors, as needed before a new automatic measurement sequence.

12.8 *SEM Linearity Check and Correction*—The linearity of SEM systems shall be checked carefully on a regular basis according to manufacturer’s specifications or the user’s quality assurance program. It is emphasized that there can be more than one reason for nonlinearity of a SEM detector. For SEM detectors operated in ion counting mode, the dead time of the pulse-counting electronic system is always one source of nonlinearity, but this can be easily corrected. As pointed out in Ref (9), there is also the possibility of an intrinsic nonlinearity for SEM detectors, possibly depending on the design of the ion optics, the dynode surfaces, or the electronics, which could cause the linearity investigation and correction to become more complicated. But in case the dead time is confirmed to be the only source of nonlinearity of a SEM system, the value can be determined in various ways (9) using CRMs, as described in 12.8.1 and 12.8.2.

12.8.1 For this procedure, the IRMM-072/8 or IRMM-074/3 (9) reference materials, characterized by a  $^{238}\text{U}/^{235}\text{U}$  ratio of  $\approx 1$  and a  $^{233}\text{U}/^{235}\text{U}$  ratio of  $\approx 0.01$ , or the NBL CRM U500, characterized by a  $^{238}\text{U}/^{235}\text{U}$  ratio of  $\approx 1$  and a  $^{234}\text{U}/^{235}\text{U}$  ratio of  $\approx 0.01$  (using new data published in Ref (5)), can be used. Peak-jumping measurements are performed for count rates between  $5 \times 10^4$  cps and  $5 \times 10^5$  cps for  $^{235}\text{U}$  (similar for  $^{238}\text{U}$ ). The  $^{233}\text{U}/^{235}\text{U}$  ratios ( $^{234}\text{U}/^{235}\text{U}$  in case of NBL CRM U500) are internally normalized using the  $^{238}\text{U}/^{235}\text{U}$  ratios of  $\approx 1$  and plotted versus the  $^{235}\text{U}$  count rate. If the data show a linear relationship with no significant intercept, a linear regression is calculated with the intercept being zero. The slope of the regression line can be used to calculate the dead time using:

$$\tau = \{\text{slope}\} / \left( 1 - \left( \frac{{}^{233}\text{U}}{{}^{235}\text{U}} \right)_{\text{CERT}} \right) \quad (1)$$

where:

$\tau$  = dead time,  
*slope* = slope of linear regression calculation based on measured  ${}^{233}\text{U}/{}^{235}\text{U}$  ratios versus the  ${}^{235}\text{U}$  count rate, and  
 $({}^{233}\text{U}/{}^{235}\text{U})_{\text{CERT}}$  = certified isotope amount ratio of used CRM.

In case NBL CRM U500 is used instead of IRMM-072/8 or IRMM-074/3, the  $({}^{233}\text{U}/{}^{235}\text{U})_{\text{CERT}}$  in Eq 1 has to be replaced by  $({}^{234}\text{U}/{}^{235}\text{U})_{\text{CERT}}$ .

12.8.1.1 In case the data do not indicate a linear relationship with a non-significant intercept, the SEM detection system is likely to be affected by other sources of nonlinearity, which shall be investigated.

12.8.2 For an “external check” of the linearity of the SEM detection system, a series of reference materials can be measured by MTE, for example, the NBL U-series (5), the IRMM-183-187 series, the IRMM-019-029 series, or the gravimetrically prepared IRMM-075 series (6, 10) with  ${}^{236}\text{U}/{}^{238}\text{U}$  ratios of  $10^{-4}$ ,  $10^{-5}$ ,  $10^{-6}$ ,  $10^{-7}$ ,  $10^{-8}$ , and  $10^{-9}$ .

12.9 SEM Versus Faraday Cup Inter-calibration—Since the inter-calibration between a SEM detector with a Faraday cup depends on the ion source focusing and ion beam shape, this calibration shall be performed in an internal manner during the course of each measurement for MTE measurements. For this internal calibration, the ion beam of one of the uranium isotopes present in the sample is switched between the SEM and one Faraday cup within each integration step during the entire measurement. To allow such an internal calibration, there shall be at least one suitable ion beam available for this purpose. This ion beam shall be within a certain intensity range, between the lower limit of reasonable Faraday cup measurements (typically 1 mV on an amplifier with  $10^{11} \Omega$ , which is affected by about the same noise as 0.5 mV on an amplifier with  $10^{12} \Omega$ ) and the upper limit for reasonable SEM measurements (typically  $1.0 \times 10^6$  cps, equivalent to 16 mV on an amplifier with  $10^{11} \Omega$ ). The isotope used for the internal calibration within MTE measurements is for most samples  ${}^{234}\text{U}$ , in few cases  ${}^{236}\text{U}$  instead. As a consequence, the sample amount to be loaded is limited to a certain range as well. For typical TIMS conditions, the sample amount for MTE measurements is about 2 to 6  $\mu\text{g}$ , which provides ion beam signals of about 20 to 30 V for the sum of the main isotopes  ${}^{235}\text{U}$  and  ${}^{238}\text{U}$ . The choice of the isotope used for the inter-calibration depends on the isotopic composition of the sample (based on process knowledge or sample supplier information, or estimated by a mass scan in the  $m/z = 233$  to 238 mass range), in the following way:

