



Designation: ~~D3552~~—17 D3552 – 24

## Standard Test Method for Tensile Properties of Fiber Reinforced Metal Matrix Composites<sup>1</sup>

This standard is issued under the fixed designation D3552; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reappraisal. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reappraisal.

*This standard has been approved for use by agencies of the U.S. Department of Defense.*

### 1. Scope

1.1 This test method covers the determination of the tensile properties of metal matrix composites reinforced by continuous and discontinuous high-modulus fibers. Nontraditional metal matrix composites as stated in 1.1.6 also are covered in this test method. This test method applies to specimens loaded in a uniaxial manner tested in laboratory air at either room temperature or elevated temperatures. The types of metal matrix composites covered are:

1.1.1 ~~Unidirectional~~—Any fiber-reinforced composite with all Unidirectional laminates (all fibers aligned in a single direction; ~~Continuous direction~~) containing either continuous or discontinuous reinforcing fibers, ~~fibers~~. Both longitudinal and transverse properties ~~properties~~ may be obtained.

1.1.2 ~~0°/90° Balanced Crossply~~—A laminate composed of only 0 and 90° plies. This is not necessarily symmetric, continuous, 0°/90° balanced crossply laminates containing either continuous or discontinuous reinforcing fibers.

1.1.3 ~~Angleply Laminate~~—Any balanced laminate consisting of  $\pm$  theta plies where theta is an acute angle with respect to a reference direction. Angleply laminates containing continuous reinforcing fibers, with layups that do not include 0° reinforcing fibers (that is,  $(\pm 45)_{ns}$ ,  $(\pm 45)_{ns}/(\pm 30)_{ns}$ ,  $(\pm 30)_{ns}$ , and so forth).

1.1.4 ~~Quasi-Isotropic Laminate~~—A balanced and symmetric laminate for which a constitutive property of interest, at a given point, displays isotropic behavior in the plane of the laminate. Multidirectional laminates containing continuous reinforcing fibers, with layups including 0° reinforcing fibers (that is,  $(0/\pm 45/90)_s$ ,  $(0/\pm 45/90)_{ns}$ ,  $(0/\pm 30)_s$ , quasi-isotropic laminates,  $(0/\pm 30)_{ns}$  laminates, and so forth).

1.1.5 ~~Unoriented and Random Discontinuous Fibers~~—Laminates containing unoriented and random discontinuous fibers.

1.1.6 ~~Directionally Solidified Eutectic Composites~~—Directionally solidified eutectic composites.

1.2 The technical content of this standard has been stable since 1996 without significant objection from its stakeholders. As there is limited technical support for the maintenance of this standard, changes since that date have been limited to items required to retain consistency with other ASTM D30 Committee standards. The standard therefore should not be considered to include any significant changes in approach and practice since 1996. Future maintenance of the standard will only be in response to specific requests and performed only as technical support allows.

<sup>1</sup> This test method is under the jurisdiction of ASTM Committee D30 on Composite Materials and is the direct responsibility of Subcommittee D30.04 on Lamina and Laminate Test Methods.

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1.3 The values stated in SI units are to be regarded as the standard. The values given in parentheses are provided for information purposes only.

1.4 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety, health, and environmental practices and determine the applicability of regulatory limitations prior to use.*

1.5 *This international standard was developed in accordance with internationally recognized principles on standardization established in the Decision on Principles for the Development of International Standards, Guides and Recommendations issued by the World Trade Organization Technical Barriers to Trade (TBT) Committee.*

## 2. Referenced Documents

### 2.1 ASTM Standards:<sup>2</sup>

[D3878 Terminology for Composite Materials](#)

[E4 Practices for Force Calibration and Verification of Testing Machines](#)

[E8 Test Methods for Tension Testing of Metallic Materials \[Metric\] E0008\\_E0008M](#)

[E83 Practice for Verification and Classification of Extensometer Systems](#)

[E177 Practice for Use of the Terms Precision and Bias in ASTM Test Methods](#)

[E456 Terminology Relating to Quality and Statistics](#)

[E1012 Practice for Verification of Testing Frame and Specimen Alignment Under Tensile and Compressive Axial Force Application](#)

## 3. Terminology

3.1 *Definitions*—Terminology [D3878](#) defines terms relating to high-modulus fibers and their composites. Terminology [E6](#) defines terms relating to mechanical testing. Terminology [E456](#) and Practice [E177](#) define terms relating to statistics. In the event of a conflict between terms, Terminology [D3878](#) shall have precedence over the other standards.

