



Standard Practice of Calibration of Force-Measuring Instruments for Verifying the Force Indication of Testing Machines¹

This standard is issued under the fixed designation E 74; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reappraisal. A superscript epsilon (ε) indicates an editorial change since the last revision or reappraisal.

This standard has been approved for use by agencies of the Department of Defense.

1. Scope

1.1 The purpose of this practice is to specify procedures for the calibration of force-measuring instruments. Procedures are included for the following types of instruments:

- 1.1.1 Elastic force-measuring instruments, and
- 1.1.2 Force-multiplying systems, such as balances and small platform scales.

NOTE 1—Verification by deadweight loading is also an acceptable method of verifying the force indication of a testing machine. Tolerances for weights for this purpose are given in Practices E 4; methods for calibration of the weights are given in NIST Technical Note 577, Methods of Calibrating Weights for Piston Gages.²

1.2 The values stated in SI units are to be regarded as the standard. Other metric and inch-pound values are regarded as equivalent when required.

1.3 This practice is intended for the calibration of static force measuring instruments. It is not applicable for dynamic or high speed force calibrations, nor can the results of calibrations performed in accordance with this practice be assumed valid for dynamic or high speed force measurements.

1.4 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

2. Referenced Documents

2.1 ASTM Standards:

- E 4 Practices for Force Verification of Testing Machines³
- E 29 Practice for Using Significant Digits in Test Data to

Determine Conformance with Specifications⁴

2.2 *American National Standard:*

B46.1 Surface Texture⁵

ELASTIC FORCE-MEASURING INSTRUMENTS

3. Terminology

3.1 Definitions:

3.1.1 *elastic force-measuring device*—a device or system consisting of an elastic member combined with a device for indicating the magnitude (or a quantity proportional to the magnitude) of deformation of the member under an applied force.

3.1.2 *primary force standard*—a deadweight force applied directly without intervening mechanisms such as levers, hydraulic multipliers, or the like, whose mass has been determined by comparison with reference standards traceable to national standards of mass.

3.1.3 *secondary force standard*—an instrument or mechanism, the calibration of which has been established by comparison with primary force standards.

3.2 Definitions of Terms Specific to This Standard:

3.2.1 *calibration equation*—a mathematical relationship between deflection and force established from the calibration data for use with the instrument in service, sometimes called the calibration curve.

3.2.2 *continuous-reading device*—a class of instruments whose characteristics permit interpolation of forces between calibrated forces.

3.2.2.1 *Discussion*—Such instruments usually have force-to-deflection relationships that can be fitted to polynomial equations. Departures from the fitted curve are reflected in the uncertainty (8.4).

3.2.3 *deflection*—the difference between the reading of an instrument under applied force and the reading with no applied force.

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² Available from National Institute for Standards and Technology, Gaithersburg, MD 20899.

³ *Annual Book of ASTM Standards*, Vol 03.01.

⁴ *Annual Book of ASTM Standards*, Vol 14.02.

⁵ Available from American National Standards Institute, 11 W. 42nd St., 13th Floor, New York, NY 10036.

3.2.4 *loading range*—a range of forces within which the uncertainty is less than the limits of error specified for the instrument application.

3.2.5 *reading*—a numerical value indicated on the scale, dial, or digital display of a force-measuring instrument under a given force.

3.2.6 *resolution*—the smallest reading or indication appropriate to the scale, dial, or display of the force measuring instrument.

3.2.7 *specific force device*—an alternative class of instruments not amenable to the use of a calibration equation.

3.2.7.1 *Discussion*—Such instruments, usually those in which the reading is taken from a dial indicator, are used only at the calibrated forces. These instruments are also called limited-load devices.

3.2.8 *uncertainty*—a statistical estimate of the limits of error in forces computed from the calibration equation of a force-measuring instrument when the instrument is calibrated in accordance with this practice.

4. Significance and Use

4.1 Testing machines that apply and indicate force are in general use in many industries. Practices E 4 has been written to provide a practice for the force verification of these machines. A necessary element in Practices E 4 is the use of devices whose force characteristics are known to be traceable to national standards. Practice E 74 describes how these devices are to be calibrated. The procedures are useful to users of testing machines, manufacturers and providers of force measuring instruments, calibration laboratories that provide the calibration of the instruments and the documents of traceability, and service organizations that use the devices to verify testing machines.

