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Standard Practice for Determining the Temperature Ratings for Cold Weather Protective Clothing¹

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INTRODUCTION

Manufacturers of cold weather protective clothing want consumers to be thermally comfortable when wearing their products. Therefore, they want to indicate the amount of warmth (that is, insulation) their products will provide to consumers at the point of sale. This is often expressed as a temperature rating on product labels and in product descriptions in catalogs. A temperature rating is commonly understood to mean the lowest air temperature at which the average adult person will have an acceptable level of thermal comfort when wearing the product. Although it is not always stated on labels or in catalogs, manufacturers are assuming that consumers will wear the appropriate amount of clothing with the cold weather garments.

Heated manikins are used to measure the thermal resistance (insulation) and evaporative resistance of clothing ensembles in accordance with Test Methods F1291 and F2370, respectively. The thermal insulation value of a cold weather protective ensemble is used in heat loss models to estimate the thermal comfort of people in cold environments. This approach is also used for sleeping bags (see ISO 23537-1).

1. Scope

1.1 This standard practice covers the determination of the temperature rating of a cold weather protective clothing garment or system of garments when worn with one of two base ensembles. It involves measuring the thermal resistance (insulation) value of a clothing ensemble (base ensemble plus the garment or garment system being evaluated) with a heated manikin in accordance with Test Method F1291. The result is used in a heat loss model to predict the lowest environmental temperature for comfort.

1.2 The predictive model used in this standard estimates the evaporative heat loss from a person wearing cold weather clothing as opposed to measuring the evaporative resistance on a sweating manikin. If a person is active and gets overheated in a cold environment, he/she is usually able to adjust the garments to dissipate excess heat.

1.3 The temperature ratings estimated by this standard practice are guidelines for thermal comfort, determined from a whole-body heat loss model (see Annex A1). Therefore,

¹ This practice is under the jurisdiction of ASTM Committee F23 on Personal Protective Clothing and Equipment and is the direct responsibility of Subcommittee F23.60 on Human Factors.

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localized cooling, discomfort, and even frostbite could still occur at extremely low temperatures because clothing insulation is not evenly distributed over the body surface. In addition, some body parts (for example, ears, fingers, toes) have a high surface area relative to their mass, and consequently lose heat at a faster rate than other parts of the body.

1.4 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety, health, and environmental practices and determine the applicability of regulatory limitations prior to use.*

1.5 *This international standard was developed in accordance with internationally recognized principles on standardization established in the Decision on Principles for the Development of International Standards, Guides and Recommendations issued by the World Trade Organization Technical Barriers to Trade (TBT) Committee.*

2. Referenced Documents

2.1 *ASTM Standards:*²
F1291 Test Method for Measuring the Thermal Insulation of Clothing Using a Heated Manikin

² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

F2370 Test Method for Measuring the Evaporative Resistance of Clothing Using a Sweating Manikin

2.2 *Other Standards:*

ISO 23537-1 Requirements for Sleeping Bags—Part 1: Thermal, Mass and Dimensional Requirements for Sleeping Bags Designed for Limit Temperatures of -20°C and Higher³

ASHRAE 55-2020 Thermal Environmental Conditions for Human Occupancy⁴

3. Terminology

3.1 Definitions:

3.1.1 *clo, n*—a unit of thermal resistance (insulation) equal to $0.155\text{ }^{\circ}\text{C}\cdot\text{m}^2/\text{W}$.

3.1.1.1 *Discussion*—The value of the clo was selected as roughly the insulation value of typical indoor clothing, which should keep a resting person (producing heat at the rate of 58 W/m^2) comfortable in an environment at $21\text{ }^{\circ}\text{C}$, air movement 0.1 m/s . When clo was developed, typical indoor clothing consisted of a three-piece suit and light underclothes.

3.1.2 *clothing area factor (f_{cl})*, *n*—the ratio of the surface area of the clothed body to the surface area of the nude body.

3.1.3 *clothing ensemble, n*—a group of garments worn together on the body at the same time.

3.1.4 *temperature rating, n*—the lowest environmental temperature at which a person can remain thermally neutral while wearing a particular clothing ensemble.

3.1.5 *thermal comfort, n*—that condition of mind which expresses satisfaction with the thermal environment and is assessed by subjective evaluation (see ASHRAE 55-2020).

