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Hydraulic fluid power — Sealing devices — Standard test methods to assess the performance of seals used in oil hydraulic reciprocating applications

*Transmissions hydrauliques — Dispositifs d'étanchéité — Méthodes d'essai
normalisées d'évaluation des performances des joints utilisés dans des
applications alternatives à l'huile hydraulique*
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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

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International Standard ISO 7986 was prepared by Technical Committee ISO/TC 131, *Fluid power systems*, Subcommittee SC 7, *Sealing devices*. Annexes A, B and C form an integral part of this International Standard. Annex D is for information only.

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Introduction

0.1 General

It is widely recognized that the results from reciprocating seal testing can be unpredictable. The background research carried out in support of the preparation of this International Standard has demonstrated that this unpredictability is primarily a function of lack of control of critical variables affecting seal installation and operation. In order to carry out direct comparisons of seal performance, it is necessary to control these variables to closer limits than may be normal in industrial practice. The major variables that can affect seal performance, often even within normal manufacturing tolerance ranges, are listed in subclause 0.3.

0.2 Purpose of the test

The purpose of the test is to provide comparative data on individual reciprocating shaft seal designs and to provide a basis for the preliminary selection of seals based on their relative performance. To achieve this, it is necessary to carry out the tests under strictly defined operating conditions. This International Standard therefore defines standard values of speed, pressure, temperature and surface finish. This will permit comparison of seal test results from sources worldwide. <https://www.iso.org/standards/catalog/standards/sist/3512d544-89fa-430a-8a86-dfec48e8007/iso-7986-1997>

To make the test results as useful as possible, a range of operating conditions has been provided, so that the most appropriate conditions can be selected as a basis for comparison for initial seal selection.

The pressures are standard working pressures, selected from ISO 2944:1974, 6,3 MPa (63 bar¹⁾), 16 MPa (160 bar), and 31,5 MPa (315 bar).

The speeds have been selected to include slow speed (where stick-slip and high wear may be problems), medium speed for general purpose hydraulics and a representative high speed.

The constraints on installation and operation in this procedure have been proved by research (primarily carried out at BHR Group in the United Kingdom, under sponsorship from European companies) and international round robin seal tests to be necessary to achieve repeatable results. Any departure from the standard operating conditions and installation criteria cannot be considered a standard test.

1) 1 bar = 0,1 MPa = 10⁵ Pa.

0.3 Factors affecting seal performance

Factors affecting seal performance include:

- a) installation;
- sealing system, i.e., design of bearing(s), seal(s) and wiper seal;
 - installation tolerances, including seal groove, shaft and bearings, extrusion gap;
 - shaft material and hardness;
 - surface finish of the shaft; variations of surface finish outside the range of Ra 0,08 μm to Ra 0,015 μm , or greater than Rt 1,5 μm , can significantly affect seal performance. Different seal materials also have significantly varying requirements for the optimum surface finish;
 - surface finish of the groove surfaces. This must be less than Ra 0,8 μm to avoid static leakage and wear of the seal during pressure cycles;
 - bearing material, including its effects on shaft texture and boundary layer.
- b) operation;
- fluid, i.e., viscosity, lubricity, compatibility with seal material, including additives and contamination level;
 - pressure, including pressure cycle;
 - speed, especially speed cycle;
 - speed/pressure cycle, i.e., stop-start conditions;
 - stroke, especially short strokes (two times the seal contact widths or less), which prevent formation of a lubricant film;
 - temperature, i.e., its effect on viscosity and seal material properties;
 - external environment.

It is necessary to consider all the above factors and their potential effect on seal performance when comparing potential seal performance in an actual application to results obtained from the standard test.

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Hydraulic fluid power — Sealing devices — Standard test methods to assess the performance of seals used in oil hydraulic reciprocating applications

1 Scope

This International Standard defines the test conditions and methods for assessing the performance of seals used in oil hydraulic reciprocating applications.

The resulting specified characteristics may be published in manufacturer's literature to enable a direct comparison of seal performance.

The seal under test may be a single seal or a combination seal package.

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2 Normative references

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The following standards contain provisions which, through reference in this text, constitute provisions of this International Standard. At the time of publication, the editions indicated were valid. All standards are subject to revision, and parties to agreements based on this International Standard are encouraged to investigate the possibility of applying the most recent editions of the standards indicated below. Members of IEC and ISO maintain registers of currently valid International Standards.

