



# SLOVENSKI STANDARD

## SIST EN 14571:2005

01-julij-2005

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### Kovinske prevleke na materialih z nekovinsko osnovo – Merjenje debeline prevleke – Metoda mikropornosti

Metallic coatings on nonmetallic basis materials - Measurement of coating thickness - Microresistivity method

Metallische Überzüge auf nichtmetallischen Grundwerkstoffen - Schichtdickenmessung - Mikro-Widerstand-Verfahren (standards.iteh.ai)

Revetements métalliques sur matériaux non-métalliques - Mesurage de l'épaisseur des revêtements - Méthode utilisant la microresistivité

Ta slovenski standard je istoveten z: EN 14571:2005

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#### ICS:

17.040.20	Lastnosti površin	Properties of surfaces
25.220.40	Kovinske prevleke	Metallic coatings

**SIST EN 14571:2005**

**en**

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EUROPEAN STANDARD

EN 14571

NORME EUROPÉENNE

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April 2005

ICS 25.220.40; 17.040.20

English version

## Metallic coatings on nonmetallic basis materials - Measurement of coating thickness - Microresistivity method

Revêtements métalliques sur matériaux non-métalliques -  
Mesurage de l'épaisseur des revêtements - Méthode  
utilisant la microrésistivité

Metallische Überzüge auf nichtmetallischen  
Grundwerkstoffen - Schichtdickenmessung - Mikro-  
Widerstand-Verfahren

This European Standard was approved by CEN on 3 March 2005.

CEN members are bound to comply with the CEN/CENELEC Internal Regulations which stipulate the conditions for giving this European Standard the status of a national standard without any alteration. Up-to-date lists and bibliographical references concerning such national standards may be obtained on application to the Central Secretariat or to any CEN member.

This European Standard exists in three official versions (English, French, German). A version in any other language made by translation under the responsibility of a CEN member into its own language and notified to the Central Secretariat has the same status as the official versions.

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## Foreword

This document (EN 14571:2005) has been prepared by Technical Committee CEN/TC 262 “Metallic and other inorganic coatings”, the secretariat of which is held by BSI.

This European Standard shall be given the status of a national standard, either by publication of an identical text or by endorsement, at the latest by October 2005, and conflicting national standards shall be withdrawn at the latest by October 2005.

This document includes a Bibliography.

According to the CEN/CENELEC Internal Regulations, the national standards organizations of the following countries are bound to implement this European Standard: Austria, Belgium, Cyprus, Czech Republic, Denmark, Estonia, Finland, France, Germany, Greece, Hungary, Iceland, Ireland, Italy, Latvia, Lithuania, Luxembourg, Malta, Netherlands, Norway, Poland, Portugal, Slovakia, Slovenia, Spain, Sweden, Switzerland and United Kingdom.

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## EN 14571:2005 (E)

## 1 Scope

This document describes a method for nondestructive measurements of the thickness of conductive coatings on nonconductive base materials. This method is based on the principle of the sheet resistivity measurement and is applicable to any conductive coatings and layers of metal and semiconductor materials. In general, the probe has to be adjusted to the conductivity and the thickness of the respective application. However, this document focusses on metallic coatings on nonconductive base materials (e.g. Copper on plastic substrates, printed circuit boards).

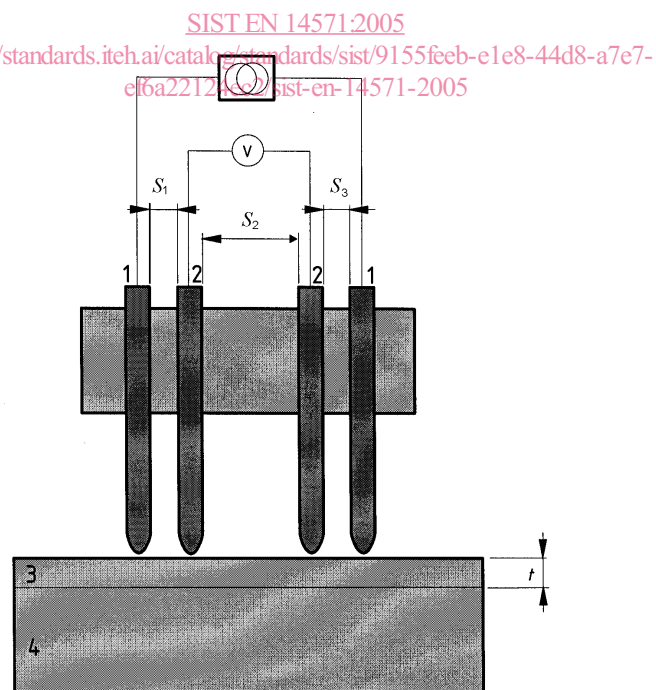
NOTE 1 This method also applies to the measurement of through-hole copper thickness of printed circuit boards. However, for this application a probe geometry different from the one described in this document is necessary.

NOTE 2 This method is also applicable for thickness measurements of conductive coatings on conductive base materials, if the resistivity of the coating and the base material is different. This case is not considered in this document.