3.1.6 *thermal insulation, n*—the resistance to dry heat transfer via conduction, convection, and radiation.

3.1.6.1 *Discussion*—The following insulation values can be determined with a thermal manikin:

R_a = thermal resistance (insulation) of the air layer on the surface of the nude manikin,

R_t = total thermal resistance (insulation) of the clothing ensemble and surface air layer around the manikin, and

R_{cl} = intrinsic thermal resistance (insulation) of the clothing ensemble.

R_a , R_t , and R_{cl} are typically used for SI units, while I_a , I_t , and I_{cl} are typically used with clo units. Total insulation values are measured directly with a manikin. Intrinsic clothing insulation values are determined by subtracting the air layer resistance around the clothed manikin from the total insulation value for the ensemble.

4. Significance and Use

4.1 This practice is used to measure the insulation provided by a cold weather clothing garment or garment system using a heated manikin (see Test Method F1291) and to predict the

³ Available from American National Standards Institute (ANSI), 25 W. 43rd St., 4th Floor, New York, NY 10036, <http://www.ansi.org>.

⁴ Available from American Society of Heating, Refrigerating, and Air-Conditioning Engineers, Inc. (ASHRAE), 180 Technology Parkway, Peachtree Corners, GA 30092, <http://www.ashrae.org>.

temperature rating for comfort at two activity levels using whole-body heat loss models.

4.1.1 The temperature rating is for an ensemble—not an individual garment. However, manufacturers want to label cold weather garments or garment systems with a temperature rating to help consumers select the product that will best meet their needs. Therefore, the insulation of a garment or garment system is measured with a standard base ensemble. Furthermore, the standard is limited to garments that cover a substantial amount of body surface area such as jackets, coats, insulated pants, coveralls, or snow suits. The temperature ratings of headwear, footwear, and handwear cannot be determined with this practice.

4.1.2 The temperature predictions determined by this standard practice are for adults only. The physiology of children is significantly different from that of adults, so a modified heat loss model needs to be used to predict the comfort of children wearing outdoor clothing.⁵

4.1.3 The temperature ratings determined by this standard practice and listed on garment labels are only guidelines for comfort and will be affected by the garments consumers wear with them, their activity level during wear, and individual differences in the physiological characteristics of people (for example, gender, age, body mass, etc.).

5. Calibration of Manikin

5.1 *Manikin*—Use a thermal manikin as described in Test Method F1291.

5.2 *Calibration*—Calibrate the manikin using the procedures in Test Method F1291.

5.2.1 The intrinsic clothing insulation value of the Test Method F1291 calibration ensemble (R_{cl}) shall be within $\pm 10\%$ of the reference value before proceeding with this method.

6. Base Ensembles

6.1 A cold weather garment or garment system is typically worn with other garments as part of an ensemble. Therefore, garment or garment systems shall be tested with a base ensemble to determine the temperature for comfort. All cold weather jackets, coveralls, and jacket/pant sets (where the jacket/pant sets are worn together) shall be tested with a lightweight base ensemble that represents the minimum amount of clothing that a reasonable person might wear with the cold weather clothing (Base Ensemble #1). All cold weather pants shall be tested with a base jacket added to the base ensemble (Base Ensemble #2). The size of the garments shall be selected based on the measurements of the manikin.

6.2 The garments used in Base Ensemble #1 are:

6.2.1 *Shirt*—Long-sleeve mock turtleneck shirt, 214 g/m^2 (6.3 oz/yd^2) $\pm 10\%$; worn with shirttail over jeans.

6.2.2 *Jeans*—Denim jeans, 397 g/m^2 (11.7 oz/yd^2) $\pm 10\%$.

6.2.3 *Men's Underwear Briefs*—Jersey knit briefs, 180 g/m^2 (5.3 oz/yd^2) $\pm 10\%$; jockey style that fits snugly at the

⁵ McCullough, E. A., Eckels, S., and Harms, C., "Determining Temperature Ratings for Children's Cold Weather Clothing," *Applied Ergonomics*, Vol 40, 2009, pp. 870–877.

waist and legs (may use briefs from Test Method **F1291** calibration ensemble).

6.2.4 *Men's Socks*—Basic knit sock that covers foot and extends up the calf no more than 25.4 cm (10 in.) from the bottom of the heel. Each individual sock shall weigh 33 ± 5 g (may use socks from Test Method **F1291** calibration ensemble).

