

# SLOVENSKI STANDARD oSIST prEN 14865-1:2007

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Railway Applications - Axlebox lubricating greases - Part 1: Method to test the ability to lubricate ordinary-speed vehicles with speeds up to 200 km/h and high-speed vehicles with speeds up to 300 km/h

Bahnanwendungen - Schmierfette für Radsatzlager - Teil 1: Prüfung der Schmierfähigkeit von Radsatzlagern von Schienenfahrzeugen für normale Geschwindigkeiten bis 200 km/h und für Hochgeschwindigkeitsfahrzeuge bis 300 km/h

<u>oSIST prEN 14865-1:2007</u>

Applications ferroviaires - Graisses Jubrifiantes pour boîtes d'essieux - Partie 1 : Méthode d'essai d'aptitude a lubrifier les véhicules circulant a des vitesses classiques jusqu'a 200 km/h et les véhicules circulant a grande vitesse jusqu'a 300 km/h

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Applications ferroviaires - Graisses lubrifiantes pour boîtes d'essieux - Partie 1 : Méthode d'essai d'aptitude à lubrifier les véhicules circulant à des vitesses classiques jusqu'à 200 km/h et les véhicules circulant à grande vitesse jusqu'à 300 km/h

This draft European Standard is submitted to CEN members for enquiry. It has been drawn up by the Technical Committee CEN/TC 256.

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Recipients of this draft are invited to submit, with their comments, notification of any relevant patent rights of which they are aware and to provide supporting documentation.

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EUROPEAN COMMITTEE FOR STANDARDIZATION COMITÉ EUROPÉEN DE NORMALISATION EUROPÄISCHES KOMITEE FÜR NORMUNG

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# **Foreword**

This document (prEN 14865-1:2006) has been prepared by Technical Committee CEN/TC 256 "Railway applications", the secretariat of which is held by DIN.

This document is currently submitted to the CEN Enquiry.

- Part 1: Method to test the ability to lubricate ordinary-speed vehicles with speeds up to 200 km/h and high-speed vehicles with speeds up to 300 km/h;
- Part 2: Method to test the mechanical stability to cover vehicle speeds up to 200 km/h.

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# Introduction

This European Standard standardizes a test method and acceptance criteria for the demand in EN 12081 for testing the ability to lubricate axlebox lubricating greases. It addresses the issue of lubricating ability of lubricating greases operating under severe conditions.

All lubricants have three main functions – to form a lubricating film that separates rolling elements and raceways, to protect the bearing from corrosion and give good longevity. For lubricating greases in axleboxes there is also the demand that the product must keep the lubricating ability, sometimes without relubrication, during very long periods of time under arduous operating and environmental conditions.

The testing procedure in this European Standard is severe and is used to discriminate between lubricating greases of different lubricating ability.

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# 1 Scope

This European Standard specifies a testing method and sets the acceptance criteria for the determining of the lubrication ability of lubricating greases intended for the lubrication of axle box bearings. The testing method is referred to in EN 12081. The lubricating ability, primarily related to the capability of lubricating greases to protect against wear, is determined in a roller bearing lubricant test rig. Wear of the rolling bearing rollers, the frictional behaviour and temperature during the test are used to discriminate between lubricating greases.

The method is carried out in order to test axlebox greases for ordinary-speed vehicles, with speeds up to 200 km/h, and for greases intended for high-speed vehicles, with speeds up to 300 km/h. The method is a discriminating process, and accepted lubricating greases will be subject to more extensive performance tests according to EN 12082.

For purpose of quality assurance and quality control, this test method is also used for batch testing of lubricating greases.

#### 2 Normative references

The following referenced documents are indispensable for the application of this European Standard. For dated references, only the edition cited applies. For undated references, the latest edition of the document (including any amendments) applies.

ISO 3170, Petroleum liquids Manual sampling RD PREVIEW

EN ISO 4259:1995, Petroleum products Determination and application of precision data in relation to methods of test

ISO 5725-2:1994, Accuracy (trueness and precision) of measurement methods and results — Part 2: Basic method for the determination of repeatability and reproducibility of a standard measurement method c2528bea3c5c/osist-pren-14865-1-2007

ISO 5725-6:1994, Accuracy (trueness and precision) of measurement methods and results — Part 6: Use in practice of accuracy values

#### 3 Terms and definitions

For the purposes of this European Standard, the following definitions apply.