3.2 *Definitions of Terms Specific to This Standard:*

3.2.1 *continuous fiber, n*—a polycrystalline or amorphous fiber that is continuous within the sample or component or that has ends outside of the stress fields under consideration.

3.2.2 *discontinuous fiber, n*—a polycrystalline or amorphous fiber that is discontinuous within the sample or component or that has its ends inside the stress fields under consideration.

## 4. Summary of Test Method

4.1 A tension specimen is mounted in the grips of a mechanical testing machine and monotonically loaded, in tension, at a constant loading rate until specimen failure occurs. The ultimate strength of the material can be determined from the maximum force carried before failure. If the coupon strain is monitored with strain or displacement transducers, then the stress-strain response of the material can be determined, from which the ultimate tensile strain, proportional limit, and tensile modulus of elasticity can be derived.

## 5. Significance and Use

5.1 This test method is designed to produce tensile property data for material specifications, research and development, quality assurance, and structural design and analysis. Factors that influence the tensile response and should be reported include the following: material, methods of material preparation and lay-up, specimen stacking sequence, specimen preparation, specimen conditioning, environment of testing, specimen alignment and gripping, speed of testing, time at temperature, and volume percent reinforcement. Properties, in the test direction, which may be obtained from this test method include the following:

5.1.1 Ultimate tensile strength,

5.1.2 Ultimate tensile strain,

<sup>2</sup> For referenced ASTM standards, visit the ASTM website, [www.astm.org](http://www.astm.org), or contact ASTM Customer Service at [service@astm.org](mailto:service@astm.org). For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

5.1.3 Tensile modulus of elasticity, and

5.1.4 Poissons ratio.

## 6. Interferences

6.1 Tension test data are used as the principal criteria for the engineering design in actual structural applications. Therefore, it is important to define test conditions that will produce realistic tensile properties, including statistical variation. Such data will allow the design engineer to determine the most appropriate and meaningful margin of safety. The following test method issues will cause significant data scatter:

6.1.1 *Material and Specimen Preparation*—Poor material fabrication practices, lack of control of fiber alignment, and damage induced by improper coupon machining are known causes of high material data scatter in composites.

6.1.2 *Gripping*—A high percentage of grip-induced failures, especially when combined with high material data scatter, is an indicator of specimen gripping problems.

6.1.3 *System Alignment*—Excessive bending will cause premature failure, as well as highly inaccurate modulus of elasticity determination. Every effort should be made to eliminate excess bending from the test system. Bending may occur as a result of misaligned grips or from specimens themselves if improperly installed in the grips or out of tolerance as a result of poor specimen preparation. If there is any doubt as to the alignment inherent in a given test machine, then the alignment should be checked.

## 7. Apparatus

7.1 *Micrometers and Calipers*—A micrometer with a ~~4 to 7 mm [0.16 to 0.28 in.]~~ 4 mm to 8 mm [0.16 in. to 0.28 in.] nominal diameter ball-interface or a flat anvil interface shall be used to measure the specimen thickness. A ball interface is recommended for thickness measurements when at least one surface is irregular (~~e.g., a coarse~~ for example, a coarse surface which is neither smooth nor flat). A micrometer or caliper with a flat anvil interface shall be used for measuring length, width, diameter, and other machined surface dimensions. The use of alternative measurement devices is permitted if specified (or agreed to) by the test requestor and reported by the testing laboratory. The accuracy of the instrument(s) shall be suitable for reading to within 1 % of the specimen dimensions. For typical specimen geometries, an instrument with an accuracy of  ~~$\pm 0.0025$  mm ( $\pm 0.0001$  in.)~~  $\pm 0.0025$  mm ( $\pm 0.0001$  in.) is adequate for thickness measurement, while an instrument with an accuracy of  ~~$\pm 0.025$  mm ( $\pm 0.001$  in.)~~  $\pm 0.025$  mm ( $\pm 0.001$  in.) is adequate for measurement of length, width, diameter, and other machined surface dimensions.