6.2.5 *Athletic Shoes*—Fabric/soft leather and soft sole.

6.2.6 *Gloves or Mittens*—Insulated knitted fleece gloves or mittens, 454 g/m^2 (13.4 oz/yd^2) $\pm 10\%$; cuffs worn under jacket sleeves.

6.2.7 *Hat*—Knitted fleece hat, 129 g/m^2 (3.8 oz/yd^2) $\pm 10\%$; worn pulled down to eyebrows.

6.2.8 The intrinsic thermal resistance value (R_{cl}) of Base Ensemble #1 shall be measured according to Test Method **F1291** and the value shall be $0.124 \text{ }^\circ\text{C}\cdot\text{m}^2/\text{W}$ (0.80 clo) $\pm 10\%$.

6.2.8.1 The thermal resistance value of the cold weather ensembles would be higher (and the predicted temperature ratings lower) if a thicker base ensemble was used. However, many people will not wear more clothing with the cold weather garments, and some people might not wear gloves, or a hat, or both. Consequently, this standard practice is specifying a lightweight base ensemble only. It is acceptable for other garments such as thermal underwear to be substituted for the knit shirt and jeans if the intrinsic thermal resistance value is $0.124 \text{ }^\circ\text{C}\cdot\text{m}^2/\text{W}$ (0.80 clo) $\pm 10\%$ and the head, hands, and feet are covered in the same way.

6.3 The garments used in Base Ensemble #2 are:

6.3.1 All of the garments in Base Ensemble #1.

6.3.2 *Jacket*—A jacket with 100 % polyester fiberfill insulation, all layers 339 g/m^2 (10.0 oz/yd^2) $\pm 10\%$. The jacket shall not have a hood, or it shall have a hood that is either detachable or a stow-away hood. A stow-away hood shall not be placed on the head during the test; it needs to be stowed in the collar. A detachable hood shall be removed from the jacket for the test.

6.3.2.1 Only the jacket used for Base Ensemble #2 shall be tested with the hood stowed or removed. Other garments or garment systems shall be tested with the hood up (see **8.5**).

6.3.3 The intrinsic thermal resistance value (R_{cl}) of Base Ensemble #2 shall be measured according to Test Method **F1291** and the value shall be $0.209 \text{ }^\circ\text{C}\cdot\text{m}^2/\text{W}$ (1.35 clo) $\pm 10\%$.

7. Sampling and Test Specimens

7.1 *Sampling*—It is acceptable to test one sample (that is, specimen) of each garment type. However, there will be some variability in garments made of fiberfill or down insulations, so it is recommended to test three specimens and average their insulation values prior to modeling so that sample variability will be reflected in the test results.

7.2 *Specimen Size and Fit*—Select the size of garments that will fit the manikin appropriately (that is, the way the manufacturer designed them to be worn on the human body during their intended end use).

8. Manikin Procedure

8.1 *Environmental Test Conditions*—The test conditions given below shall be standard for all tests unless otherwise stated.

8.1.1 *Air Temperature*—The air temperature shall be at least $12 \text{ }^\circ\text{C}$ lower than the manikin's mean surface temperature (that is, $23 \text{ }^\circ\text{C}$) during a test. When ensembles with high insulation values are tested (for example, cold weather clothing), the air temperature shall be lowered so that a minimum average heat flux of 20 W/m^2 from the manikin's segments is maintained. A temperature around 20 to $23 \text{ }^\circ\text{C}$ may be needed for the nude test and the base ensemble test. A lower air temperature (for example, $5 \text{ }^\circ\text{C}$) will be needed for heavy cold weather ensembles.

8.1.2 *Air Velocity*—The air velocity shall be 0.4 ± 0.1 m/s during a test.

8.1.3 *Relative Humidity*—Select a level between 30 and 80 % relative humidity $\pm 5\%$, preferably 50 %. The relative humidity has no effect on measurements of insulation under steady-state conditions.

8.1.4 If it is necessary to test the cold weather ensembles in different environmental conditions (air temperature, air velocity, or relative humidity), the conditions shall be clearly defined and reported.

8.2 *Mean Surface (Skin) Temperature of Manikin*—The manikin's surface temperature shall be maintained at $35 \pm 0.5 \text{ }^\circ\text{C}$ for all tests. The mean surface temperature shall not be allowed to drift more than $\pm 0.2 \text{ }^\circ\text{C}$ during a 30 min test.