#### 3.1

# lubricating grease

semi-solid product consisting of a mixture of liquid lubricant and thickened with soaps or other thickeners, and may also contain other ingredients, imparting special properties (additives)

#### 3.2

# grease lubricating ability

lubricating ability of the grease during the stressing duration of the test, see 3.3, determined as the mean rolling elements wear rate from tests with four tapered roller bearings.

NOTE In the FE8 test, the lubricating ability of grease is determined by wear and not by the service life of the grease.

#### 3.3

# stressing duration

period of time, t, during which the lubricating grease sample is stressed dynamically and thermally until the test is terminated by the first failure of the test bearings or by the end of the testing period, see 3.4

#### 3.4

#### testing period

time required for testing,  $t_p$ , until failure occurs of one of the test bearings or 500 hours if a test run without interruption

NOTE For approval, the required time for a test is always 500 hours (plus an initial operation during 24 hours at 750 r/min in the 1 500 r/min test). If a bearing will fail earlier, the test is failed.

#### 3.5

#### frictional moment

torque acting as a mechanical resistance to rotation, resulting from bearing friction

#### 3.6

#### frictional moment of the test bearing arrangement

torque,  $M_{\rm f}$ , required for driving the two test bearings, see Figure 1, obtained by measuring the force for retaining the bearing housing when the shaft is rotating

#### 3.7

#### frictional moment of the test bearing arrangement at start

torque,  $M_{rs}$ , of the test bearing arrangement immediately after starting the test

#### 3.8

#### run-in period

period of time,  $E_p$ , from the start of the test until the steady-state is reached

NOTE 1 During the run-in period, the grease is distributed and the run-in wear occurs. Due to the smoothing of the contacting areas, the ratio of the lubricant film thickness to the sum of the roughness of the contact areas increases, thereby increasing the separating effect of the lubricant film. Depending on the smoothing of the contacting surfaces, the frictional moment is continuously reduced during the run-in process.

NOTE 2 For the test run at 1 500 r/min, there is a special run-in period of 24 hours before the real test starts. This run-in is carried out with the lower speed 750 r/min and with the axial load  $Ea = 10 \text{ kN}_{2.9 \text{ebc}} + 4e \cdot 36 - b \cdot 73a - 4e \cdot 36 - b \cdot 73a$ 

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#### 3.9

### Frictional moment of the test bearing arrangement at steady-state

torque,  $M_{rb}$  is obtained after the run-in period and is reached when the frictional moment stabilizes at a fairly constant value (variation can be 20 %)

#### 3.10

#### steady-state temperature

temperature,  $\theta_{\rm B}$ , obtained at the end of the run-in period

#### 3.11

#### test temperature

temperature,  $\theta$ , measured at the outer ring of the spring-side test bearing

NOTE Owing to better heat dissipation, the bearing at the drive side may be 2 to 5 °C cooler.

#### 3.12

#### rolling element wear

wear loss in weight,  $m_w$ , during the stressing period due to wear caused by rolling and sliding movements in the rolling element raceway contacts and rolling element wear from cage contacts

NOTE The loss in weight is determined by weighing the rolling elements on a precision balance before and after the stressing period. A change of the magnetic properties, which may occur during the stressing time of steel parts, can affect the weighing result when an electronic balance is used. To avoid possible weighing errors, the rolling bearing part to be weighed has to be placed at a proper distanced from the electronics, e.g. by suitable equipment.

#### 3.13

## mean rolling element wear

mean rolling element wear in weight,  $m_{wm}$ , from two tests according to this European Standard, each with two bearings, carried out in the same test rig and with lubricating grease from the same sample

#### 3.14

#### combined mean rolling element wear from repeatability tests

mean rolling element wear in weight,  $m_r$ , from four or more tests, each with two bearings, carried out in the same test rig and with lubricating grease from the same sample

### 3.15

### combined mean rolling element wear from reproducibility tests

mean rolling element wear in weight,  $m_R$ , from tests, each with two bearings, carried out with two or more tests in different laboratories and with lubricating grease from the same sample

#### 3.16

#### test speed

operating speed, n, of the test bearing arrangement

#### 3.17

#### test load

load,  $F_a$ , constant in size and acting on the test bearings in axial direction

#### 3.18

#### outlier

a deviating test value that is not fulfilling the statistical criteria specified in ISO 5725-2

