

Designation: B 917/B 917M - 01

Standard Practice for Heat Treatment of Aluminum-Alloy Castings from All Processes¹

This standard is issued under the fixed designation B 917/B 917M; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ϵ) indicates an editorial change since the last revision or reapproval.

1. Scope*

1.1 This practice is intended, when specified by material specification or purchase order, for the use in the heat treatment of aluminum alloy castings from all casting processes.

1.1.1 The heat treatment of aluminum alloy castings used in specific aerospace applications is covered in AMS 2771^2 and specific AMS² material specifications.

1.1.2 The heat treatment of wrought aluminum alloys is covered in Practice **B** 918.

1.2 The values stated in either inch-pound units or SI units are to be regarded separately as standards. The SI units are shown in brackets or in separate tables. The values stated in each system are not exact equivalents, therefore each system must be used independent of the other. Combining values from the two systems may result in non-conformance with the practice.

1.3 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the usre of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

2. Referenced Documents atalog/standards/sist/b2fcf34c-

2.1 The following documents of the issue in effect on the date of material purchase form a part of this specification to the extent referenced herein:

2.2 ASTM Standards:

- **B 26/B 26M** Specification for Aluminum-Alloy Sand Castings³
- **B** 108 Specification for Aluminum-Alloy Permanent Mold Castings³
- B 275 Practice for Codification of Certain Nonferrous Metals and Alloys, Cast and Wrought³
- B 557 Test Methods of Tension Testing Wrought and Cast Aluminum and Magnesium-Alloy Products³

- **B 557M** Test Methods of Tension Testing Wrought and Cast Aluminum and Magnesium- Alloy Products [Metric]³
- **B 618** Specification for Aluminum-Alloy Investment Castings³
- **B 686** Specification for Aluminum-Alloy Castings, High Strength³
- **B** 881 Terminology Relating to Aluminum- and Magnesium-Alloy Products³
- B 918 Practice for Heat Treatment of Wrought Aluminum Aloys³
- G 110 Practice for Evaluating Intergranular Corrosion Resistance of Heat Treatable Aluminium Alloys by Immersion in Sodium Chloride + Hydrogen Peroxide Solution⁴
 2.3 ANSI Standard:

H35.1 Alloy and Temper Designation Systems for Aluminum⁵

3. Terminology

3.1 Definitions:

3.1.1 Refer to Terminology **B** 881 for terminology relating to the heat treatment of castings.

4. Equipment

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4.1 *Heating Media*—Aluminum castings are typically heat treated in air chamber furnaces; however lead baths, oil baths, fluidized beds, or even superheated steam may be used in specific applications. However the use of uncontrolled heating is not permitted. Whichever heating means are employed, careful evaluation is required to ensure that the casting responds properly to heat treatment and is not overheated or damaged by the heat treatment environment. Salt baths are not recommended for the commercial heat treatment of aluminum castings in volume. (**Warning:** Nitrate baths must not be used in the heat treatment of 5xx.0 series castings because of the inherent explosion hazard.

4.2 *Air Chamber Furnaces* may be oil or gas-fired or may be electrically heated. The atmosphere in air chamber furnaces must be controlled to prevent porosity resulting from solution heat treatment. Furnace components that are significantly

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¹ This practice is under the jurisdiction of ASTM Committee B07 on Light Metals and Alloys and is the direct responsibility of Subcommittee B07.01 on Aluminum Alloy Ingots and Castings.

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² Available from SAE-AEROSPACE, 400 Commonwealth Drive, Warrendale, PA 15096-0001, USA.

³ Annual Book of ASTM Standards, Vol 02.02.

⁴ Annual Book of ASTM Standards, Vol 03.02.

⁵ Available from American National Standards Institute, 25 West 43rd Street, 4th Floor, New York, NY 10036.

hotter than the metal should be suitably shielded for section thicknesses of less than 0.250 in. [6 mm] to prevent adverse radiation effects. The atmosphere in air chamber furnaces must be controlled to prevent porosity resulting from solution heat treatment (see Note 1). The suitability of the atmosphere in an air-chamber furnace can be demonstrated by testing, in accordance with 8.4.3.1, that products processed in that furnace are substantially free of heat treat induced porosity.