7.2 *Testing Machine*, comprised of the following:

7.2.1 *Fixed Member*—A fixed or essentially stationary member carrying one grip.

7.2.2 *Movable Member*—A movable member carrying a second grip.

7.2.3 *Loading Mechanism*—A loading mechanism for imparting to the movable member a controlled velocity with respect to the stationary member, this velocity to be regulated as specified in Section 11.

7.2.4 *Force Indicator*—A suitable force-indicating mechanism capable of showing the total force carried by the test specimen. This mechanism shall be essentially free of inertia lag at the specified rate of testing and shall indicate the force with an accuracy of  $\pm 1$  % of the indicated value, or better. The accuracy of the testing machine shall be verified in accordance with Practice E4. Further, the calibrated force range used for a particular test shall be chosen to ensure the anticipated maximum forces are between ~~20~~ 20 % to 80 % of the calibrated force range. This is to ensure a linear calibrated force response and protect the force indicator from overload conditions.

7.2.5 *Grips*:

7.2.5.1 *General*—Grip designs shall be suited to the specimens being tested. The grip designs described in Test Methods E8 shall be applicable but should be sized according to the specimen dimensions.

7.2.5.2 *Grips for Round Specimen*—The grips for round specimens shall be standard threaded grips or split-shoulder grips with shoulder surfaces designed to mate with corresponding specimens described in Section 8. The grips shall be self-aligning.

7.2.5.3 *Grips for Flat Specimens*—The grips shall be wedge-type grips or lateral pressure grips with serrated or knurled surfaces for contact with the specimen. The grips shall be self-aligning; that is, they shall be attached to their respective fixed and movable members in such a manner that when any force is applied, the grips will place the axis of a correctly mounted specimen in coincidence with the applied force direction such that no significant moment is placed on the specimen test section, either in the thickness or width direction. The lateral pressure that is imposed by the wedge-type grips or applied by the lateral pressure grips shall be sufficient to prevent slippage between the grip face and the specimen tab surface without causing excessive lateral compressive damage to the specimen. If the serrations are too coarse, emery cloth or similar materials may be used to distribute the gripping force more uniformly over a larger area of the specimen tab. The serrations shall be maintained clean and care shall be taken to maintain specimen alignment during installation.

7.2.5.4 *Grip Alignment*—To ensure a uniform axial tensile stress state within the specimen test section, the following grip alignment criteria shall be maintained. Test systems shall be aligned according to Test Methods E1012. The alignment specimen shall be aligned such that the maximum percent bending throughout the test section, determined at an applied average strain of ~~500  $\mu\epsilon$~~ , 500  $\mu\epsilon$ , shall not exceed 10 %, and the maximum measured strain from any of the strain gages on the alignment specimen, as a result of gripping stresses at zero applied force, shall not exceed ~~50  $\mu\epsilon$~~ , 50  $\mu\epsilon$ .

7.2.6 *Strain*—Strain should be determined by means of either strain gages or an extensometer.

7.2.6.1 *Strain Gages*—The strain gage should be not less than ~~3 mm~~ 3 mm in length for the longitudinal direction and not less than ~~1.5 mm~~ 1.5 mm in length for the transverse direction. The gages, surface preparation, and bonding agents should be chosen to provide for adequate performance on the subject materials and suitable strain-recording equipment shall be used.

7.2.6.2 *Extensometers*—Extensometers used for composite specimen shall satisfy Practice E83, Class B-1 requirements can be used in place of strain gages for 25-mm (1-in.) gage length specimens or exclusively for high-temperature tests beyond the range of strain gage applications. Extensometers shall be calibrated periodically in accordance with Method E83.