12.9.1 Mainly for DU, NU, and LEU samples with  ${}^{234}\text{U}/{}^{238}\text{U}$  ratios between  $3 \times 10^{-5}$  and  $5 \times 10^{-4}$  and with  ${}^{236}\text{U}/{}^{238}\text{U}$  ratios below  $3 \times 10^{-5}$ , the  ${}^{234}\text{U}$  ion beam is used for the internal calibration.

12.9.2 Mainly for DU (in principle also in case of NU and LEU) samples with  ${}^{234}\text{U}/{}^{238}\text{U}$  ratios below  $3 \times 10^{-5}$  and with  ${}^{236}\text{U}/{}^{238}\text{U}$  ratios higher than  $3 \times 10^{-5}$ , the  ${}^{236}\text{U}$  ion beam is used for the internal calibration (also called “reverse” MTE, (6)). Due to the availability and frequent use of amplifiers with resistors of  $10^{12} \Omega$  and  $10^{13} \Omega$ , this “reverse” MTE procedure has become obsolete and is therefore not described in this revision any more.

12.9.3 In the rare case that both the  ${}^{234}\text{U}/{}^{238}\text{U}$  and the  ${}^{236}\text{U}/{}^{238}\text{U}$  ratios are below  $3 \times 10^{-5}$ , the larger one of  ${}^{234}\text{U}$  and  ${}^{236}\text{U}$  shall be used. This might only apply to quite highly enriched  ${}^{235}\text{U}$  or  ${}^{238}\text{U}$  materials, for example, for spike materials. In this case, an internal calibration using a suitable ion beam from an added  ${}^{233}\text{U}$  spike (11) is another option, which would require isobaric corrections because of the possible  ${}^{234}\text{U}$  and  ${}^{236}\text{U}$  contents of the  ${}^{233}\text{U}$  spike. As another option, if amplifiers with a resistor of  $10^{13} \Omega$  are available for measuring  ${}^{234}\text{U}$  and  ${}^{236}\text{U}$ , a MTE measurement of  ${}^{234}\text{U}/{}^{238}\text{U}$  and  ${}^{236}\text{U}/{}^{238}\text{U}$  ratios between  $1 \times 10^{-5}$  and  $3 \times 10^{-5}$  using only Faraday cups is recommended over using the SEM.

12.9.4 For all samples, that is, DU, NU, LEU, or HEU, with any values for the  ${}^{234}\text{U}/{}^{238}\text{U}$  and  ${}^{236}\text{U}/{}^{238}\text{U}$  ratios, an MTE measurement can always be performed using Faraday cups only, thus without using the SEM and without the need for a SEM intercalibration. This shall be carefully considered in view of the associated uncertainties originating on one hand from the SEM calibration and SEM linearity correction (see 12.8) and on the other hand from the higher relative amplifier noise in case of low signals on the Faraday cups. In case both ratios  ${}^{234}\text{U}/{}^{238}\text{U}$  and  ${}^{236}\text{U}/{}^{238}\text{U}$  are higher than  $5 \times 10^{-4}$ , the SEM cannot be used for MTE, only Faraday cups shall be used. In case the  ${}^{236}\text{U}/{}^{238}\text{U}$  ratio is below  $1 \times 10^{-5}$  the use of the SEM for detecting  ${}^{236}\text{U}$  is recommended.

12.9.5 For an “external” check of the SEM versus Faraday intercalibration, a suitable sample with a  ${}^{236}\text{U}/{}^{238}\text{U}$  ratio being in the “overlap” range between SEM and Faraday measurements (between  $3 \times 10^{-5}$  and  $5 \times 10^{-4}$ ) can be measured in a comparative way, first using the SEM and secondly using the Faraday cup for the  ${}^{236}\text{U}$  ion beam. The results shall agree to each other within their

uncertainties. If this is not the case, the reason shall be investigated. Using reference materials such as IRMM-187 and NBL CRM 010 with suitable  $^{236}\text{U}/^{238}\text{U}$  ratios, it was shown in Ref (6) that the above described intercalibration procedure is accurate within uncertainties of about 0.4 % ( $k = 2$ ).

