# INTERNATIONAL STANDARD

ISO 5730

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# Stationary shell boilers of welded construction (other than water-tube boilers)

iTeh Schaudières à tubes de fumée de construction soudée (autres que chaudières àquatubulaires) (standards.iteh.ai)

ISO 5730:1992 https://standards.iteh.ai/catalog/standards/sist/0aee8a70-6c30-4668-a932-7f0e838bcce2/iso-5730-1992



Reference number ISO 5730:1992(E)

#### Contents

	Pa	ge
Secti	on 1 General	1
1.1	Scope	1
1.2	Normative references	1
1.3	Definitions	2
1.4	Symbols	3
1.5	Information to be supplied by the purchaser and the manufacturer	6
Secti	on 2 Materials	7
2.1	Introduction	7
2.2	General	7
2.3	Manufacture of the steel	7
2.4	ForgingsiTeh STANDARD PR	ENIEW
2.5	Heat treatment	<b>i</b> )
2.6	Chemical composition	8
2.7	Mechanical properties s://standards.iteh.ai/catalog/standards/sist/0ace8a7(	)- <b>8</b> c30-4668-a932-
2.8	Verification procedures	9
2.9	General rules for carrying out acceptance tests	9
2.10	Number, selection and preparation of samples and test pieces	9
2.11	Method of testing	9
2.12	Retests	9
2.13	Documents	9
2.14	Marking	10
Secti	on 3 Design of the parts under pressure	11
3.1	General	11
3.2	Design pressure	11

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	3.3	Calculation pressure	11
	3.4	Calculation temperature	11
	3.5	Furnaces	12
	3.6	Nominal design stress	12
	3.7	Cylindrical shells under internal pressure	12
	3,8	Unstayed dished heads without openings	13
	3.9	Design of openings in cylindrical shells, spherical shells and dished heads	13
	3,10	Design of isolated openings in shell boiler flat end plates	17
	3,11	Fillet welds attaching compensating plates to shells under internal pressure	18
	3.12	Minimum thickness of nozzles and branch connections	18
	3.13	Access and inspection openings	18
	3.14	Stays, stiffeners and supported surfaces	20
iTeh S	3.15 A	Unpierced tubes and pipes, and tube plates	25
(	3.16 <b>Sta</b>	Furnaces and wet back reversal chambers of cylindrical form subject to external pressure	26
	3.17	Boiler supports	28
https://standards.it	eh.ai/ca Secți	talog/standards/sist/0ace8a70-6c30-4668-a932- on 4. Workmanship and construction in fabrication other than	20
		weiging	20
	4.1	Plate identification	29
	4.2	Cutting of forgings	29
	4.3	Cylindrical shells	29
	4.4	Tell-tale holes	29
	4.5	End plates and tube plates	29
	4.6	Plain tubes and stay tubes	30
	4.7	Manhole frames and openings	30
	4.8	Seating for mountings	31
	4.9	Cylindrical furnaces	32
	4.10	Water-cooled reversal chambers	32
	4.11	Stays	32
	Secti	on 5 Workmanship and construction in welding	34
	5.1	General	34