## 8. Test Specimens

### 8.1 General:

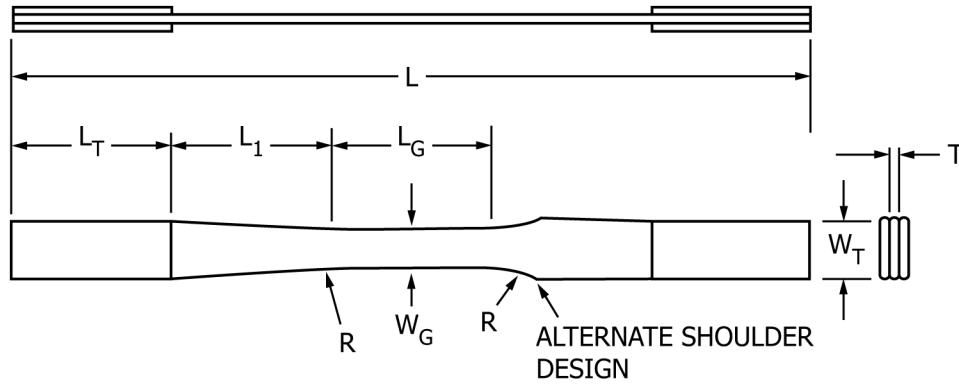
8.1.1 *Test Specimen Size*—Within the limitations of material availability and economy, the specimens shall be sized large enough to be statistically representative of the material to provide meaningful data and, where possible, large enough to affix strain gages or extensometers. Gage lengths incorporating deformation-measuring devices shall be at least ~~13 mm~~ 13 mm (1/2 in.) in length.

NOTE 1—Nonstandard subscaled specimen geometries are supplied for applications in which material size limitations preclude a 13-mm (1/2-in.) gage length. These geometries are useful in material development studies but are not considered as a standard. Test data from these nonstandard specimens shall be evaluated and reported separately in light of their size limitation.

8.1.2 *Specimen Preparation*—Mechanical property determinations of metal matrix composite specimens are particularly sensitive to the effects of improper specimen preparation methods. Great care should be exercised, especially in machining or trimming. Diamond grinding, water jet cutting, or electrical discharge machining (EDM) shall be used. Obtain final dimensions by water-lubricated precision diamond grinding. The depth of diamond grinding required should be determined through careful examination of the as-machined surfaces. Edges should be flat and parallel within the specified tolerances. Grinding must be conducted with adequate precautions to minimize damaging vibrations. In the EDM method, the sample must be suitably mounted for good electrical contact to prevent extraneous arcing and specimen damage. Surface finishing may be accomplished chemically by slight matrix etching or manually by light sanding or filing.

8.1.3 *Specimen Cross Section*—The cross section of the specimen shall be uniform over the gage length. A slight, gradual taper can be tolerated, provided that the minimum section is at the mid length of the gage length and symmetrical with respect to its centerline. In round specimens, the taper shall be limited to a 0.5 % difference in the diameter between the mid length and the ends of the gage length. In flat specimens, the taper shall not exceed 1 % in the width of the test section. The thickness shall not be tapered. To be statistically representative of the material, a minimum of 200 continuous filaments, chopped fibers, or both, is suggested in composites that are oriented in the direction of the force.

8.2 *Flat Specimens*—The standard dimensions of flat specimens are shown in Fig. 1 and are discussed in subsequent sections in terms of the volume fraction and placement geometry of the reinforcement.