## 2 Measurement principle

The sheet resistivity method uses the so called four-point probe as shown in Figure 1. A row of four spring-loaded metal tips are placed in contact with the surface of the conductive coating. The tip distances between the outer and inner tips  $S_1$  and  $S_3$  are equal. Usually a constant current is passed through the two outer contacts (4 and 7). The introduced current penetrates the conductive material of the coating with the resistivity  $\rho$ . The resulting voltage drop is measured across the two inner contacts (5 and 6).

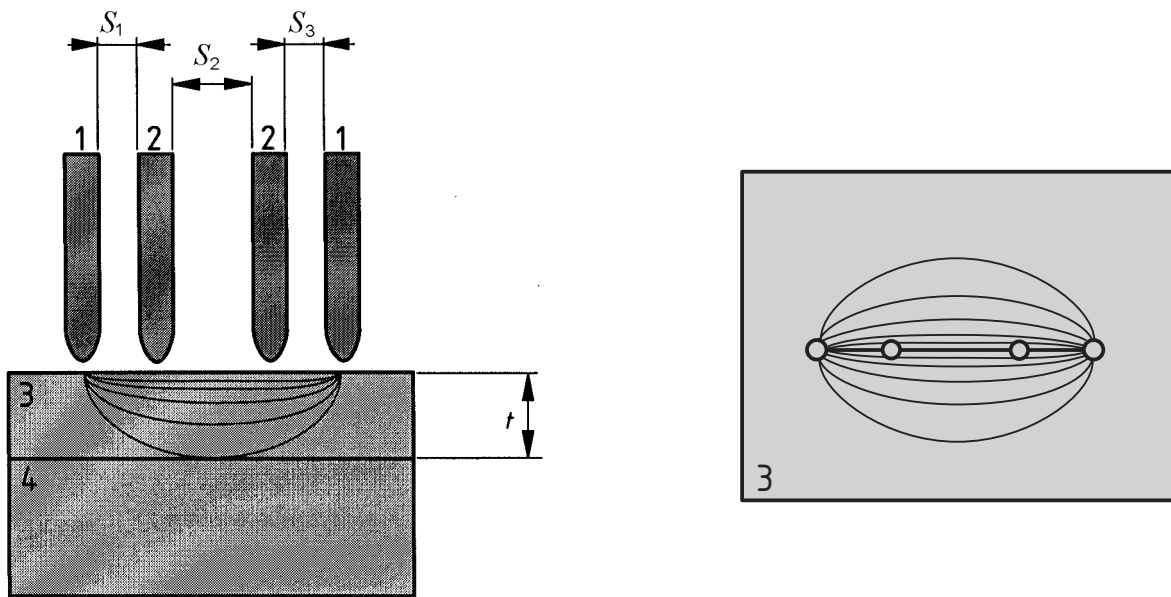
In general, the flow of the introduced current is non-uniformly distributed over the cross-section of the coating and is not parallel to the coating (see Figure 2). The current density decreases with increasing distance from the direct line between the contacts 4 and 7 (with depth and width). If the current is effectively limited by the thickness of the coating, the voltage drop between 5 and 6 is a measure of the thickness.



### Key

- 1 Outer contact of the probe
- 2 Inner contact of the probe
- 3 Conductive coating
- 4 Nonconductive base material
- $t$  Coating thickness

Figure 1 — Schematic representation of the sheet resistivity method



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- 2 Inner contacts of the probe
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**Figure 2 — Schematic representation of the non-uniformly distributed current within the coating**

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The measured voltage drop depends on the resistivity of the metallic coating, on the probe geometry (distance of the 4 probe contacts  $S_1$ ,  $S_2$ ,  $S_3$ ), the applied current and the thickness of the coating. If the resistivity of the coating can be expected to be homogenous and the thickness is sufficiently small, the measured voltage drop is determined only by the unknown thickness and the applied current. In general, there is no simple and practical equation to calculate the thickness as a function of the material resistivity, the probe geometry and the measured voltage and current. However, there are some well known approximations for practical use in certain cases. Especially in the case of equal tip distances ( $S_1=S_2=S_3= S$ ) and for a thickness to probe spacing ratio  $t/s < 0,5$  the coating thickness,  $t$ , in micrometres, can be calculated using the equation:

$$t = \rho \frac{I}{V} \frac{\ln(2)}{\pi} \quad \left[ \text{when } \frac{t}{S} < 0,5 \right] \quad (1)$$

where

$\rho$  is the resistivity coating, in ohm.m;

$V$  is the potential difference across the inner probe tips, in Volts;

$I$  current passed through outer probe tips, in amps;

$S$  is the equal probe tip spacing ( $S=S_1=S_2=S_3$ ).

Usually the supplied current  $I$  is held constant. Therefore, the coating thickness is inversely proportional to the measured voltage :

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$$t = \frac{C}{V} \quad (2)$$

where

$C$  is a the constant  $0,221\rho l$

Equation (2) is the basis for many applications in the above case. In general suitable correction functions for Equation (2) are necessary if the prerequisite of a ratio  $t/s < 0,5$  or an equal probe tip spacing is not satisfied.