5. Reference Standards

5.1 Force-measuring instruments used for the verification of the force indication systems of testing machines may be calibrated by either primary or secondary standards.

5.2 Force-measuring instruments used as secondary standards for the calibration of other force-measuring instruments shall be calibrated by primary standards. An exception to this rule is made for instruments having capacities exceeding the range of available primary standards. Currently the maximum primary force-standard facility in the United States is 1 000 000-lbf (4.4-MN) deadweight calibration machine at the National Institute of Standards and Technology.

6. Requirements for Force Standards

6.1 *Primary Standards*—Weights used as primary force standards shall be made of rolled, forged, or cast metal. Adjustment cavities shall be closed by threaded plugs or suitable seals. External surfaces of weights shall have a finish of 125 or less as specified in ANSI B46.1.

6.1.1 The force exerted by a weight in air is calculated as follows:

$$\text{Force} = \frac{Mg}{9.80665} \left(1 - \frac{d}{D} \right) \quad (1)$$

where:

- M = mass of the weight,
- g = local acceleration due to gravity, m/s^2 ,
- d = air density (approximately 0.0012 Mg/m^3),
- D = density of the weight in the same units as d (Note 4), and
- 9.80665 = the factor converting SI units of force into the customary units of force. For SI units, this factor is not used.

6.1.2 The masses of the weights shall be determined within 0.005 % of their values by comparison with reference standards traceable to the national standards of mass. The local value of the acceleration due to gravity, calculated within 0.0001 m/s^2 (10 milligals), may be obtained from the National Geodetic Information Center, National Oceanic and Atmospheric Administration.⁶

NOTE 2—If M , the mass of the weight, is in pounds, the force will be in pound-force units (lbf). If M is in kilograms, the force will be in kilogram-force units (kgf). These customary force units are related to the newton (N), the SI unit of force, by the following relationships:

$$1 \text{ lbf} = 4.448 22 \text{ N} \quad (2)$$

$$1 \text{ kgf} = 9.806 65 \text{ N (exact)}$$

The pound-force (lbf) is defined as that force which, applied to a 1-lb mass, would produce an acceleration of 9.80665 m/s^2 .

The kilogram-force (kgf) is defined as that force which, applied to a 1-kg mass, would produce an acceleration of 9.80665 m/s^2 .

6.2 *Secondary Standards*—Secondary force standards may be either elastic force-measuring instruments used in conjunction with a machine or mechanism for applying force, or some form of mechanical or hydraulic mechanism to multiply a relatively small deadweight force. Examples of the latter form include single- and multiple-lever systems or systems in which a force acting on a small piston transmits hydraulic pressure to a larger piston.

6.2.1 Elastic force-measuring instruments used as secondary standards shall be calibrated by primary standards and used only over the Class AA loading range (see 8.5.2.1). Secondary standards having capacities exceeding 1 000 000 lbf (4.4 MN) are not required to be calibrated by primary standards. Several secondary standards of equal compliance may be combined and loaded in parallel to meet special needs for higher capacities. The uncertainty (see 8.4) of such a combination shall be calculated by adding in quadrature using the following equation:

$$U_c = \sqrt{U_o^2 + U_1^2 + U_2^2 + \dots + U_n^2} \quad (3)$$

where:

- U_c = uncertainty of the combination, and
- $U_{o, 1, 2, \dots, n}$ = uncertainty of the individual instruments.

6.2.2 The multiplying ratio of a force multiplying system used as a secondary standard shall be measured at not less than three points over its range with an accuracy of 0.05 % of ratio or better. Some systems may show a systematic change in ratio with increasing force. In such cases the ratio at intermediate

⁶ Available from the National Oceanic and Atmospheric Administration, Rockville, MD.

points may be obtained by linear interpolation between measured values. Deadweights used with multiplying-type secondary standards shall meet the requirements of 6.1 and 6.1.2. The force exerted on the system shall be calculated from the relationships given in 6.1.1. The force multiplying system shall be checked annually by elastic force measuring instruments used within their class AA loading ranges to ascertain whether the forces applied by the system are within acceptable ranges as defined by this standard. Changes exceeding 0.05 % of applied force shall be cause for reverification of the force multiplying system.