ISO 286-2:1988, *ISO system of limits and fits — Part 2: Tables of standard tolerance grades and limit deviations for holes and shafts.*

ISO 1052:1982, *Steels for general engineering purposes.*

ISO 1629:1995, *Rubber and latices — Nomenclature.*

ISO 2944:1974, *Fluid power systems and components — Nominal pressures.*

ISO 3274:1996, *Geometrical Product Specification (GPS) — Surface texture: Profile method — Nominal characteristics of contact (stylus) instruments.*

ISO 4288:1996, *Geometrical Product Specification (GPS) — Surface texture: Profile method — Rules and procedures for the assessment of surface texture.*

ISO 6743-4:1982, *Lubricants, industrial oils and related products (class L) — Classification — Part 4: Family H (Hydraulic systems).*

ISO 10766:1996, *Hydraulic fluid power — Cylinders — Housing dimensions for rectangular-section-cut bearing rings for pistons and rods.*

3 Symbols

See table 1.

Table 1 — Symbols, quantities and units

Symbol	Quantity	Unit
d	Seal lip inside diameter	mm
D	Nominal seal housing diameter	mm
E	Seal length	mm
F	Friction force	N
d_h	Seal heel inside diameter	mm
l	Leakage	ml
L	Seal housing length	mm
p_{test}	Test pressure (forward stroke)	MPa
p_{return}	Return pressure (return stroke)	MPa
S_l	Radial seal section – lip	mm
S_h	Radial seal section – heel	mm
v	Test speed	m/s
W	Leakage collection zone	mm
R_a	Shaft surface texture, arithmetical mean deviation	μm
R_t	Shaft surface texture, total height of the surface profile	μm

4 Test installation

4.1 General

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4.1.1 The tests described in this specification shall be conducted using a suitable test rig possessing the features shown in figure 1 and detail assembly as shown in figure 2.

4.1.2 The bearing housing shall be designed and constructed as detailed in figure 3 and figure 4 and shall be made of steel. Bearing material shall be polyester fabric/polyester material and shall contain no glass, ceramic, metallic or other potentially abrasive filler. The bearing shall comply with ISO 10766.

4.1.3 A circuit comprising components capable of cycling the pressure and controlling the flow to the specifications given in table 2 shall be provided to circulate the test fluid through the test seal housing.

Table 2 — Circuit specification

Characteristic	Specification
Fluid flow	4 l/min to 10 l/min
Filtration	10 μm absolute (through which fluid is continuously circulated)
Fluid reservoir	20 l to 50 l
Filter change	after every 1 000 h test running
Test oil change	after every 3 000 h test running

New test oil shall be circulated through a new filter for 5 h prior to beginning a test with new oil.

4.2 Mechanical details

4.2.1 Test rig rod

A test rod complying with table 3 shall be used.

Table 3 — Test rod specification

Parameter	Specification
Diameter	36 mm, tolerance f8 (per ISO 286-2)
Material	Shaft material in accordance with ISO 1052, induction hardened before coating with hard chrome with a coating thickness of 0,015 mm to 0,03 mm
Surface texture	Ground and polished to Ra 0,08 to Ra 0,15 μm when measured in accordance with 9.1.1

4.2.2 Test rig stroke

The length of stroke shall be limited to 500 mm \pm 20 mm.

4.2.3 Test seal housing dimensions

Housings for the test seals shall comply with the dimensions specified in figure 2.

4.2.4 Leakage collection and drain

4.2.4.1 Rod seal (see figures 1 and 2): At the atmospheric extremity of each seal beyond which a wiper seal is installed, a leakage zone, W , of 20 mm \pm 5 mm shall be provided. Provision shall be made for the collection from within this zone of any leakage that has drained away, for subsequent measurement (see 4.2.4.2). The wiper seals shall be made of nitrile (NBR) rubber (see ISO 1629) with a hardness of 70 IRHD to 75 IRHD and shall conform with the dimensions given in figure 7. New wiper seals shall be installed for each test.

4.2.4.2 Drain: Leakage drains having a minimum bore of 6 mm shall be provided.

5 Test parameters

5.1 Test fluid

Test fluid shall be synthetic hydrocarbon hydraulic oil, poly-alpha-olefin ISO-L-HS 32 in accordance with ISO 6743-4. [An example of an oil that conforms to this specification is Mobil SHC 524 2).]

5.2 Test fluid temperature

The temperature of the test fluid throughout the tests shall be maintained at 60 °C to 65 °C when measured in the centre of the pressure chamber. The test fluid temperature shall be measured with a suitable thermocouple at the position specified in figure 2.