Because the introduced current decreases with increasing penetration depth, a sufficiently thick coating does not limit the current and the coating appears to be infinite to this method. The wider the probe spacing the deeper the current penetrates into the conductive material. Consequently, the measurement range is determined by the probe spacing for a given coating material. The probe geometry (tip spacing) has to be adjusted with respect to the conductivity and the expected thickness range of the application of interest. Furthermore, the sensitivity of this method decreases with increasing thickness.

The application of Equation (2) is also limited by very thin coatings because the resistivity is expected to be constant and not a function of the thickness. However, for very thin thicknesses the resistivity starts to increase and below a critical thickness this increase of the resistivity is strongly pronounced. Typical values of this critical thickness are in the range of approximately 10 nm to 300 nm for metals. For measurements in this range and below this critical thickness a special calibration or additional correction functions are necessary.

Because the introduced current decreases with increasing distance in width, the current flow is not affected by a sample width wider than a critical width. Therefore, the sample width has to be wider than this critical width. Otherwise, the measured thickness becomes a function of the sample width and the sample width has to be considered in addition. The probe spacing also determines the value of the critical width for a given coating material.

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### 3 Factors affecting measurement uncertainty

#### 3.1 Range of measurement

The measurable thickness range is determined by the probe geometry (tip distance) and the conductivity of the coating. The probe geometry has to be adjusted to the thickness range of interest.

Usually the manufacturer provides the uncertainty of the respective probe for the recommended thickness range.

#### 3.2 Coating resistivity

Measurements will be affected by the resistivity of the coating if the resistivity of the coating differs from the resistivity of the calibration standard(s) used to calibrate the instrument. A 5 % difference in resistivity will result in a 5 % error unless this difference is accounted for in the calibration procedure.

Furthermore, a homogenous resistivity throughout the coating is expected for this method. The measurement will be affected by a resistivity variation of the coating. This can be caused by composition variation of the coating, by coating defects (e.g. cracks, porosity, voids, inclusions) or by a surface preparation or contamination.

#### 3.3 Width of the sample

Below a critical width, determined by probe design (tip spacing) and to a lesser degree on the electrical conductivity of the metallic coating, the coating thickness measurement becomes dependent upon the width of the electrical current path (e.g. conductive track width of printed circuit boards). The instrument shall therefore be calibrated using calibration standards of the width to be measured or appropriate correction functions shall be used.



NOTE 1 An exact positioning of the probe in the middle of the sample (e.g. conductive track) and parallel to its direction is necessary to avoid measurement errors. Usually special probe positioning systems or probe guides are provided by the manufacturers.

NOTE 2 If the critical path width is not known, or for some reason is unobtainable, it may be obtained using a number of reference standards having the same thickness (made from the same piece of uniform material), but of different known widths (see Annex A).

### 3.4 Curvature

Sharp or small radii of curvature will greatly affect the thickness measurement. This effect is minimised if the probe is placed on the surface so that its axis is parallel to that of the curved surface. Alternatively, calibration standards of the same curvature can be used. The influence decreases with increasing radii of curvature.

### 3.5 Surface roughness

Measurements are affected by surface topography of the metallic coating. Rough surfaces can cause thickness measurement errors. In such cases it is strongly recommended to perform a sufficient number of measurements at different locations on the sample and using the mean together with the standard deviation as a representative thickness value of the coating.

### 3.6 Temperature

A temperature change between calibration and measurement causes errors of the measured thickness because the resistivity of the coating varies with temperature. This temperature influence is important especially if the resistivity temperature coefficient of the coating material is high (e.g. Cu :  $\alpha=0,0039\text{ K}^{-1}$ ). Therefore, the temperature of the sample should be measured and the thickness should be corrected with respect to temperature. Some manufacturers provide instruments with a temperature sensor and an automatic temperature correction for this purpose.

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### 3.7 Probe contact pressure

The pressure with which the probe contacts are applied to the test specimen can affect the instrument readings. The applied pressure should therefore be made constant and as low as possible to minimise sample damage but still steady to ensure a good repeatability (reliable contact to the coating). This is achieved in practice by using a constant pressure probe having tips supported by adapted springs. The shape of the tips can be sharpened or rounded with respect to the coating material to achieve a reliable contact.

The current through the two outer tips should be applied only if the contact of the tips is established in order to avoid possible damages of the surface.

## 4 Calibration of instruments

### 4.1 General

Before use each instrument shall be calibrated in accordance with the manufacturer's instructions, using suitable calibration standards. Appropriate attention shall be given to the factors listed in Clause 3 and to the procedures of Clause 5.

### 4.2 Calibration standards

Calibration standards of known coating thickness, uniform and homogenous coating resistivity and sufficient width (above the critical width) shall be used.

At least two or more calibration standards having different but known thicknesses appropriately distributed over the thickness range of interest shall be used for instrument calibration. Two calibration standards are the minimum if a