iii

### ISO 5730:1992(E)

5.2	Materials	34
5.3	Design	34
5.4	Heat treatment and post-weld heat treatment	36
5.5	Non-destructive testing	37
5.6	Openings in or adjacent to welds	39
5.7	Fillet welds	39
5.8	Fabrication	40
5,9	Inspection and tests	51
5.10	Requirements of test results of welded production test plates	56
Sect	ion 6 Inspection and testing	58
6.1	Qualification of inspectors	58
6.2	Inspection during construction (standards.ifeh.a	<b>5</b> 8
6.3	Pressure tests	59
	ISO 5730:1992	
Sect	ISO 5730:1992 ion 7 Documentation, certification and stamping 7f0e838bcce2/iso-5730-1992	)- <b>60</b> 30-4668-a932-
Sect	ISO 5730:1992 ion 7 Documentation, certification and stamping //de838bcce2/iso-5730-1992 Design specification, drawings and data sheets	)-60 <sup>30-4668-a932-</sup> 60
Sect 7.1 7.2	ISO 5730:1992 ion 7 Documentation, certification and stamping Design specification, drawings and data sheets Documents to be submitted to the inspector	)- <u>60</u> 30-4668-a932- 60 60
Sect 7.1 7.2 7.3	ISO 5730:1992 ion 7 Documentation, certification and stamping //oes38bcce2/iso-5730-1992 Design specification, drawings and data sheets Documents to be submitted to the inspector Stamping	60 60 60
Sect 7.1 7.2 7.3 Sect	ISO 5730:1992 ion 7 Documentation, certification and stamping Toessecce/iso-5730-1992 Design specification, drawings and data sheets Documents to be submitted to the inspector Stamping ion 8 Safety valves, fittings and mountings	)- <u>60</u> 30-4668-a932- 60 60 60 61
Sect 7.1 7.2 7.3 Sect 8.1	ISO 5730:1992 ion 7 Documentation, certification and stamping	0-60 <sup>30-4668-a932-</sup> 60 60 60 61 61
Sect 7.1 7.2 7.3 Sect 8.1 8.2	ISO 5730:1992 ion 7 Documentation, certification and stamping	0-60 <sup>30-4668-a932-</sup> 60 60 60 61 61 61 62
Sect 7.1 7.2 7.3 Sect 8.1 8.2 8.3	ISO 5730:1992 ion 7 Documentation, certification and stamping	0-60 <sup>30-4668-a932-</sup> 60 60 60 61 61 61 62 63
Sect 7.1 7.2 7.3 Sect 8.1 8.2 8.3 8.4	ISO 5730:1992 ion 7 Documentation, certification and stamping	0-60 <sup>30-4668-a932-</sup> 60 60 60 61 61 61 62 63 63
Sect 7.1 7.2 7.3 Sect 8.1 8.2 8.3 8.4 8.5	ISO 5730:1992 ion 7 Documentation, certification and stamping	0-60 <sup>30-4668-a932-</sup> 60 60 60 61 61 61 62 63 63 63
Sect 7.1 7.2 7.3 Sect 8.1 8.2 8.3 8.4 8.5 8.6	ISO 5730:1992 ion 7 Documentation, certification and stamping distributes and data sheets Design specification, drawings and data sheets Documents to be submitted to the inspector Stamping ion 8 Safety valves, fittings and mountings Safety valves Water gauges Steam pressure gauges Blowdown mountings Valves for connections Materials for valves and fittings	0-60 <sup>30-4668-a932-</sup> 60 60 60 61 61 61 62 63 63 63 63
Sect 7.1 7.2 7.3 Sect 8.1 8.2 8.3 8.4 8.5 8.6 8.7	ISO 5730:1992 ion 7 Documentation, certification and stamping Design specification, drawings and data sheets Documents to be submitted to the inspector Stamping ion 8 Safety valves, fittings and mountings Safety valves Water gauges Steam pressure gauges Blowdown mountings Valves for connections Materials for valves and fittings Flanges and bolting	0-60 <sup>30-4668-a932-</sup> 60 60 60 61 61 61 62 63 63 63 63 64 64

#### Annexes

Α	Information to be supplied by the purchaser to the manufacturer	122
B	Typical examples of acceptable weld details	123
С	Calculation of tube plate temperatures	146
D	Feed-water and boiler water quality	162
Ε	Model form for inspection certificate	167
F	Model forms for welding procedure approval/welder approval certificates	172
G	Ultrasonic examination of welds	183
н	Magnetic particle examination	197
J	Informative references	203

#### Figures

iTeh S	AWet back boiler PREVIEW	65
2	Wet back boiler (and and and a strength and a stren	65
3	Wet back boiler	66
https://standards.itel	<u>ISO 5730:1992</u> n.ai/ <b>Atyogack.ballsi</b> st/0acc8a70-6c30-4668-a932	66
5	7f0e838bcce2/iso-5730-1992 Semi-wet back boiler	67
6	Relation between heat input and furnace tube inside diam- eter	68
7	Shape factor <i>C</i> for unstayed dished heads without openings	69
8	Reinforcement of openings and branches	70
9	Non-radial branches and adjacent branches	74
10	Compensation for branch in flat end plate	77
11	Compensation for elliptical manholes or inspection openings in flat end plates	78
12	Welding of compensating plates	79
13	Openings for access and inspection	80
14	Typical arrangement of end plate in a multitubular boiler	83
15	Outer limits for supported areas, breathing spaces, main circles and sub-circles in flanged end plates	84
16	Use of sub-circles (twin furnace)	85
17	Use of sub-circles (single furnace)	86