7. Calibration

7.1 Basic Principles—The relationship between the applied force and the deflection of an elastic force-measuring instrument is, in general, not linear. As force is applied, the shape of the elastic element changes, progressively altering its resistance to deformation. The result is that the slope of the force-deflection curve changes gradually and uniformly over the entire range of the instrument. This characteristic full-scale nonlinearity is a stable property of the instrument that is changed only by a severe overload or other similar cause.

7.1.1 Localized Nonlinearities—Superposed on this curve are localized nonlinearities introduced by the imperfections in the force indicating system of the instrument. Examples of imperfections include: non-uniform scale or dial graduations, irregular wear between the contacting surfaces of the vibrating reed and button in a proving ring, and voltage and sensing instabilities in a load cell system. Some of these imperfections are less stable than the full-scale nonlinearity and may change significantly from one calibration to another.

7.1.2 Curve Fitting—In the treatment of the calibration data, a second degree polynomial fitted to the observed data using the method of least squares has been found to predict within the limit of the uncertainty (8.4) deflection values for applied force throughout the loading range of the elastic force measuring instrument. Such an equation compensates effectively for the full-scale nonlinearity, allowing the localized nonlinearities to appear as deviations. A statistical estimate, called the uncertainty, is made of the width of the band of these deviations about the basic curve. The uncertainty is, therefore, an estimate of the limits of error contributed by the instrument when forces measured in service are calculated by means of the calibration equation. Actual errors in service are likely to be greater if forces are applied under loading and environmental conditions differing from those of the calibration.

7.1.3 Curve Fitting for High Resolution Devices—The use of calibration equations of the 3rd, 4th, or 5th degree is restricted to devices having a resolution of 1 increment of count per 50000 or greater active counts at the maximum calibration load. Annex A1 recommends a procedure for obtaining the degree of the best fit calibration curve for these devices.

NOTE 3—Experimental work by several force calibration laboratories in fitting higher than second degree polynomials to the observed data indicates that, for some devices, use of a higher degree equation may result in a lower uncertainty than that derived from the second degree fit. (ASTM RR: E28-1009) Overfitting should be avoided. Equations of greater than 5th degree cannot be justified due to the limited number of

force increments in the calibration protocol. Errors caused by round-off may occur if calculations are performed with insufficient precision.

A force measuring device not subjected to repair, overloading, modifications, or other significant influence factors which alter its elastic properties or its sensing characteristics will likely exhibit the same degree of best fit on each succeeding calibration as was determined during its initial calibration using this procedure. A device not subjected to the influence factors outlined above which exhibits continued change of degree of best fit with several successive calibrations may not have sufficient performance stability to allow application of the curve fitting procedure of Annex A1.

7.2 Selection of Calibration Forces—A careful selection of the different forces to be applied in a calibration is essential to provide an adequate and unbiased sample of the full range of the deviations discussed in 7.1 and 7.1.1. For this reason, the selection of the calibration forces is made by the standardizing laboratory. An exception to this, and to the recommendations of 7.2.1 and 7.2.4, is made for specific force devices, where the selection of the forces is dictated by the needs of the user.

7.2.1 Distribution of Calibration Forces—Distribute the calibration forces over the full range of the instrument, providing, if possible, at least one calibration force for every 10 % interval throughout the range. It is not necessary, however that these forces be equally spaced. Calibration forces at less than one tenth of capacity are permissible and tend to give added assurance to the fitting of the calibration equation. If the lower limit of the loading range of the device (see 8.5.1) is anticipated to be less than one tenth of the maximum force applied during calibration, then forces should be applied at or below this lower limit. In no case should the smallest force applied be below the theoretical lower limit of the instrument as defined by the values:

$$400 \times \text{resolution for Class A loading range} \quad (4)$$

$$2000 \times \text{resolution for Class AA loading range}$$

An example of a situation to be avoided is the calibration at ten equally spaced force increments of a proving ring having a capacity deflection of 2000 divisions, where the program will fail to sample the wear pattern at the contacting surfaces of the micrometer screw tip and vibrating reed because the orientation of the two surfaces will be nearly the same at all ten forces as at zero force. Likewise, in a load cell calibration, forces selected to give readings near the step-switch points will fail to sample the slidewire irregularities or mismatching of the slidewire span to the step-switch increments.