NOTE 1—Heat treat induced porosity may lower mechanical properties and commonly causes blistering of the surface of the material. The condition is most likely to occur in furnaces in which the products of combustion contact the work, particularly if the gases are high in water vapor or contain compounds of sulfur. Surface discoloration is a normal result of solution heat treatment of aluminum alloys and should not be interpreted as evidence of damage from overheating or as heat treat induced porosity.

4.3 Automatic Recording and Control Equipment to control temperature of air furnaces shall be capable of maintaining temperature in the working zone to within $\pm 10^{\circ}$ F [$\pm 5^{\circ}$ C] of the specified temperature.

4.4 *Quench Baths*—Quenching is normally performed by immersion of castings in a hot-water bath as described in Tables 1-4. The water baths must be located close enough to solution heat-treating facilities to minimize delay in quenching. Tanks must be of adequate size for the expected work load and must have the means of providing adequate circulation of the quenching media about the work load. Means for heating or cooling the quench water should be available when needed.

NOTE 2—Quenching may be performed by alternative means such as total immersion in a glycol and water solution, a liquefied gas, cold water, hot water, or boiling water, or by air blast or fog to minimize distortion provided samples from the material, so quenched, will conform to the (a) mechanical properties, (b) other requirements of the applicable casting specification and (c) not exhibit more intergranular corrosion susceptibility than if the metal was immersion quenched in cold water. The use of water sprays or high-velocity high-volume jets of water in which the material is thoroughly and effectively flushed is satisfactory for quenching. Alternative quench media are frequently contingent on the particular alloy and the end use of the casting.

5. Furnace Temperature Uniformity and Calibration Requirements

5.1 Calibration of Equipment:

5.1.1 Thermocouple wire and sensors shall be calibrated against wire or sensors whose calibration is traceable to the National Institute of Standards and Technology (NIST). Thermocouples made from calibrated wire rolls may be used in lieu of individually calibrated thermocouples in which case, the roll calibration shall be that of the average of samples taken from both ends of the roll. The roll shall not be used if the difference in the highest and lowest reading exceeds $2^{\circ}F$ [1°C].

5.1.2 Working instruments shall be calibrated at least once every three months against a test instrument that is traceable to the National Institute of Standards and Technology (NIST). Accuracy shall be \pm 0.3 % of range.

5.2 Furnace Temperature Survey:

5.2.1 A temperature survey, to ensure compliance with the applicable recommendations presented herein, shall be performed for each furnace.

5.2.2 A new temperature survey shall be made after any modification, repair, adjustment (for example, to power controls, or baffles), or rebuild which may have altered the temperature uniformity characteristics of the furnace and reduced the effectiveness of the heat treatment.

5.3 Batch Furnace Surveys:

5.3.1 The initial temperature survey shall be made at the maximum and minimum temperature of solution heat treatments and precipitation heat treatments for which each furnace is to be used. There shall be at least one test location for each 25 ft³ [0.70 m³] of air furnace volume up to a maximum of 40 test locations, with a minimum of nine test locations, one in each corner and one in the center.

5.3.2 After the initial survey, each furnace shall be surveyed monthly, except as provided in 5.3.7. The monthly survey shall be at one operating temperature for solution heat treatment and one for precipitation heat treatment.

5.3.3 There shall be at least one test location for each 40 ft^3 [1 m³] of load volume, with a minimum of nine test locations, one in each corner and one in the center.

5.3.4 The surveys shall reflect the normal operating characteristics of the furnace. If the furnace is normally charged after being stabilized at the correct operating temperature, the temperature-sensing elements shall be similarly charged. If the furnace is normally charged cold, the temperature-sensing elements shall be charged cold. After insertion of the temperature-sensing elements, readings should be taken frequently enough to determine when the temperature of the hottest region of the furnace approaches the bottom of the temperature range being surveyed. From that time until thermal equilibrium is reached, the temperature of all test locations should be determined at 2-min intervals in order to detect any over-shooting. After thermal equilibrium is reached, readings should be taken at 5-min intervals for sufficient time to determine the recurrent temperature pattern, but for not less than 30 min. Before thermal equilibrium is reached, none of the temperature readings should exceed the maximum temperature of the range being surveyed. After thermal equilibrium is reached, the maximum temperature variation of all elements (both load and furnace thermocouples) shall not exceed 20°F [10°C] and shall not vary outside the range being surveyed.