**iTeh Standards**  
**(<https://standards.itih.ai>)**  
**Document Preview**

[ASTM C1832-23](#)

<https://standards.itih.ai/catalog/standards/sist/0dc86eff-5707-4571-a619-b0e59ffa289c/astm-c1832-23>

## 12.10 Mass Fractionation Correction:

12.10.1 In theory, the “classical” total evaporation (TE) and, therefore, also the MTE methods are expected to yield isotope amount ratios that do not need correction for mass fractionation. In practice, measurable mass fractionation for uranium measurements has been observed. To be consistent in the evaluation of the data and the associated uncertainties, it is recommended to perform a mass fractionation correction also for measurement sequences in which the ratios seem to be mass fractionation free, that is, where the *K*-factor (see 12.10.2) is equal to unity within its uncertainty. For MTE measurements it is recommended to perform the mass fractionation correction by measuring a certified isotope reference material in sequence with the samples, and calculate a mass fractionation correction factor based upon the deviation of the measured major ratio from the certified ratio. The mass fractionation correction factor, adjusted for isotope mass difference, is then applied to all measured sample ratios. It is important that the reference materials are prepared and measured in the same manner as the samples. For the MTE method, the major ratio  $^{235}\text{U}/^{238}\text{U}$  is used to calculate a correction factor, known as the *K*-factor, which is then applied also for performing corrections for the minor ratios  $^{234}\text{U}/^{238}\text{U}$  and  $^{236}\text{U}/^{238}\text{U}$  internally (for details see Section 14).

12.10.2 The mass fractionation correction factor, *K*, is calculated as follows:

$$K = (R_c / R_m) \quad (2)$$

where:

*K* = mass fractionation correction factor,  
*R<sub>m</sub>* = average measured isotope amount ratio for the CRM, and  
*R<sub>c</sub>* = certified isotope amount ratio value for the CRM.

12.10.3 To correct individual measured isotope amount ratios, calculate the appropriate mass fractionation correction factor based upon the mass difference between isotopes (= 3 for the major ratio, the  $^{235}\text{U}/^{238}\text{U}$  ratio) and multiply the sample ratio by the applicable mass fractionation correction factor.

12.10.4 An alternative to measuring a CRM using the MTE method to perform the mass fractionation correction, the major ratio of the sample can also be determined separately with possibly lower uncertainty using the double spike method as described in Test Method C1871. The correction of the minor ratios of the sample can be performed internally using the result for the major ratio (for details see Section 14).

## 13. Procedure

<https://standards.iteh.ai/catalog/standards/sist/0dc86eff-5707-4571-a619-b0e59ffa289c/astm-c1832-23>

### 13.1 Sample Preparation:

13.1.1 *Sample Dissolution*—Dissolve an appropriate sample amount to obtain the desired filament loading solution for the mass spectrometric analysis. See Practice C1347 for the dissolution of uranium.

13.1.2 Prepare the sample and any reference material solutions as purified nitrates, using identical chemical preparation and handling steps. For uranium samples hydrolyzed from uranium hexafluoride, it is recommended that the samples are converted to  $\text{U}_3\text{O}_8$  before dissolution in nitric acid and analysis. The solution concentrations shall be chosen to allow for a convenient filament loading (for example, a 1 mg U/mL solution yields 1 μg of uranium per μL, see also 13.2).

13.1.3 *Sample Purification*—Use Practice C1411 or similar procedure to separate uranium from plutonium other impurities.

13.2 *Sample Loading and Conditioning*—Samples for MTE are usually directly loaded on the filament by drop deposition. Samples and reference materials shall be prepared for analysis by the same method at similar mass loadings. Drop deposition onto the filament can be accomplished with the use of a microsyringe fitted with a plastic tip. Change the tip between sample loadings to prevent cross contamination. For filaments loaded by drop deposition, the solution shall be evaporated by passing sufficient electrical current through the filament to cause gentle drying without boiling. Samples for MTE are usually prepared in a 1 *M* nitric acid with a uranium concentration between 1 to 6 mg/g, which is equivalent to 1 to 6 μg/μL. Depending on the uranium amount to be loaded, more than 1 μL may be needed. Deposit drops very carefully and slowly. It is recommended to keep the filament heated by passing 0.50.5 A to 0.7 A current and depositing 1 μL drops at a time. After all drops are loaded, the sample solution on the filament is heated until dryness, for at least one more minute, and then heated for 10 s at a higher current of 1.5 A for conditioning. Alternatively, a stepped-heating program can be used to condition samples, that is, to convert samples to suitable chemical forms. Avoid quick evaporation of the sample or melting the filament. At different facilities, different loading and