7.2.2 The resolution of an analog type force-measuring instrument is determined by the ratio between the width of the pointer or index and the center to center distance between two adjacent scale graduation marks. Recommended ratios are $\frac{1}{2}$, $\frac{1}{5}$, or $\frac{1}{10}$. A center to center graduation spacing of at least 1.25 mm is required for the estimation of $\frac{1}{10}$ of a scale division. To express the resolution in force units, multiply the ratio by the number of force units per scale graduation. A vernier scale of dimensions appropriate to the analog scale may be used to allow direct fractional reading of the least main instrument scale division. The vernier scale may allow a main scale division to be read to a ratio smaller than that obtained without its use.

7.2.3 The resolution of a digital instrument is considered to be one increment of the last active number on the numerical

indicator, provided that the reading does not fluctuate by more than plus or minus one increment when no force is applied to the instrument. If the readings fluctuate by more than plus or minus one increment, the resolution will be equal to half the range of fluctuation.

7.2.4 Number of Calibration Forces—A total of at least 30 force applications is required for a calibration and, of these, at least 10 must be at different forces. Apply each force at least twice during the calibration.

7.2.5 Specific Force Devices (Limited Load Devices)—Because these devices are used only at the calibrated forces, select those forces which would be most useful in the service function of the instrument. Coordinate the selection of the calibration forces with the submitting organization. Apply each calibration force at least three times in order to provide sufficient data for the calculation of the standard deviation of the observed deflections about their average values.

7.3 Temperature Equalization During Calibration:

7.3.1 Allow the force-measuring instrument sufficient time to adjust to the ambient temperature in the calibration machine prior to calibration in order to assure stable instrument response.

7.3.2 The recommended value for room temperature calibrations is 23°C (73.4°F) but other temperatures may be used.

7.3.3 During calibration, monitor and record the temperature as close to the elastic device as possible. It is recommended that the test temperature not change more than $\pm 0.5^\circ\text{C}$ (1°F) during calibration. In no case shall the ambient temperature change by more than $\pm 1.0^\circ\text{C}$ during calibration.

7.3.4 Deflections of non-temperature compensated devices may be normalized in accordance with Section 9 to a temperature other than that existing during calibration.

7.3.5 Deflections of non-temperature compensated devices must be corrected in accordance with Section 9 to a nominal calibration temperature if the temperature changes more than $\pm 0.2^\circ\text{C}$ during calibration.

7.4 Procedural Order in Calibration—Immediately before starting the calibration, preload the force-measuring instrument to the maximum force to be applied at least two times. Preloading is necessary to reestablish the hysteresis pattern that tends to disappear during periods of disuse, and is particularly necessary following a change in the mode of loading, as from compression to tension. Some instruments may require more than two preloads to achieve stability in zero-force indication.

NOTE 4—Overload or proofload tests are not required by this practice. It must be emphasized that an essential part of the manufacturing process for a force-measuring instrument is the application of a series of overloads to at least 10 % in excess of rated capacity. This must be done by the manufacturer before the instrument is released for calibration or service.

7.4.1 After preloading, apply the calibration forces, approaching each force from a lesser force. Forces shall be applied and removed slowly and smoothly, without inducing shock or vibration to the force-measuring instrument. The time interval between successive applications or removals of forces, and in obtaining readings from the force-measuring instrument, shall be as uniform as possible. If a calibration force is to be followed by another calibration force of lesser magnitude, reduce the applied force on the instrument to zero before

applying the second calibration force. Whenever possible, plan the loading schedule so that repetitions of the same calibration force do not follow in immediate succession.