v

18	Determination of factor y	87
19	Example of gusset stays	88
20	Permitted weld details of plain bar stay	89
21	Permitted weld details of stay tubes	90
22	Permitted weld details of bar stays with washers	91
23	Permitted weld details of reversal chamber bar stays	93
24	Typical methods of welding girder stays to reversal cham- bers	94
25	Distances from manhole reinforcing ring	97
26	Location of stays in reversal chamber back plates	98
27	Details of welded gusset stays	99
28	Details for welded and pinned gusset stays	100
29	Details for diagonal link stays	101
30	Notation used for tube bends	101
31	Design factors $C_1$ and $C_0$ (standards itch a)	102
32	Permitted methods of attaching plain tubes	103
33	Second moments of area and cross-sectional area for Fox and Morrison type furnaces ds.itchai/catalog/standards/sist/0ace8a70-	6 <b>.394</b> 4668-a932-
34	Furnace stiffeners up to and including 22 mm thick for plain and corrugated sections	111
35	Furnace stiffeners thicker than 22 mm for plain and corru- gated sections	111
36	Bowling hoops	112
37	Coefficient for calculation of stress at saddle supports	113
38	Mounting screwed into steel distance piece	114
39	Access opening for wet back boilers	115
40	Cutting up the test plate	115
41	Bend test specimens for pipes and tubes	116
42	Test pieces for fillet welds	116
43	Plate alignment	118
44	Reduced section tensile test specimen	119
45	Selection of reduced section tensile test specimens in a thick plate	119
46	All-weld-metal tensile test specimen	119

· · · · ·	47	Side bend test specimen	120
	48	Impact test specimen - V-notch	121
	49	Crossing weld zones where weld imperfections are not per- mitted	121
	B.1	Standard weld preparation details	126
	<b>B.2</b>	Weld preparation details for set-in branches	127
	B.3	Set-on branches	128
	<b>B</b> .4	Set-in branches	129
	B.5	Set-in branches	130
	<b>B</b> .6	Set-in branches	131
	<b>B.</b> 7	Set-in branches	132
	<b>B</b> .8	Forged branch connections	133
	B.9	Forged branch connections	133
iTeh S	B.10	Set-on branches with added compensation rings	134
	B.11 Sta B.12	Set in branches with added compensation rings ndards.iteh.ai) Butt-welded studded connections	135 136
https://standards.i	B.13 iteh.ai/c	Flanges atalog standards/sist/0aee8a70-6c30-4668-a932-	137
	B.14 B.15	Weid neck flange 1992 Attachment of unflanged flat end plates or tube plates to	138
	B.16	shell	139
	<b>B</b> .17	Attachment of furnaces to tube plates or end plates (dished or flat)	141
	B.18	Plate preparation for butt-welded longitudinal and circumferential seams	144
	B.19	Cross seams in end plates	144
	<b>B</b> .20	Attachment of access tube to end plate	145
	C.1	Radiation coefficient $h'_{R}$ for black exchange ( $F = 1$ )	151
	C.2	Determination of overall exchange factor $m{F}$	152
	C.3	$A_{\rm R}/A_{\rm C}$ for a cylindrical chamber with diameter $D$ and length $L$	153
	C,4	Basis convection coefficient $h'_{CO}$	154
	C.5	Determination of correction factor $h_{\rm CO}/h'_{\rm CO}$	155

#### ISO 5730:1992(E)

C.6	Determination of correction factor $h_{\rm CE}/h_{\rm CO}$	155
C.7	Non-dimensional tube area	156
C.8	Non-dimensional plate area	157
C.9	Tube/plate area ratio	158
C.10	Factor $\eta$	159
C.11	Factor $\phi$	160
C.12	Factor $\beta$	161
D.1	Guidance values for silica (SiO <sub>2</sub> )	165
D.2	Guidance values for alkalinity (CaCO <sub>3</sub> )	166
G.1	ISO reference block	191
G.2	Use of reference blocks	191
G.3	Distance-amplitude correction curve	193
G.4	Movements of the shear wave probe for detection of longi- tudinal flaws	194 VIEW
G.5	Reference plane for butt welds (standards iteh ai	195
G.6	Graph representing the ultrasonic beam path	195
G.7	Determination of the conventional length of flaws	<b>196</b> 6c30-4668-a932-
Ц 1	Direction of magnetization 7f0e838bcce2/iso-5730-1992	202