5.3 Test housing rod bearings

Rod bearings as specified in 4.1.2 shall be used in housings that comply with figure 3 and ISO 10766.

2) This information is given for the convenience of users of this International Standard and does not constitute an endorsement by ISO of the product named. Equivalent products may be used if they can be shown to lead to the same results.

5.4 Test fluid pressure

The appropriate test pressure, p_{test} , shall be selected from the following list, as appropriate to the intended application, in each case with a tolerance of $\pm 2\%$:

- 6,3 MPa (63 bar);
- 16 MPa (160 bar);
- 31,5 MPa (315 bar).

5.5 Speed of linear actuator

The speed of the reciprocating rod shall be limited to one of the specified linear speeds below, in each case with a tolerance of $\pm 5\%$:

- 0,05 m/s;
- 0,15 m/s;
- 0,5 m/s.

5.6 Pressure and stroke cycle for dynamic test

The test pressures and strokes shall be cycled as follows:

- a) a forward stroke at constant pressure, p_{test} ;
- b) a return stroke at constant pressure, p_{return} .

The pressure cycle shall be maintained within the specification given in figure 5 and stroke cycle within the specification given in figure 6.

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6 Assembly and dismantling of seals

All test seals shall be installed in their housings in the manner prescribed by the seal manufacturer. Lightly wipe test oil onto the test shaft and seal before assembly. After assembly, wipe excess oil from the test shaft to avoid erroneous leakage measurements and excess lubrication.

7 Methods of measurement and measuring apparatus

7.1 Seal leakage

Measuring cylinders of a maximum capacity of 10 ml and an accuracy of 0,1 ml shall be used at the start of each test. If leakage exceeds 10 ml during the test, then larger measuring cylinders with an accuracy of 1 ml shall be used.

7.2 Seal friction

7.2.1 Load cell

The load cell shall be installed on the test rig between the linear actuator and rod and shall be capable of measuring the tensile and compressive forces induced by the friction of the seal. The load cell shall be connected to a suitable conditioning apparatus and chart recorder so that a permanent record of the seal friction may be taken. A chart recorder that has a suitable frequency response and is capable of determining the amplitude of the stick/slip forces shall be used.

7.2.2 Determination of dynamic seal friction

7.2.2.1 The inherent total friction of the sliding bearing surfaces and of any leakage collection wipers, F_i , shall be determined at the beginning of each test programme (see 4.1 and 4.2.4.1).

7.2.2.2 The mean frictional forces (in newtons) of the test seals from the chart recorder trace (see figure 8 and figure 9) shall be subsequently determined by the following formula:

$$F_S = \frac{F_T - F_i}{4}$$

where

F_S is the mean mid-stroke value of forward stroke and return stroke friction forces of each seal under test, in newtons;

F_i is the inherent total friction at mid-stroke of the test rig only (see 7.2.2.1), in newtons;

F_T is the sum of the friction at mid-stroke of the test rig for two test seals on the forward and return strokes, in newtons.

NOTE — Because F_S is a mean value, it cannot be taken as an absolute indication of actual friction for one seal for a given stroke.

7.2.3 Procedure for determining breakout friction

7.2.3.1 Set test circuit to pressure for the required static test period, e.g. 16 h.

7.2.3.2 On completion of the static test period, set drive circuit to zero pressure.

7.2.3.3 Set drive pump to test speed.

7.2.3.4 Set direction to give rod travel with rod extending at seal A.

7.2.3.5 Start chart recorder (see 7.2.1).

7.2.3.6 Gradually adjust drive circuit pressure to give shaft motion.

7.2.3.7 Record friction at the instant of shaft movement on test data sheet (see figure 9).

7.2.3.8 Increase drive circuit pressure to overcome any increase in the running friction and continue dynamic test.

7.3 Pressure measurement

7.3.1 Pressure gauge

A pressure gauge with a suitable pressure range shall be used and shall be installed to ensure that the gauge is reliable in a cyclic pressure condition.

7.3.2 Pressure transducer

A suitable pressure transducer shall be installed in the seal housing as specified in figure 2 to provide a record of the test pressure cycle. The pressure transducer shall have temperature compensation to provide accurate measurement to $\pm 0,5\%$ at 65 °C.

7.4 Surface roughness

A surface roughness measuring instrument that complies with ISO 3274 and includes an electric wave filter shall be used.