NOTE 5—For any force-measuring instrument, the errors observed at corresponding forces taken first by increasing the force to any given test force and then by decreasing the force to that test force may not agree. Force-measuring instruments are usually used under increasing forces, but if a force-measuring instrument is to be used under decreasing force, it should be calibrated under decreasing forces as well as under increasing force. Use the procedures for calibration and analysis of data given in Sections 7 and 8 except where otherwise noted. When a force measuring device is calibrated with both increasing and decreasing forces, it is recommended that the same force increments be applied, but that separate calibration equations be developed.

7.4.2 The standardizing laboratory shall decide whether or not a zero-force reading is to be taken after each calibration force. Factors such as the stability of the zero-force reading and the presence of noticeable creep under applied force are to be considered in making this decision. It is pointed out, however, that a lengthy series of incremental forces applied without return to zero reduces the amount of sampling of instrument performance. The operation of removing all force from the instrument permits small readjustments at the load contacting surfaces, increasing the amount of random sampling and thus producing a better appraisal of the performance of the instrument. It is recommended that not more than five incremental forces be applied without return to zero. This is not necessary when the instrument is calibrated with decreasing forces; however, any return to zero prior to application of all the individual force increments must be followed by application of the maximum force before continuing the sequence.

7.5 Randomization of Loading Conditions—Shift the position of the instrument in the calibration machine before repeating any series of forces. In a compression calibration, rotate the instrument by an amount such as one-third, one-quarter, or one-half turn, keeping its load axis on the center load axis of the machine, or replace the bearing block under the instrument by a block having different deflection characteristics. In a tension calibration, rotate coupling rods by amounts such as one-third, one quarter, or one-half turn, and shift and realign any flexible connectors. In a calibration in both tension and compression, perform a part of the compression calibration, do the tension calibration, then finish the compression calibration afterward. Introduce variations in any other factors that normally are encountered in service, as for example, disconnecting and reconnecting electrical cables. Allow sufficient warmup time if electrical disconnections are made.

NOTE 6—A situation to be avoided is rotating the force-measuring instrument from 0° to 180° to 0° during calibration, since the final position duplicates the first, and reduces the randomization of loading conditions.

8. Calculation and Analysis of Data

8.1 Deflection—Calculate the deflection values for the force-measuring instrument as the differences between the readings of the instrument under applied force and the averages of the zero-force readings taken before and after each application of force. If a series of incremental force readings has been taken without return to zero, a series of interpolated zero-force readings may be used for the calculations. In calculating the

average zero-force readings and deflections, express the values to the nearest unit in the same number of places as estimated in reading the instrument scale. Follow the instructions for the rounding method given in Practice E 29.

8.2 Calibration Equation—Fit a polynomial equation of the following form to the force and deflection values obtained in the calibration using the method of least squares:

$$\text{Deflection} = A_0 + A_1 F + A_2 F^2 + \dots + A_5 F^5 \quad (5)$$

where:

F = force, and
 A_0 through A_5 = coefficients.

A 2nd degree equation is recommended with coefficients A_3 , A_4 , and A_5 equal to zero. Other degree equations may be used. For example the coefficients A_2 through A_5 would be set equal to zero for a linearized load cell.

8.2.1 For high resolution devices (see 7.1.3), the procedure of Annex A1 may be used to obtain the best fit calibration curve. After determination of the best fit polynomial equation, fit the pooled calibration data to a polynomial equation of that degree per 8.2, and proceed to analyze the data per 8.3-8.5.2.2.

8.3 Fit separate polynomials of degree 1, 2, 3, 4, and 5 to the mean data. Denote the computed residual standard deviations by s_1 , s_2 , s_3 , s_4 , and s_5 respectively. The residual standard deviation from an m_1 -degree fit is:

$$s_{m_1} = \sqrt{\frac{d_1^2 + d_2^2 + \dots + d_n^2}{n_1 - m_1 - 1}} \quad (6)$$

where:

d_1, d_2 , etc. = differences between the fitted curve and the n observed mean values from the calibration data,

n_1 = number of distinct non-zero force increments, and

m_1 = the degree of polynomial fit.

NOTE 7—It is recognized that the departures of the observed deflections from the calibration equation values are not purely random, as they arise partly from the localized nonlinearities discussed in 7.1.1. As a consequence, the distributions of the residuals from the least squares fit may not follow the normal curve of error and the customary estimates based on the statistics of random variables may not be strictly applicable.