#### Tables

1	Internationally standardized steel types for shell boilers	10
2	Breathing spaces between furnaces and shells when the thickness of the end plate is 25 mm or less	20
3	Weld attachments	23
4	Design parameters for unflanged flat end plates	24
5	Breathing spaces between furnaces and shells when the thickness of the end plate exceeds 25 mm	25
6	Conditions for omitting sections of fillet welds (back welds) from corner joints of flat end plates	36
7	Extent of radiographic or ultrasonic testing for butt welds	38
8	Recommended preheating temperatures for welding of plates, sections, bars and forgings	40
9	Test specimens to be taken from the test plates for butt- welded pipes and tubes	41

# ISO 5730:1992(E)

10	Widths of bend test specimens for pipes and tubes	42
11	Maximum misalignment of plates with circumferential joints	46
12	Maximum misalignment of plates with longitudinal joints	46
13	Maximum reinforced thickness for finished longitudinal and circumferential joints in plates	46
14	Rate of heating above 300 °C during post-weld heat treat- ment	48
15	Rate of cooling to 300 °C during post-weld heat treatment	48
16	Acceptance levels of profile defects in butt welds found by visual examination	52
17	Permitted reinforcement	52
18	Acceptance levels of defects in butt welds found by radi- ography	53
19	Methods of non-destructive testing for connections etc	55
20	Bend test requirements	57
iTeh ST	Guidance conditions for feed-water quality	164
(st	a Guidance conditions for boiler water quality	164
D.3	Guidance conditions for boiler water quality when fed with defonized water	164
	7f0e838bcce2/iso-5730-1992	

#### Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75% of the member bodies casting a vote.

International Standard ISO 5730 was prepared by Technical Committee ISO/TC 11, *Boilers and pressure vessels*, Sub-Committee SC 5, Shell boilers.

Annexes A, B, C, D, E, F, G, H and J of this International Standard are for information only. *Tibes://standards.iteh.ai/catalog/standards/sist/0aee8a70-6c30-4668-a932-*7/0e838bcce2/iso-5730-1992

#### INTERNATIONAL STANDARD

## Stationary shell boilers of welded construction (other than water-tube boilers)

#### Section 1: General

#### 1.1 Scope

1.1.1 This International Standard specifies requirements for both directly fired boilers and wasteheat boilers with a gas-side pressure not exceeding 0,05 N/mm<sup>2</sup> (0,5 bar)<sup>1)</sup>, of cylindrical horizontal de-signs, constructed from carbon or carbon manganese steels by fusion welding and, in the case ds. of directly fired boilers, a design pressure not exceeding 3 N/mm<sup>2</sup>. The boilers covered by this Inter<sub>5730:1992</sub> national Standard are hintended for land use for dards/sist for 68a This International Standard does not cover providing steam or high-pressure hot water. (Typical examples are shown in figures 1 to 5.) This International Standard does not apply to water-tube boilers, to boilers for railway locomotives, or to marine boilers.

1.1.2 This International Standard applies to the boiler proper, from the feed-water inlet connection to the steam outlet connection and to all other connections, including those required for valves and steam and water fittings. If welded ends are used, the requirements specified herein begin or end at the weld where flanges, if used, would have been fitted.

1.1.3 This International Standard applies to boilers having a capacity of greater than 0,025 m<sup>3</sup>, a pressure greater than 0,1 N/mm<sup>2</sup> and a water temperature in excess of 120 °C.

1.1.4 Air preheaters, mechanical stokers, gas- or oil-burning equipment, forced- or induced-draught equipment or other accessories which may be required by the purchaser are not considered as parts

1)  $1 \text{ N/mm}^2 = 1 \text{ MN/m}^2 = 1 \text{ MPa}$ 

 $1 \text{ bar} = 10^5 \text{ N/m}^2 = 10^5 \text{ Pa}$ 

of a boiler for the purposes of this International Standard. Superheaters and economizers either integral with or separate from the boiler shall be constructed to the requirements of the future International Standard for water-tube boilers.

Carrier -

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1.1.5 This International Standard does not cover brickwork setting, insulation or furnace fittings.

iso-57601e890f construction since they cannot be written in sufficient detail to ensure good workmanship and construction. Each manufacturer is responsible for taking every necessary step to make sure that the quality of workmanship and construction is such as to ensure compliance with good engineering practice.