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# 4 Symbols

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For the purposes of this European Standard, the following symbols apply: 36-b73a-

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- $E_p$  run-in period, in hours
- Fa test load, in newtons
- $M_{\rm r}$  frictional moment of the test bearing arrangement, in newton metres
- $M_{\rm rb}$  frictional moment of the test bearing arrangement at steady-state, in newton metres
- $M_{\rm rs}$  frictional moment of the test bearing arrangement at start, in newton metres
- $m_{\rm R}$  combined mean value of rolling element wear from tests in different laboratories for establishing reproducibility, in milligrams
- $m_{\rm r}$  combined mean rolling element wear from tests in one test rig for establishing repeatability, in milligrams
- $m_{\rm w}$  rolling element wear, in milligrams
- $m_{\rm wm}$  mean value of rolling element wear from four tested bearings, in milligrams
- n test speed, in revolutions per minute
- R<sub>w</sub> reproducibility limits, in milligrams
- $r_{\rm w}$  repeatability limits, in milligrams
- $s_r$  repeatability standard deviation, in milligrams

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- s<sub>R</sub> reproducibility standard deviation, in milligrams
- t stressing duration, in hours
- t<sub>p</sub> testing period, in hours
- $\mu_{R}$  permissible variation of reproducibility, in milligram
- $\mu_{\rm r}$  permissible variation of repeatability, in milligram
- $\theta$  test temperature, in degrees Celsius
- $\theta_{\rm B}$  steady-state temperature, in degrees Celsius

# 5 Testing principle

The testing procedure corresponds to component wear tests. The two tapered roller bearings installed in the test rig as testing elements are filled with a defined amount of the grease to be tested. The bearings are axially loaded with the test load  $F_a$  and driven with the test speed n.

After a short run-in period  $E_p$ , a practically constant frictional moment, called steady-state moment  $M_{rb}$ , is obtained for the duration of the test.

The steady-state temperature  $\theta_{\rm B}$  depends on frictional energy from the bearings. The steady-state temperature can be controlled by separate heating or cooling and maintained at a specific value independent of variation of bearing friction. A bearing failure due to lubrication break-down causes a progressive increase of the frictional moment  $M_{\rm F}$  to a multiple of the steady-state frictional moment.

Even if a failure does not occur during the testing period  $r_p$ , the lubrication capacity of the grease may be inadequate and by that bring about moderate to severe abrasion of wear of the bearing components. The resulting loss in weight of the rolling elements  $m_w$  is used for assessing the wear-inhibiting capability, or in other words the lubricating ability of the lubricating grease.

### 6 Reagents and material

Use only reagents of recognised analytical grades, e.g. white spirit according to BS 245.

# 7 Test equipment<sup>1)</sup>

### 7.1 Test rig FE8

Figure 1 shows the basic layout of the test head for grease testing with the FE8 test rig. The test head is coupled to a drive unit via the tapered end (Key 7) of the test head shaft (Key 6). The test head is supported by the drive unit via the test head shaft (Key 6). The tapered end (Key 7) is attached to a tapered bore of the driving shaft of the drive unit before starting a test and detached when the test is finished. The driving shaft of the drive unit is driven directly by an electric motor or by a gear.

<sup>1)</sup> Information about suppliers can be obtained from Fachausschuss Mineralöl- und Brennstoffnormung, FAM, (technical committee for mineral oil and fuel standardization), Kapstadtring 2.22297 Hamburg, Germany.

Various speeds between 7,5 and 3 000 r/min can be chosen. The test bearings (Keys 3 and 4) are installed in the head. The bearings are axially loaded by means of Belleville springs (Key 1). The width of the spacer ring (Key 2) and the deflection characteristic of the selected springs determine the magnitude of the load and have to be calibrated according to the maintenance plan. Instead of a spacer ring (Key 2) it is possible to use a load cell to bring about the correct load.

The test head is provided with inserted thermocouples for measuring the outer ring temperature of the bearings (Key 5).

The frictional moment of the bearings is measured. This is carried out by means of a force transducer (beam with strain gauges) that transmits the holding force of the housing at (Key 8) to an amplifier. A plotter records the holding force. The holding force prevents the housing from rotating due to the frictional moment from the bearings.

# 7.2 Test bearings

For the test, two tapered roller bearings are mounted in the test head. The bearings are similar to standard bearing 31312, but are provided in a special execution for the FE8 test<sup>1)</sup>.

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