5.3.5 For furnaces of $10 \text{ ft}^3 [0.25 \text{ m}^3]$ or less the temperature survey may be made with a minimum of three thermocouples located at front, center, and rear or at top, center, and bottom of the furnace.

5.3.6 For furnaces used only for precipitation treatment, after the initial temperature-uniformity survey, as outlined in 5.3.7, surveys need not be made more often than at each 6-month interval provided that (*a*) test specimens from each lot are tested and meet applicable material specifications requirements, (*b*) the furnace is equipped with a multipoint recorder, or (*c*) one or more separate load thermocouples are employed to measure and record actual metal temperatures.

5.3.7 Monthly surveys for batch furnaces are not necessary when the furnace or bath is equipped with a permanent multipoint recording system with at least two sensing thermocouples in each zone or when one or more separate load thermocouples are employed to measure actual metal temperature, providing that uniformity surveys show a history of satisfactory performance for a period of at least 6 months. The sensing thermocouples shall be installed so as to record the temperature of the heated media (air, lead, etc.) or actual metal temperatures. However, periodic surveys shall also be made at 6-month intervals in accordance with the procedures outlined for the monthly survey.

5.4 Continuous Furnace Surveys:

5.4.1 For continuous heat-treating furnaces, the type of survey and the procedures for performing the survey should be established for each particular furnace involved. The types of continuous heat-treating furnaces may vary considerably, depending upon the product and sizes involved. For some types and sizes of furnaces, the only practical way to survey the furnace is to perform an extensive mechanical property survey of the limiting product sizes to verify conformance with the specified mechanical properties for such items. When the type and size of the furnace makes this practical, monthly surveys should be made, using a minimum of two load thermocouples attached to the material. The surveys should reflect the normal operating characteristics of the furnace. The results of these surveys shall indicate that the metal temperature never exceeds the allowable maximum metal temperature specified for solution heat treatment (Tables 1-4 as appropriate) after all load thermocouples have reached the minimum metal temperature specified.

5.4.2 Furnace control temperature-measuring instruments shall not be used to read the temperature of the test temperature sensing elements.

5.5 *Monitoring of Quench*—A monitoring plan shall be developed and utilized for all modes of quenching for all products covered by this practice. The plan should incorporate conductivity or hardness checking, or both, to determine the uniformity of the quench. Areas having substantially higher conductivity or lower hardness than other areas of similar thickness in the lot shall be investigated to ensure that the requirements of the material specification are met.

5.6 Temperature-Measuring System Check—The accuracy of the temperature-measuring system shall be checked under operating conditions weekly. Check should be made by inserting a calibrated test temperature-sensing element adjacent to the furnace temperature-sensing element and reading the test temperature-sensing element with a calibrated test potentiometer. When the furnace is equipped with dual potentiometer measuring systems which are checked daily against each other, the above checks may be conducted every 3 months rather than every week. The test temperature-sensing element, potentiometer, and cold junction compensation combination shall have been calibrated against National Institute of Standards and Technology primary or secondary certified temperaturesensing elements, within the previous 3 months, to an accuracy of $\pm 2^{\circ}$ F [$\pm 1^{\circ}$ C].

5.6.1 If the difference between the two readings in 5.6 exceeds $\pm 10^{\circ}$ F [$\pm 6^{\circ}$ C], the cause of the difference shall be determined and corrected before commencing additional thermal processing. The responsible quality organization shall be notified and appropriate corrective action shall be taken and documented including an evaluation of the possible effects of the deviation on castings processed since the last successful test.