**1.1.7** Informative references are given in annex J.

#### 1.2 Normative references

PREVIEW

The following standards contain provisions which, through reference in this text, constitute provisions of this International Standard. At the time of publication, the editions indicated were valid. All standards are subject to revision, and parties to agreements based on this International Standard are encouraged to investigate the possibility of applying the most recent editions of the standards indicated below. Members of IEC and ISO maintain registers of currently valid International Standards.

ISO 148:1983, Steel — Charpy impact test (V-notch).

ISO 1027:1983, Radiographic image quality indicators for non-destructive testing - Principles and identification.

ISO 1106-1:1984, Recommended practice for radiographic examination of fusion welded joints Part 1: Fusion welded butt joints in steel plates up to 50 mm thick.

ISO 1106-2:1985, Recommended practice for radiographic examination of fusion welded joints ---Part 2: Fusion welded butt joints in steel plates thicker than 50 mm and up to and including 200 mm in thickness.

ISO 1106-3:1984, Recommended practice for radiographic examination of fusion welded joints ---Part 3: Fusion welded circumferential joints in steel pipes of up to 50 mm wall thickness.

ISO 2504:1973, Radiography of welds and viewing conditions for films - Utilization of recommended patterns of image quality indicators (I.Q.I.).

ISO 2604-1:1975, Steel products for pressure purposes — Quality requirements — Part Tr. Forgings.

ISO 2604-2:1975, Steel products for pressure our-ras poses - Quality requirements - Part 2: Wrought seamless tubes.

poses - Quality requirements - Part 3: Electric resistance and induction-welded tubes.

ISO 2605-1:1976, Steel products for pressure purposes - Derivation and verification of elevated temperature properties - Part 1: Yield or proof stress of carbon and low alloy steel products.

ISO 2605-3:1985, Steel products for pressure purposes - Derivation and verification of elevated temperature properties - Part 3: An alternative procedure for deriving the elevated temperature yield or proof stress properties when data are limited.

ISO 4126-1:1991, Safety valves - Part 1: General requirements.

ISO 5579:1985, Non-destructive testing - Radiographic examination of metallic materials by X- and gamma rays - Basic rules.

ISO 5580:1985, Non-destructive testing - Industrial radiographic illuminators - Minimum requirements.

ISO 6947:1990, Welds - Working positions - Definitions of angles of slope and rotation.

ISO 9328-1:1991, Steel plates and strips for pressure purposes — Technical delivery conditions — Part 1: General requirements.

ISO 9328-2:1991, Steel plates and strips for pressure purposes — Technical delivery conditions — Part 2: Unalloyed and low-alloyed steels with specified room temperature and elevated temperature properties.

ISO 10474:1991, Steel and steel products - Inspection documents.

#### 1.3 Definitions

For the purposes of this International Standard, the following definitions apply. Throughout this International Standard additional definitions have been included as necessitated by the specific text concerned.

1.3.1 purchaser: Individual or organization who buys the completed boiler from the manufacturer.

1.3.2 designer: Individual or organization who assumes the sole responsibility for the design of the boiler. He/it determines the shape, dimensions and thickness of the boiler, selects the materials and details the methods of construction and testing.

1.3.3 manufacturer: Individual or organization who ISO 5730 fabricates or assumes responsibility for the fabri-ISO 2604-3:1975, Steel products for pressure pur-2/iso-5730-1992

> 1.3.4 material supplier: Individual or organization not being a material producer, who supplies material or prefabricated standardized parts to be used in the construction of the boiler or any component thereof.

> 1.3.5 producer of the supplied construction material; material producer; Individual or organization who produces materials for the fabrication of the boiler, components or prefabricated standardized parts.

> 1.3.6 regulating authority: Authority in the country of installation which is legally charged with the enforcement of that country's requirements of the law and regulations relating to boilers.

> 1.3.7 inspecting authority: That independent body or association, acting on behalf of

a) the purchaser or owner and/or

b) the regulating authority,

which performs the check that the design, materials and construction requirements comply with this International Standard.

2

**1.3.8 inspector:** Person employed and trained by an inspecting authority to carry out the functions of that inspecting authority as indicated in 1.3.7 (see also 6.1).

**1.3.9 national standard:** Specific standard which has proved to be satisfactory in use, which is acceptable to the regulating authority, which is a specification or rule prepared by a national standards body or similar authority, and which includes rules prescribed by government authorities and having the force of law.