8.3 *Nude Test*—Measure the thermal resistance (R_a) provided by the air layer surrounding the nude manikin by conducting a test using the same procedures given for the cold weather ensemble tests (see **8.5**).

8.3.1 A new nude test shall be conducted for every series of cold weather clothing tests since this value (R_a) is used to calculate the standardized total thermal resistance of each clothing ensemble.

8.4 *Base Ensemble Test*—Measure the total thermal resistance (R_t) provided by Base Ensemble #1 (and Base Ensemble #2 if cold weather pants will be evaluated) by conducting a test using the same procedures given for the cold weather ensemble tests (see **8.5**).

8.4.1 The base ensemble tests shall be conducted periodically to document that the intrinsic thermal resistance values for these ensembles meet the requirements given in the standard within $\pm 10\%$ (see **6.2** and **6.3**).

8.5 *Cold Weather Ensemble Test*—Dress the standing manikin in the appropriate base ensemble and the cold weather garment (such as a jacket, coverall, or pants) or garment system (such as a work jacket and pants set) to be tested. Garment test items with a hood shall be tested with the hood drawn up over the hat and tightened around the face. Position the manikin so that it is hanging vertically a few inches off the floor with its arms at its sides. Take a photograph of the ensemble on the manikin for the report (optional).

8.5.1 Conduct the test in accordance with procedures given in Test Method **F1291**.

8.5.2 *Replication of Tests*—Conduct three replications of the test, with at least 15 min in between test periods. If more than one specimen is available of each garment type, test each separately one time.

9. Insulation Calculations

9.1 The parallel method of calculating the total thermal resistance of the clothing ensemble shall be used. First the total thermal resistance for each single zone is calculated using Eq 1:

$$R_i = (T_i - T_a)A_i / H_i \quad (1)$$

where:

- R_i = total thermal resistance (insulation) of the clothing and surface air layer around a single zone of the manikin ($^{\circ}\text{C}\cdot\text{m}^2/\text{W}$),
- A_i = surface area of a single zone of the manikin (m^2),
- T_i = surface temperature of a single zone of the manikin ($^{\circ}\text{C}$),
- T_a = air temperature ($^{\circ}\text{C}$), and
- H_i = power required to heat a single zone of the manikin (W).

9.2 Then calculate the parallel weighted average for the multi-zone sections of the manikin using Eq 2:

$$R_t = A_{tot} / \sum(A_i / R_i) \quad (2)$$

where:

- R_t = total thermal resistance (insulation) of the clothing on the manikin zone grouping ($^{\circ}\text{C}\cdot\text{m}^2/\text{W}$), and
- A_{tot} = total surface area of manikin zone grouping (m^2).

9.2.1 It is **not** valid to use only the zones of the manikin covered by the cold weather garment in the calculation of thermal resistance used to determine the temperature ratings for comfort. The total thermal resistance value for the whole body shall be used to determine the temperature ratings.

9.3 Determine the average total thermal resistance value (R_t) of the ensemble to the nearest $0.001\text{ }^{\circ}\text{C}\cdot\text{m}^2/\text{W}$ (or nearest 0.01 clo) by averaging the values from the three replications of the test.

9.4 Determine the average intrinsic thermal resistance value of the clothing alone (R_{cl}) to the nearest $0.001\text{ }^{\circ}\text{C}\cdot\text{m}^2/\text{W}$ (or nearest 0.01 clo) using the mean R_t value and Eq 3:

$$R_{cl} = R_t - (R_a / f_{cl}) \quad (3)$$

where:

- R_{cl} = intrinsic thermal resistance (insulation) of the clothing ($^{\circ}\text{C}\cdot\text{m}^2/\text{W}$),
- R_t = total thermal resistance (insulation) of the clothing and surface air layer around the manikin ($^{\circ}\text{C}\cdot\text{m}^2/\text{W}$),
- R_a = thermal resistance (insulation) of the air layer on the surface of the nude manikin ($^{\circ}\text{C}\cdot\text{m}^2/\text{W}$), and
- f_{cl} = clothing area factor (dimensionless).