Alloy ^A	Final Temper ^A	Metal Temperature, $\pm 10^{\circ} F$	Time at Temperature, h	Metal Temperature, $\pm 10^{\circ} F$	Time at Temperature, h
201.0	Т6	960	2 ^E	room temperature	12 to 24
		then 980	14 to 20	then 310	20
	T7	960	2 ^E	room temperature	12 to 24
		then 980	14 to 20	then 370	5
A201.0	Τ7	955	2 ^E	room temperature	12 to 24
		then 985	14 to 20	then 370	5
203.0	Т6	955	2 ^E	room temperature	12 to 24
		then 1010	5	then 425	16
204.0	T4	970	10	room temperature	5 days ^F
A206.0	T4	950	2 ^E	room temperature	5 days
		then 985	14 to 20	·	
	T43	950	2 ^E	room temperature	12 to 24
		then 985	14 to 20	then 320	0.5 to 1
	T6 ^G	950	2 ^E	room temperature	12 to 24
		then 985	14 to 20	then 310	20
	Τ7	950	2 ^E	room temperature	12 to 24
		then 985	14 to 20	then 370	4 to 5
222.0	0 ^{<i>D</i>,<i>H</i>}			600 ^{<i>H</i>}	3
	T61	945	6 to 12	310	11
242.0	0 ^{<i>D</i>,<i>H</i>}			650 ^H	3
	T571			400	8
	T61	960	2 to 6'	450	1 to 3
A242.0	T75	965	6 to 10	550	2 to 5
295.0	T4	960	6 to 12		
	T6	960	6 to 12	310	3 to 6
	T62	960	6 to 12	310	12 to 24
	Τ7	960	6 to 12	500	4 to 6

TABLE 1 Recommended Heat Treatment for Sand and Investment Type Alloys (Inch-Pound Units)

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TABLE 1	Continued
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		Solution He	eat Treatment ^{B,C}	Precipitation He	Precipitation Heat Treatment ^D		
Alloy ^A	Final Temper ^A	Metal Temperature, $\pm 10^{\circ}F$	Time at Temperature, h	Metal Temperature, ±10°F	Time at Temperature, h		
296.0	T4	950	4 to 8				
	Т6	950	4 to 8	310	2 to 8		
	Τ7	950	4 to 8	500	4 to 6		
319.0	Τ4	940	6 to 10				
	T5			400	8		
	Т6	940	6 to 12	310	2 to 5		
328.0	Т6	960	12	310	2 to 5		
355.0	T51			440	7 to 9		
	T6	980	6 to 12	310	3 to 5		
	T7	980	6 to 12	440	3 to 5		
	T71	980	6 to 12	475	4 to 6		
C355.0 ^J	Т6	985	6 to 12	room temperature	8		
0000.0	16	300	01012	then 310	3 to 5		
356.0	T51			440	7 to 9		
000.0	T6	 1000	 6 to 12	310	3 to 5		
	T7	1000	6 to 12	400	3 to 5		
	T71	1000	6 to 12	400	2 to 4		
A356.0	T6	1000	6 to 12		2 to 5		
A350.0	T61	1000		310 330	6 to 12		
			6 to 12				
	T7	1000	6 to 12	440	8		
	T71	1000	6 to 12	475	3 to 6		
357.0	T6	1000 ^H	8	330	6 to 12		
/	T61	1000	10 to 12	310	10 to 12		
A357.0 ^J	T61	1000 ^{<i>H</i>}	8 to 10	room temperature then 310	8 8		
520.0	T4	810	12 to 18 ^{<i>K</i>}				
705.0	T1			room temperature	21 days		
	T5			210	8		
707.0	T1			room temperature	21 days		
	T7	990	8 to 16	350	4 to 10		
710.0	T5			_ room temperature	21 days		
		ntins://si	randards.	or 315	6 to 8		
712.0	Т5			room temperature	21 days		
712.0	10			• or 315	6 to 8		
713.0	T1			room temperature	21 days		
710.0	T5			250	16		
771.0	T5			355	3 to 5		
771.0	T51			405	6		
	T52						
	152 T6	<u>AST</u>	<u>M B. 7/B917M-01</u>	330 ⁷	6 to 16 ^L		
		1090		265 57360 ^{3,D} 1d29b19444/as	$\frac{3}{17}$		
	rds.itehT53catalog T71	g/standards/sist/b21 1090	$c_{1340-c_{190}}^{c_{1340-c_{190}}^{c_{190}}}$	285	tm-4917-b917m-01 15		
850.0	T5			430	7 to 9		
851.0	T5			430	7 to 9		
852.0	T5			430	7 to 9		
052.0	10			430	1 10 9		