#### 1.4 Symbols

For the purposes of this International Standard, the general terminology and symbols indicated below shall apply. Throughout this International Standard, additional terminology and symbols have been included where necessary to meet the requirements of the specific text concerned. It should also be noted that in some clauses of section 3 (Design of the parts under pressure) the same additional symbol is used in different formulae to represent different terms. However, in all such cases, the special meaning of each symbol is indicated for each formula.

a	Dimensions indicated in figures 14, 16 to 18, 43 and 47.	mm
a,	Inner major axis of compensating plate.	mm
ao	Outer major axis of compensating plate.	mm
A	Effective radiant heating surface (see figures 1 to 5).	m²
A <sub>f</sub>	Cross-sectional area effective as compensation without consideration of allow- ances.	mm²
$A_{\rm fb}$	Cross-sectional area of branch effective as compensation.	mm <sup>2</sup>
$A_{\rm fp}$	Cross-sectional area of reinforcing pad effective as compensation.	mm <sup>2</sup>
Afs	Cross-sectional area of main body effective as compensation.	mm²
Ap	Pressure-loaded area without consideration of allowances.	mm²
A <sub>pb</sub>	Pressure-loaded area relative to branch.	mm <sup>2</sup>
Aps	Pressure-loaded area relative to main body,730-1992	mm <sup>2</sup>
b	Dimensions indicated in figures 14 a16 to 19 34, 35, 43 47 and 8.1668-a932-	mm
$b_1$	Minor axis of manhole. 7f0e838bcce2/iso-5730-1992	mm
b <sub>i</sub>	Inner minor axis of compensating plate.	mm
bo	Outer minor axis of compensating plate.	mm
B <sub>1</sub>	Distance from end plate of shell to centre of saddle.	mm
<i>B</i> <sub>2</sub>	Width of saddle top plate.	mm
с	Corrosion allowance.	mm
С	Shape factor (figure 7).	
$C_1$	Constant depending on method of support as given in 3.14.2.4.	
<i>C</i> <sub>2</sub>	Effective length of nozzle as given in 3.10.2 and figure 10.	mm
$C_3$	Factor for the calculation of stress at saddle support.	
d	Diameter of tube hole.	mm
$d_{i}$	Internal diameter.	mm
$d_{\rm ib}$	Internal diameter of branch.	mm
$d_{ip}$	Diameter of inner periphery of circular pad or compensating plate.	mm
$d_{is}$	Internal diameter of main body (cylindrical shell, spherical shell or dished head).	mm
$d_{g}$	Depth of welded-on girder stay.	mm
$d_{\rm m}$	Mean diameter.	mm
$d_{o}$	Outside diameter.	mm
$d_{\rm ob}$	Outside diameter of branch.	mm
$d_{op}$	Diameter of outer periphery of circular pad or compensating plate.	mm
$d_{os}$	Outside diameter of main body.	mm

d,	Diameter of stay.	mm
D <sub>b</sub>	Gasket mean diameter.	mm
$D_1$	Bolt circle diameter.	mm
e	Minimum wall thickness.	mm
Cob	Calculated wall thickness of branch or standpipe.	mm
Cor	Calculated wall thickness of furnace.	mm
ean	Calculated wall thickness of end plate.	mm
ece	Calculated wall thickness of main body (cylindrical or spherical shell or dished	
US I	head).	mm
ect	Calculated wall thickness of tube.	mm
eg	Thickness of gusset stay.	mm
e <sub>rb</sub>	Actual wall thickness of branch or standpipe minus allowances for corrosion and	
	minus tolerances.	mm
$e_{rep}$	Actual wall thickness of flat end plate.	mm
e <sub>rf</sub>	Actual wall thickness of furnace.	mm
$e_{\rm rp}$	Effective wall thickness of reinforcing pad.	mm
e <sub>rs</sub>	Actual wall thickness of main body (cylindrical or spherical shell or dished head) minus allowances for corrosion and minus tolerances.	mm
e.	Ordered tube thickness.	mm
E	Young's modulus of elasticity at design temperature.	N/mm <sup>2</sup>
f	Nominal design stress of STANDADD DDEVIEW	N/mm <sup>2</sup>
f	Existing mean stress.	N/mm2
fa	Existing mean stress between the centres of two openingsai	N/mm2
σaφ fr	Allowable stress for the branch material	N/mm2
f.	Combined stress at supports.	N/mm <sup>2</sup>
f.	Allowable stress for the reinforcing plate material-720 1000	N/mm2
f.	Allowable stress for the material of the main body	N/mm2
F	Calculation heat flux	W/m2
r. 9.	Clear height as shown in figure 13	mm
G	Gas mass flow rate in first pass tubes	$ka/(m^2 \cdot s)$
h	Minimum width of nusset stay	mm
h.	Depth of curvature of dished head	mm
h.	Height of manhole frame.	mm
h.	Length of skirt of dished head	mm
, H	Net heat input (burner heat release rate based on the net calorific value of the fuel plus any preheat)	·····
I <sub>1</sub>	Second moment of area of one complete furnace corrugation about its neutral axis excluding corrosion allowance	mm4
In	Second moment of area of stiffeners	mm4
ĸ	Thermal conductivity.	(W·mm)/(m2·K)
l.	Effective length of branch contributing to reinforcement	mm
l <sub>rbi</sub>	Effective length of inward projection of set-through branch contributing to re-	
	inforcement.	mm
l <sub>rp</sub>	Effective width of reinforcing pad.	mm
l <sub>rs</sub>	Effective length of main body contributing to reinforcement.	mm
L	Distance between two effective points of furnace support.	mm