9.4.1 Use the value of 1.25 for the f_{cl} of Base Ensemble #1.

9.4.2 Use the value of 1.30 for the f_{cl} of Base Ensemble #2.

9.4.3 Use the value of 1.35 for the f_{cl} of a cold weather clothing ensemble (that is, the garment or garment system worn with the base ensemble). It is possible to determine the f_{cl} value for each ensemble using a photographic method, but it is very time consuming. Therefore, an average value for cold weather clothing ensembles is used here.

9.5 Calculate the standardized total thermal resistance value ($R_{t,s}$) of the cold weather clothing ensembles to the nearest $0.001\text{ }^{\circ}\text{C}\cdot\text{m}^2/\text{W}$ (or nearest 0.01 clo) using a standard air layer resistance of $0.078\text{ }^{\circ}\text{C}\cdot\text{m}^2/\text{W}$ (0.50 clo) in Eq 4:

$$R_{t,s} = R_{cl} + (R_{a,s} / f_{cl}) \quad (4)$$

where:

- R_{cl} = intrinsic thermal resistance (insulation) of the clothing ($^{\circ}\text{C}\cdot\text{m}^2/\text{W}$),
- $R_{t,s}$ = standardized total thermal resistance (insulation) of the clothing and surface air layer around the manikin ($^{\circ}\text{C}\cdot\text{m}^2/\text{W}$),
- $R_{a,s}$ = standard thermal resistance (insulation) of the air layer on the surface of the nude manikin, $0.078\text{ }^{\circ}\text{C}\cdot\text{m}^2/\text{W}$ (0.50 clo), and
- f_{cl} = clothing area factor (dimensionless).

9.5.1 The thermal resistance of the air layer measured with a nude manikin (R_a) varies from lab to lab based on the air velocity and the airflow patterns in the chamber. Therefore, each lab needs to use their own R_a value to determine R_{cl} and use the standard $R_{a,s}$ of $0.078\text{ }^{\circ}\text{C}\cdot\text{m}^2/\text{W}$ (0.50 clo) to calculate a standardized total thermal resistance value $R_{t,s}$ for each cold weather ensemble.

9.5.2 If necessary, the thermal resistance in SI units may be converted to clo units using the equivalency provided in 3.1.1.

10. Temperature Ratings

10.1 The heat exchange between the body and the environment depends upon the environmental conditions, the clothing worn, and the activity of the person. All of these factors vary each time a person dons cold weather protective clothing and goes outdoors.

10.1.1 *Environment Conditions*—Air temperature, relative humidity, radiant temperature (for example, solar load), and air velocity (that is, wind) affect thermal comfort. These conditions vary from day to day and throughout the day and night.

10.1.2 *Clothing Worn*—Resistance to dry heat transfer from the body to the environment (that is, insulation value), resistance to evaporative heat transfer (that is, vapor permeability), and pumping during movement are clothing variables that affect thermal comfort. The garments that a person wears with a cold weather garment will change each time he/she wears it, causing the insulation value for the clothing system to vary. People also vary the way that they wear the cold weather garment (for example, hood down, zipper open, without liner, etc.), and these changes will affect insulation and comfort. In addition, if the garments get wet or penetrated by wind, the insulation value will decrease.

10.1.3 *Metabolic Heat Production*—Metabolic heat production is directly affected by a person's activity level. A person's

activity level will vary from sleeping/resting to running or working hard.⁶ As a person's activity level increases, the amount of metabolic heat produced by the body increases, and less insulation is needed for comfort. If the clothing insulation stays the same, the preferred temperature for comfort will be lower when a person is active. However, it is difficult to remain active for long periods of time while wearing thick, protective clothing. If a person is active and begins to feel too warm, he/she will adjust the clothing to dissipate the heat.

10.1.4 *Other Human Factors*—A person's gender, age, body surface area to mass ratio, muscle mass, and perceptions of comfort vary among people and affect thermal comfort also.

10.2 The average total thermal resistance (insulation) value for a cold weather clothing ensemble is used in a heat loss model to estimate the lowest temperature for comfort. (See [Annex A1](#) for equations.) The assumptions for the model are:

10.2.1 Radiant temperature is assumed to be equal to air temperature in the model. In outdoor environments, the radiant heat from the sun provides warmth to a person during the day, and it is possible that he/she will lose more radiant heat to the environment on a clear night.