8.4 Uncertainty—For the purposes of this practice, uncertainty is defined as 2.4 times the standard deviation. If the calculated uncertainty is less than the instrument resolution, the uncertainty is then defined as that value equal to the resolution. Express the uncertainty in force units, using the average ratio of force to deflection from the calibration data.

NOTE 8—Of historical interest, the limit of 2.4 standard deviations was originally determined empirically from an analysis of a large number of force-measuring instrument calibrations and contains approximately 99 % of the residuals from least-squares fits of that sample of data.

8.5 Loading Range—This is the range of forces within which the uncertainty of a force-measuring instrument does not exceed the maximum permissible limits of error specified as a fraction or percentage of force. Since the uncertainty for the instrument is of constant force amplitude throughout the entire range of the instrument, it will characteristically be less than

the specified percentage of force at instrument capacity but will begin to exceed the specified percentage at some point in the lower range of the instrument, as illustrated in Fig. 1. The loading range shown in the figure thus extends from the point, A , where the uncertainty and error limit lines intersect, up to the instrument capacity. The loading range shall not include forces outside the range of forces applied during the calibration.

8.5.1 Lower Limit of Loading Range—Calculate the lower end of the loading range for a specified percentage limit of error, P , as follows:

$$\text{Lower limit} = \frac{100 \times \text{uncertainty}}{P} \quad (7)$$

8.5.2 Standard Loading Ranges—Two standard loading ranges are listed as follows, but others may be used where special needs exist:

8.5.2.1 Class AA—For instruments used as secondary reference standards, the uncertainty of the instrument must not exceed 0.05 % of force. The lower force limit of the instrument is 2000 times the uncertainty, in force units, obtained from the calibration data.

NOTE 9—For example, an instrument calibrated using primary force standards had a calculated uncertainty of 16 N (3.7 lbf). The lower force limit for use as a Class AA device is therefore $16 \times 2000 = 32\,000$ N ($3.7 \times 2000 = 7400$ lbf). The uncertainty will be less than 0.05 % of force for forces greater than this lower force limit to the capacity of the instrument. In no case shall the lower limit be less than 2 % (1/50) of the capacity of the instrument.

8.5.2.2 Class A—For instruments used to verify testing machines in accordance with Practices E 4, the uncertainty of the instrument must not exceed 0.25 % of force. The lower force limit of the instrument is 400 times the uncertainty, in force units, obtained from the calibration data.

NOTE 10—In the example of Note 11 the lower force limit for use as a Class A device is $16 \times 400 = 6400$ N ($3.7 \times 400 = 1480$ lbf). The uncertainty will be less than 0.25 % of force for forces greater than this lower force limit up to the capacity of the instrument.

NOTE 11—The term “loading range” used in this practice is parallel in meaning to the same term in Practices E 4. It is the range of forces over which it is permissible to use the instrument in verifying a testing machine or other similar device. When a loading range other than the two standard ranges given in 8.5.2 is desirable, the appropriate limit of error should be specified in the applicable method of test.

8.5.3 Precision and Bias—The magnitudes of uncertainty (see 8.4) and lower limit of loading ranges (see 8.5.2) which determine compliance to this standard are derived quantities based on statistical analysis of the calibration data. The calculated uncertainty is 2.4 times the standard deviation. As a function of probability, this limit of uncertainty means that, with 99 % probability, the error will not exceed the value of uncertainty.

8.6 Specific Force Devices—Any force-measuring device may be calibrated as a specific force device. Elastic rings, loops, and columns with dial indicators as a means of sensing deformation are generally classed as specific force devices because the relatively large localized nonlinearities introduced by indicator gearing produce an uncertainty too great for an adequate loading range. These instruments are, therefore, used only at the calibrated forces and the curve-fitting and analytical