Design	$L^A$	$L_T^B$	$L_1$	$L_G$	$W_G$	$R$	$W_T$ (minimum)
Unidirectional and Crossply Laminate Standard Specimen Geometries							
A (reduced section)	152	32	31	26	10	368	13
B (straight sided)	152	32	...	88	10	...	10
C (reduced section)	127	25	25	25	10	25	see Note 1
D (straight sided)	127	25	...	76	13	...	13
E (straight sided)	127	25	...	51	10	...	10
Nonstandard Subscale Specimen Geometries							
F (reduced section)	76	19	6	25	6	13	see Note 1
G (straight sided)	76	25	...	25	13	...	13
Angleply and Quasi-Isotropic Laminate Standard Specimen Geometries (Note 2)							
Angleply and Multidirectional Laminate Standard Specimen Geometries (Note 2)							
H (reduced section) ( $\pm 45$ ) <sub>ns</sub> and (0/ $\pm 45/90$ ) <sub>s</sub>	152	32	31	26	15	368	18
H (reduced section) ( $\pm 45$ ) <sub>ns</sub> and (0/ $\pm 45/90$ ) <sub>s</sub>	152	32	31	26	15	368	18
I (reduced section) ( $\pm 30$ ) <sub>ns</sub> and (0/ $\pm 30$ ) <sub>s</sub>	152	32	31	26	14	368	17
I (reduced section) ( $\pm 30$ ) <sub>ns</sub> and (0/ $\pm 30$ ) <sub>s</sub>	152	32	31	26	14	368	17
J (straight sided) ( $\pm 45$ ) <sub>ns</sub> and (0/ $\pm 45/90$ ) <sub>s</sub>	152	32	...	88	15	...	15
J (straight sided) ( $\pm 45$ ) <sub>ns</sub> and (0/ $\pm 45/90$ ) <sub>s</sub>	152	32	...	88	15	...	15
K (straight sided) ( $\pm 30$ ) <sub>ns</sub> and (0/ $\pm 30$ ) <sub>s</sub>	152	32	...	88	14	...	14
K (straight sided) ( $\pm 30$ ) <sub>ns</sub> and (0/ $\pm 30$ ) <sub>s</sub>	152	32	...	88	14	...	14

<sup>A</sup>May be increased if value indicated in table is insufficient.

<sup>B</sup> $T$  = Specimen thickness, not altered.

NOTE 1—For Specimens C and F,  $W_T = W_G + 2T$ . Taper of the tab is desirable.

NOTE 2—For angleply and quasi-isotropic/multidirectional laminate specimens with different ply orientations,  $W_{Gmax} = \tan\theta(L_G)$ .

FIG. 1 Flat Tension Specimen Design (Dimensions in mm)

### 8.2.1 Unidirectional and Crossply Laminate Composites:

8.2.1.1 *Longitudinal Specimens*—The test specimens for unidirectional and crossply laminate composites tested in the axial direction are shown in Fig. 1, Design A, B, C, D, and E. If necessary, to transition the force into the specimen, or to prevent gripping damage to the filaments near the surface, tabs can be bonded onto the specimen gripping section. The tab length shall be long enough to provide a shear area,  $2W_T L_T$  at each end of the specimen, which is large enough to transfer the maximum force to the specimen. For all but the shortest specimen length, the radius of the curvature of the shoulder should be at least 25 mm (1 in.), and if practical, the edge of the shoulder should be a straight line joining the arc segment and the corner of the tab section. The recommended standard designs for axial specimens of unidirectional and crossply laminate composites are Designs A and B. Designs C, D, and E are considered standard designs when composite material size limitations are encountered. As stated in Note 1, for size-limited panels or blanks used in materials development studies, a nonstandard subscaled specimen (Design F) may be used. Further size limitations (for example, whisker-reinforced composite blanks) will require small specimens, and a standard design is not offered here. Any deviation of specimen geometry from the listed standards or the use of Design F (or any other nonstandard small specimen design) shall be noted in the data summary.

8.2.1.2 *Transverse Specimens*—Transverse strengths of unidirectional composites are low, and larger widths are required to obtain representative and reproducible data. Specimens for such data shall use either Design A or F. However, Design A is the preferred specimen geometry for transverse specimens. Where the length of available composite material direction does not permit a 76-mm (3-in.) specimen (Design G), the gage section may be reduced to a 13-mm (0.5-in.) length. In such cases, the active region of a strain gage, when used, must be placed accurately within the gage length. Any deviation of specimen geometry from the listed standards or the use of Design G (or any other nonstandard small specimen design) shall be noted in the data summary.