^A Designations conform to ANSI H35.1 and to Practice B 275.

^B Quench in water at 150 to 212°F except as noted.

^c Time at solution temperature may be increased for section thickness over 1 in.

^D No quenching required. Cool in still air outside the furnace.

^E Cooling not required prior to second step.

F In order to expedite testing, alloy 204.0 test specimens may be precipitation heat treated after quenching by holding at 255°F for 2 h.

^G This alloy is stress corrosion crack prone when in the T6 temper and should not be used in the T6 temper for applications that see, even mildly corrosive environments. ^H Solution treatment temperature of 1010°F may be used (to obtain higher solubility) provided no portion of the heat treat oven exceeds 1020°F.

¹Quenching is accomplished by air blast.

^J Stress relieve for dimensional stability in the following manner: (1) Hold at 775 ± 25°F for 5 h. Then (2) Furnace cool to 650°F for 2 or more h. Then (3) Furnace cool to 450°F for not more than $\frac{3}{4}$ h. Then (4) Furnace cool to 250°F for approximately 2 h. Then (5) Cool to room temperature in still air outside the furnace.

^K Quench in water at 150 to 212°F for a controlled time of 10 to 20 s, then cool in still air outside the furnace.

^L Time required depends on variations in cooling rate between 650° and 450°F during stress-relief procedure (Footnote J).

TABLE 2 Recommended Heat Treatment for Sand and Investment Type Aluminum	Alloys	[SI Units]	
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	Final Temper ^A	Solution Heat Treatment ^{B,C}		Precipitation Heat Treatment ^D	
Alloy ^A		Metal Temperature, $\pm 5^{\circ}\mathrm{C}$	Time at Temperature, h	Metal Temperature, $\pm 5^{\circ}\mathrm{C}$	Time at Temperature, h
201.0	Т6	515	2 ^E	room temperature	12 to 24
		then 525	14 to 20	then 155	20
	Τ7	515	2 ^E	room temperature	12 to 24
		then 525	14 to 20	then 190	5
A201.0	Τ7	515	2 ^E	room temperature	12 to 24
		then 530	14 to 20	then 190	5