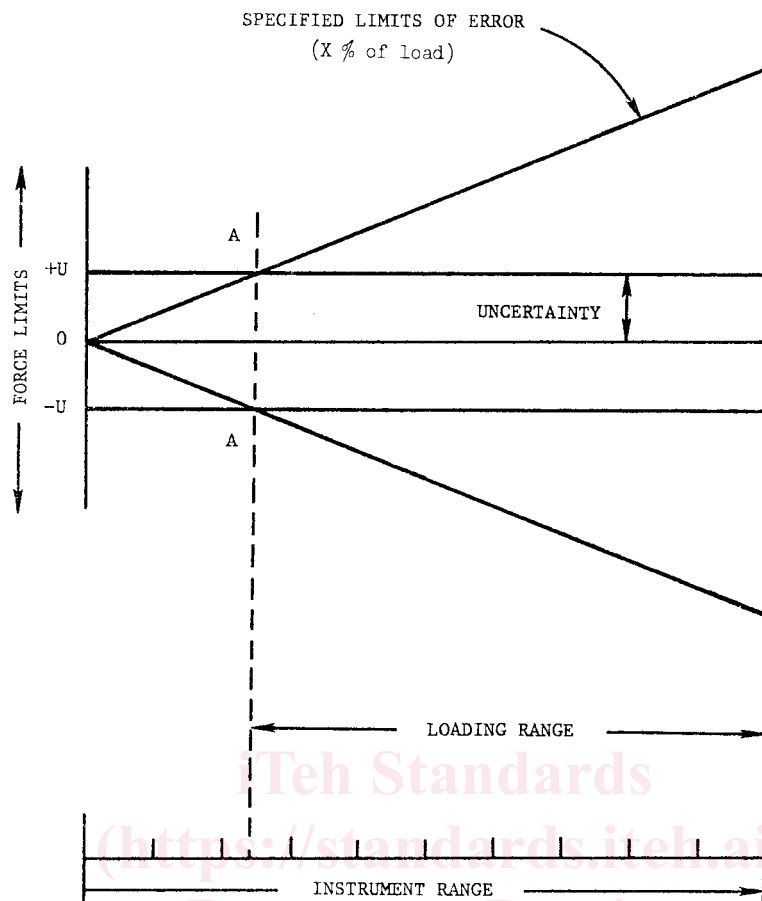


FIG. 1 Relationship of Loading Range to Instrument Uncertainty and Specified Limits of Error

procedures of 8.2-8.4 are replaced by the following procedures:

8.6.1 *Calculation of Nominal Force Deflection*—From the calibration data, calculate the average value of the deflections corresponding to the nominal force. If the calibration forces applied differ from the nominal value of the force, as may occur in the case of a calibration by secondary standards, adjust the observed deflections to values corresponding to the nominal force by linear interpolation provided that the load differences do not exceed ± 1 % of capacity force. The average value of the nominal load deflection is the calibrated value for that force.

8.6.2 *Standard Deviation for a Specific Force Device*—Calculate the range of the nominal force deflections for each calibration force as the difference between the largest and smallest deflections for the force. Multiply the average value of the ranges for all the calibration forces by the appropriate factor from Table 1 to obtain the estimated standard deviation of an individual deflection about the mean value.

TABLE 1 Estimates of Standard Deviation from the Range of Small Samples

Number of Observations at Each Force	Multiplying Factor for Range
3	0.591
4	0.486
5	0.430
6	0.395

8.6.3 *Uncertainty for Specific Force Devices*—The uncertainty for a specific force device is defined as 2.0 times the standard deviation, plus the resolution. Convert the uncertainty into force units by means of a suitable factor and round to the number of significant figures appropriate to the resolution. The uncertainty is expressed as follows:

$$\text{Uncertainty} = (2s + r)f \quad (8)$$

where:

s = standard deviation,

r = resolution

f = average ratio of force to deflection from the calibration data.

8.6.4 *Precision Force*—A specific force device does not have a loading range as specified in 8.5, since it can be used only at the forces for which it was calibrated. The use is restricted, however, to those calibrated forces that would be included in a loading range calculated in 8.5-8.5.2.2.

9. Temperature Corrections for Force-Measuring Instruments During Use

9.1 *Referenced Temperature of Calibration*—It is recommended that the temperature to which the calibration is referenced be 23°C (73°F), although other temperatures may be referenced (see 7.3.2).

9.2 *Temperature Corrections*—Nearly all mechanical elastic force-measuring instruments require correction when used at a