8.2.2 Angleply and Quasi-Isotropic Multidirectional Laminate Composites:

8.2.2.1 Specimens—The test specimens for angleply and quasi-isotropic multidirectional laminate composites tested in the axial direction are shown in Fig. 1, Design H, I, J, and K. If necessary, to transition the force into the specimen, or to prevent gripping damage to the filaments near the surface, tabs can be bonded onto the specimen gripping section. The tab length shall be long enough to provide a shear area,  $2W_T L_T$  at each end of the specimen, which is large enough to transfer the maximum force to the specimen. The recommended designs for axial specimens of angleply and quasi-isotropic multidirectional laminate composites are Designs H and I for composites with ply orientations of  $45^\circ$  and  $30^\circ$ , respectively. If other ply orientations are to be tested, the maximum gage width can be calculated by:  $W_{Gmax} = \tan \theta (L_G)$ . Any deviation of specimen geometry from the listed standards or the use of another nonstandard specimen design shall be noted in the data summary.

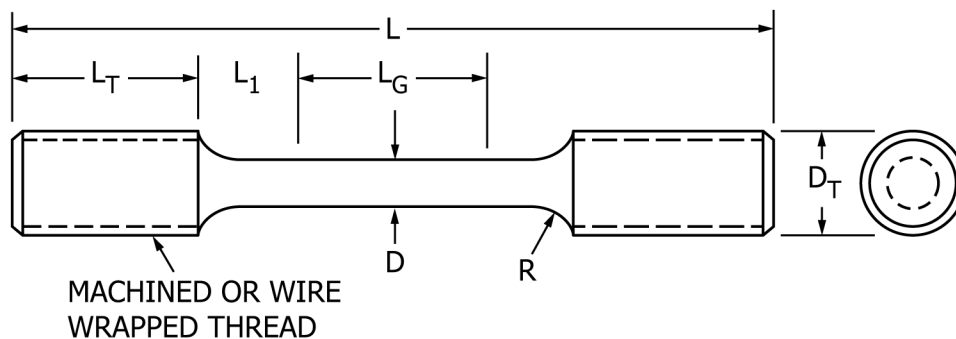
8.3 Round Specimens:

8.3.1 General—Metal matrix composites fabricated by the various liquid infiltration and other techniques that produce massive materials, in contrast to the flat panels produced (for example, by diffusion bonding), are better suited to round cross-section specimen shapes. The preparation of such specimens requires as much care as is required for the preparation of the flat ones. Round specimens may be prepared by reducing the diameter of the test section from a larger composite stock, by building up the head section over a small, constant-diameter composite rod for subsequent machining to the standard head design, or by preforming the head to the final specimens dimensions.

8.3.1.1 Threaded Specimens—Threads can be machined by various means into the cylindrical surface of the head or they can be formed by winding a hard wire into a performed or roughened head. The design for the threaded specimen is shown in Fig. 2, with a listing of the standard dimensions. For continuous filament or for long-fiber composites, the fibers in the gage section shall extend over the complete length of the specimen. For whisker-reinforced composites (small specimens), it is permissible to extend the reinforced section into the grip section only to the extent it ensures that fracture will occur within the gage length.

8.3.1.2 Shouldered Specimen—The loading shoulder of the usual shouldered specimen is an abrupt, flat, or conical transition surface between the small-diameter test section and the larger cylindrical head, as shown in Fig. 3. In continuous-filament composite specimens, the fibers in the gage section shall extend over the entire length of the specimen whereas, in whisker-reinforced specimens, the reinforced region may be permitted to extend into the grip section only sufficiently far enough to ensure that fracture will occur within gage length as in the threaded specimens.

8.3.1.3 Conical Grip Section—The usual head in the shouldered specimen may be insufficient to carry the cylindrical shear stresses that must be developed in very strong, unidirectional reinforced composites.



$L$	$L_T$	$L_1$	$L_G$	$D$	$D_T$	$R$	Thread
102	25	13	25	6	14	6	M14-1.5 (1/2 -13)
76	19	6	25	6	14	6	M14-1.5 (1/2 -13)
76	19	6	25	4	10	8	M10-1.25 (3/8 -16)
76	19	6	25	3	8	3	M8-1.25 (1/4 -20)
51	13	6	13	3	8	3	M8-1.25 (1/4 -20)
51	13	6	13	2	3.5	2	M3.5-0.6 (6-32) or wire wrapped

FIG. 2 Threaded Cylindrical Specimen (Dimensions in mm)