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TABLE	2	Continued
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		Solution Heat	Treatment ^{B,C}	Precipitation Heat Treatment ^D		
Alloy ^A	Final Temper ^A	Metal Temperature, ±5°C	Time at Temperature, h	Metal Temperature, ±5°C	Time at Temperature, h	
203.0	T6	515 then 545	2 ^E 5	room temperature then 220	12 to 24 16	
204.0	Τ4	520	10	room temperature	5 days ^F	
A206.0	T4	510	2 ^E	-		
A200.0	14			room temperature	5 days	
		then 530	14 to 20			
	T43	510	2 ^E	room temperature	12 to 24	
		then 530	14 to 20	then 160	0.5 to 1	
	T6 ^{<i>G</i>}	510	2 ^E	room temperature	12 to 24	
		then 530	14 to 20	then 155	20	
	T7	510	2 ^E	room temperature	12 to 24	
	.,	then 530	14 to 20	then 190	4 to 5	
222.0	$O^{D,H}$			315 ^{<i>H</i>}	3	
222.0						
	T61	510	6 to 12	155	11	
242.0	0 ^{<i>D</i>,<i>H</i>}			345 ^{<i>H</i>}	3	
	T571			205	8	
	T61	515	2 to 6'	230	1 to 3	
A242.0	T75	520	6 to 10	290	2 to 5	
295.0	T4	515	6 to 12			
	T6	515	6 to 12	155	3 to 6	
	T62	515	6 to 12	155		
					12 to 24	
	T7	515	6 to 12	260	4 to 6	
296.0	T4	510	4 to 8			
	Т6	510	4 to 8	155	2 to 8	
	Τ7	510	4 to 8	260	4 to 6	
319.0	T4	505	6 to 10			
010.0	T5			205	8	
			 6 to 10			
	T6	505	6 to 12	155	2 to 5	
328.0	Т6	515	12 m o 9 m o	155	2 to 5	
355.0	T51		<u>anuaru</u>	225	7 to 9	
	Т6	525	6 to 12	155	3 to 5	
	T7	525	6 to 12	225	3 to 5	
	T71	525	6 to 12	245	4 to 6	
C355.0 ^J	Т6	530	6 to 12	room temperature	8	
000010			0.10.12	then 155	3 to 5	
356.0	TE1			225	7 to 9	
550.0	T51			155		
	T6	540	6 to 12		3 to 5	
	T7	540	6 to 12	205	3 to 5	
	T71	540	6 to 12	245	2 to 4	
A356.0	Т6	540 ASTMI	R0 16 to 12 1 7 V _ 0 1	155	2 to 5	
	T61	540	6 to 12	165	6 to 12	
	s.iteh.ai/Tatalog/s	tan 540 ds/sist/b2 fcf34	- 6 to 12-40ab-915	7-225 d29b19444/astm	-b 8 17-b917m-	
	T71	540	6 to 12	245	3 to 6	
357.0	Т6	540 ^{<i>H</i>}	8	165	6 to 12	
007.0						
	T61	540	10 to 12	155	10 to 12	
A357.0 ⁷	T61	540 ^{<i>H</i>}	8 to 10	room temperature	8	
				then 155	8	
520.0	T4	430	12 to 18 ^{<i>K</i>}			
705.0	T1			room temperature	21 days	
	T5			100	8	
707.0	T1			room temperature	21 days	
	T7	530	 8 to 16	175	4 to 10	
710.0						
710.0	T5			room temperature	21 days	
	_			or 155	6 to 8	
712.0	T5			room temperature	21 days	
				or 155	6 to 8	
713.0	T1			room temperature	21 days	
	T5			120	16	
771.0	T5			180	3 to 5	
771.0						
	T51			205	6	
	T52			165 ⁷	6 to 16 ^L	
	Т6	590	6 ^D	130	3	
	T53			180 ^{<i>J</i>,<i>D</i>}	4	
	T71	590	6 ^D	140	15	
850.0	T5			220	7 to 9	
851.0						
0.100	T5			220	7 to 9	
852.0	T5			220	7 to 9	

^A Designations conform to ANSI H35.1 and to Practice B 275. ^B Quench in water at 65 to 100°C except as noted.

^C Time at solution temperature may be increased for section thickness over 25 mm.

^D No quenching required. Cool in still air outside the furnace. ^E Cooling not required prior to second step.

F In order to expedite testing, alloy 204.0 test specimens may be precipitation heat treated after quenching by holding at 125°C for 2 h.

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^G This alloy is stress corrosion crack prone when in the T6 temper and should not be used in the T6 temper for applications that see, even mildly corrosive environments.

^H Solution treatment temperature of 545°C may be used (to obtain higher solubility) provided no portion of the heat treat oven exceeds 550°C.

¹Quenching is accomplished by air blast.

^{*J*} Stress relieve for dimensional stability in the following manner: (1) Hold at 415 \pm 15°C for 5 h. Then (2) Furnace cool to 345°C for 2 or more h. Then (3) Furnace cool to 230°C for not more than $\frac{3}{4}$ h. Then (4) Furnace cool to 120°C for approximately 2 h. Then (5) Cool to room temperature in still air outside the furnace.

 $^{\kappa}$ Quench in water at 65 to 100°C for a controlled time of 10 to 20 s, then cool in still air outside the furnace.

^L Time required depends on variations in cooling rate between 345° and 230°C during stress-relief procedure (Footnote ^J).