$L_1$	Shortest distance from the edge of the access opening to the centre-line of the stay furthest away from the access opening, or, where there is no access opening, half the maximum distance between the centre-lines of the stays.	mm
L <sub>2</sub>	Distance between the rear plate of the reversal chamber and the boiler back end plate.	mm
$L_{\rm b}$	Length of boiler between end plates.	mm
$L_{i}$	Length of leg of fillet weld around inner periphery of pad or compensating plate.	mm
La	Length of welded-on girders.	mm
$L_{\rm h}$	Heated length of furnace.	mm
Lo	Length of leg of fillet weld around outer periphery of pad or compensating plate.	mm
$L_{s}$	Length of shell between end plates.	mm
$L_{t}$	Mean pitch of adjacent tubes.	mm
$p^{-1}$	Calculation pressure.	N/mm <sup>2</sup>
$p_{b}$	Centre-to-centre distance of adjacent openings, referred to wall centre, without allowances.	mm
$p_{\mathrm{b} \varphi}$	Centre-to-centre distance of adjacent openings, offset by angle $\varphi$ , referred to wall centre without allowances.	mm
$p_{c}$	Pitch of corrugations.	mm
$p_{\rm t}$	Hydrostatic test pressure.	N/mm <sup>2</sup>
Q	Force on saddle.	N
r <sub>ik</sub>	Inside radius of knuckle of dished head.	mm
ris	Inside radius of curvature of dished head or spherical shell.	mm
r <sub>ms</sub>	Mean radius of shell. (standards iteh ai)	mm
r <sub>ok</sub>	Outside radius of knuckle of dished head.	mm
ros	Outside radius of curvature of dished head or spherical shell.	mm
<i>R</i> <sub>m</sub>	Minimum tensile strength for the grade of material concerned at room tempera- ture. 7f0e838bcce2/iso-5730-1992	N/mm <sup>2</sup>
$R_{p0,2}$	Minimum value of yield point (0,2 $\%$ proof stress) for the grade of material concerned at temperature <i>t</i> .	N/mm²
$\boldsymbol{S}$	Pitch of welded-on girders.	mm
$S_1$	Factor of safety.	
$S_2$	Factor of safety.	
$S_{o}$	Original cross-sectional area of test piece subjected to a tensile test.	mm²
t	Calculation temperature.	°C
t <sub>m</sub>	Maximum metal temperature.	°C
t <sub>s</sub>	Saturation temperature corresponding to design pressure.	°C
u	Out-of-roundness, or ovality.	%
v	Weld factor.	
w	Depth of corrugations.	mm
W	Force exerted by the pressure on the end plate in the zone assumed to be supported by the gusset.	N
x	Stress reduction factor.	
X <sub>2</sub>	Cross-sectional area of longitudinal section of furnace wall of length equal to one pitch and thickness $e_{\rm rf} - c$ .	mm²
у	Factor determined from figure 18 using the ratio $b/a$ .	
φ	Angle of connecting lines between the centres of two openings relative to the axis of the main body.	dearee