10.2.2 The effect of wind was not used in the model. Wind will reduce the insulation of a clothing system by decreasing the resistance provided by the external air layer around the body and by penetrating the clothing layers (creating convection currents inside the ensemble). Cold weather garments vary in their wind resistance properties.

10.2.3 An average 50 % relative humidity was used in the model. This parameter varies widely within a 24 h period and from day to day.

10.2.4 The permeability index for the clothing was set at 0.4. This value was used with the insulation value for each clothing ensemble to determine the evaporative resistance of the clothing. The permeability index might be lower for ensembles that are very thick, or are made with shell fabrics that impede moisture vapor transport, or both. However, if a person gets overheated in the cold, he/she will adjust garment closures or open the garment to provide cooling.

10.2.5 The pumping effect was not taken into account in the model. The pumping effect refers to the decrease in clothing insulation during body movement. It occurs because convection heat transfer increases as air is pumped between garment layers and in and out of garment openings during movement. The decrease in clothing insulation varies widely from 10 to 50 % depending upon the design and fit of the clothing. It is typically about 15 to 20 % for outdoor ensembles since garment openings are usually restricted at the wrists, neck, ankles, etc. to prevent cold air from getting inside the ensemble.

10.2.6 The model uses physical and physiological data for an average person. Since human variability affects thermal comfort, the temperature rating predictions need to be considered rough estimates of the air temperature that will result in comfort.

⁶ *The Compendium of Physical Activities Guide*, available at: https://cdnlinks.lww.com/permalink/mss/a/mss_43_8_2011_06_13_ainsworth_202093_sdc1.pdf

10.2.7 The model predicts a temperature rating for low activity (2 MET) and for moderately high activity (4 MET). A person who is lying down or sitting perfectly still produces about 1 MET of heat. A person who is walking very slowly produces about 2 MET of heat, whereas a person who is walking very fast produces about 4 MET. At higher levels of activity, a person will need less insulation and will begin to sweat in the clothing unless he/she adjusts the clothing.

10.2.8 This is a whole-body heat loss model that predicts overall comfort for the body under steady-state conditions. The model treats the insulation of the ensemble as if it were evenly distributed over the body surface. In reality, some parts of the body are better insulated than others in outdoor ensembles. It is possible for localized cooling and discomfort to occur on different parts of the body like the hands, feet, and face, particularly if they are exposed to the environment and/or the air temperature is below freezing.

11. Temperature Rating Calculations

11.1 Total insulation values ranging from 1.0 to 4.0 clo were used in the model to predict the corresponding temperature ratings for 2.0 MET and 4.0 MET of activity. The resulting regression equations were created.

$$TR_2 = -23.78 \cdot I_{t,s} + 89.83 \quad (5)$$

$$TR_4 = -48.61 \cdot I_{t,s} + 86.70 \quad (6)$$

where:

TR_2 = temperature rating (°F) for 2 MET of activity,
 TR_4 = temperature rating (°F) for 4 MET of activity, and
 $I_{t,s}$ = standardized total thermal resistance (insulation) of the clothing and surface air layer around the manikin (clo).

11.1.1 The standardized total thermal resistance (insulation) value shall be converted to clo units (to the nearest 0.01 clo) before predicting the temperature ratings using [Eq 5](#) and [Eq 6](#).

11.2 *Temperature Rating Range*—Use [Eq 5](#) to predict the temperature rating for 2 MET of activity to the nearest 0.1 °F from the standardized total insulation value ($I_{t,s}$) for the cold weather clothing ensemble. Use [Eq 6](#) to predict the temperature rating for 4 MET of activity to the nearest 0.1 °F from the standardized total insulation value ($I_{t,s}$). For example, a jacket ensemble with a standardized total thermal resistance (insulation) value of 2.00 clo will have a temperature rating range of –10.5 °F at high activity to 42.3 °F at low activity.

11.2.1 Convert the temperature rating in °F to °C.

11.3 *Single Temperature Rating*—If only one temperature rating is given for a garment, the comfort temperature predicted from [Eq 5](#) for 2 MET of activity shall be used.

12. Report

12.1 State that the clothing ensembles were tested as directed in Practice F2732.

12.2 Report the following information:

12.2.1 Describe the garments used in the ensembles (for example, fiber content, design features, fabric structure) and provide dressing details.

NOTE 1—It is recommended to include a photograph of the manikin