TABLE 3 Recommended Heat Treatment for Permanent Mold Type Alloys (Inch-Pound Units)

		Solution Heat Treatment ^{B,C}		Precipitation Heat Treatment ^D	
Alloy ^A	Final Temper ⁴	Metal Temperature, $\pm 10^{\circ} F$	Time at Temperature, h	Metal Temperature, $\pm 10^{\circ} F$	Time at Temperature, h
201.0	Τ6	960 then 980	2 14 to 20	room temperature then 310	12 to 24 20
	Τ7	960 then 980	2 14 to 20	room temperature then 370	12 to 24
A201.0	Τ7	955	2	room temperature	5 12 to 24
203.0	Т6	then 985 955	14 to 20 2	then 370 room temperature	5 12 to 24
204.0	T4	then 1010 970	5 10	then 425 room temperature	16 5 days ^{<i>E</i>}
A206.0	T4	950	2	room temperature	5 days
	T43	then 985 950	14 to 20 2	room tomporaturo	12 to 24
	143	then 985	2 14 to 20	room temperature then 320	0.5 to 1
	T6 ^F	950	2	room temperature	12 to 24
	10	then 985	14 to 20	then 310	20
	T7	950	2	room temperature	12 to 24
		then 985	 14 to 20	then 370	5
208.0	T6	940	4 to 12	310	2 to 5
222.0	T551	- Hen S	tangaros	340	16 to 22
	T65	950	4 to 12	340	7 to 9
242.0	T571	· · ··· · · / / · · · · ·	T 1.4	340	22 to 26
	T	TINS://STAI	10.21°0.S.IT	or 400	7 to 9
000.0	T61	960	4 to 12	400	3 to 5
296.0	T6 T4	950	8	310	1 to 8
319.0	T6	940 CUM e	4 to 10 revie	310	 2 to 5
332.0	T5			400	7 to 9
336.0	T551			400	7 to 9
550.0	T65	960	 1.5 ⁸ D0171 (01	400	7 to 9
333.0	T5	ASTM B	9177B917M-01	400	7 to 9
	TE		6 to 1210ab 0157	7131020b10////actm	
	$\frac{1}{17}$ $\frac{1}{10}$ $\frac{1}{10}$ $\frac{1}{10}$ $\frac{1}{10}$ $\frac{1}{10}$	and 940 SISU 02101540	6 to 12	/150029019444/astm	$-b^{2}$ to 5 $-b^{9}17$ m-0
354.0	T61	980	10 to 12	room temperature	8
				then 310	10 to 12
	T62	980	10 to 12	room temperature	8
				then 340	6 to 10
355.0	T51			440	7 to 9
	T6	980	4 to 12	310	2 to 5
	T62	980	4 to 12	340	14 to 18
	T7	980	4 to 12	440	7 to 9
C355.0 ^G	T71	980	4 to 12	475	3 to 6 8
0355.0-	T61	980	6 to 12	room temperature	o 10 to 12
356.0	T51			then 310 440	7 to 9
000.0	T6	 1000	 4 to 12	310	2 to 5
	T71	1000	4 to 12	440	7 to 9
A356.0 ^G	T6	1000	4 to 12	310	2 to 5
	T61	1000	4 to 12	room temperature	8
				then 310	6 to 12
	Τ7	1000	4 to 12	440	8
	T71	1000	4 to 12	475	3 to 6
357.0	Т6	1000 ^{<i>H</i>}	8	330	6 to 12
A357.0 ^G	T61	1000 ^{<i>H</i>}	10	room temperature	8
	_			then 310	8
359.0 ^G	T61	1000	10 to 14	room temperature	8
		1000		then 310	10 to 12
	T62	1000	10 to 14	room temperature	8
	- <i>i</i>	1000	0 1 10	then 340	6 to 10
A444.0	T4	1000	8 to 12		 01. dovo
705.0	T1			room temperature	21 days
707.0	T5 T1			210	10 21 days
101.0					
707.0	T1 T7	 990	 8 to 16	room temperature 350	21 days 4 to 10