EUROPEAN STANDARD

NORME EUROPÉENNE

EUROPÄISCHE NORM

EN 60099-4/A1

August 2006

ICS 29.120.50; 20.240.10

English version

Surge arresters
Part 4: Metal-oxide surge arresters without gaps for a.c. systems
(IEC 60099-4:2004/A1:2006)

Parafoudres
Partie 4: Parafoudres à oxyde métallique sans éclateurs pour réseaux à courant alternatif
(CEI 60099-4:2004/A1:2006)

Überspannungsableiter
Teil 4: Metalloxidableiter ohne Funkenstrecken für Wechselspannungsnetze
(IEC 60099-4:2004/A1:2006)

This amendment A1 modifies the European Standard EN 60099-4:2004; it was approved by CENELEC on 2006-07-01. CENELEC members are bound to comply with the CEN/CENELEC Internal Regulations which stipulate the conditions for giving this amendment the status of a national standard without any alteration.

Up-to-date lists and bibliographical references concerning such national standards may be obtained on application to the Central Secretariat or to any CENELEC member.

This amendment exists in three official versions (English, French, German). A version in any other language made by translation under the responsibility of a CENELEC member into its own language and notified to the Central Secretariat has the same status as the official versions.

CENELEC members are the national electrotechnical committees of Austria, Belgium, Cyprus, the Czech Republic, Denmark, Estonia, Finland, France, Germany, Greece, Hungary, Iceland, Ireland, Italy, Latvia, Lithuania, Luxembourg, Malta, the Netherlands, Norway, Poland, Portugal, Romania, Slovakia, Slovenia, Spain, Sweden, Switzerland and the United Kingdom.

CENELEC
European Committee for Electrotechnical Standardization
Comité Européen de Normalisation Electrotechnique
Europäisches Komitee für Elektrotechnische Normung

Central Secretariat: rue de Stassart 35, B - 1050 Brussels

Ref. No. EN 60099-4:2004/A1:2006 E

Foreword

The text of document 37/324/FDIS, future amendment 1 to IEC 60099-4:2004, prepared by IEC TC 37, Surge arresters, was submitted to the IEC-CENELEC parallel vote and was approved by CENELEC as amendment A1 to EN 60099-4:2004 on 2006-07-01.

The following dates were fixed:

– latest date by which the amendment has to be implemented at national level by publication of an identical national standard or by endorsement	(dop)	2007-04-01
– latest date by which the national standards conflicting with the amendment have to be withdrawn	(dow)	2009-07-01

Endorsement notice

The text of amendment 1:2006 to the International Standard IEC 60099-4:2004 was approved by CENELEC as an amendment to the European Standard without any modification.

INTERNATIONAL STANDARD

IEC 60099-4

2004

AMENDMENT 1
2006-05

Amendment 1

Surge arresters –

Part 4: Metal-oxide surge arresters without gaps for a.c. systems

*This **English-language** version is derived from the original **bilingual** publication by leaving out all French-language pages. Missing page numbers correspond to the French-language pages.*

International Electrotechnical Commission, 3, rue de Varembé, PO Box 131, CH-1211 Geneva 20, Switzerland
Telephone: +41 22 919 02 11 Telefax: +41 22 919 03 00 E-mail: inmail@iec.ch Web: www.iec.ch

Commission Electrotechnique Internationale
International Electrotechnical Commission
Международная Электротехническая Комиссия

PRICE CODE S

For price, see current catalogue

FOREWORD

This amendment has been prepared by IEC technical committee 37: Surge arresters.

The text of this amendment is based on the following documents:

FDIS	Report on voting
37/324/FDIS	37/325/RVD

Full information on the voting for the approval of this amendment can be found in the report on voting indicated in the above table.

The committee has decided that the contents of this publication will remain unchanged until the maintenance result date indicated on the IEC web site under "http://webstore.iec.ch" in the data related to the specific publication. At this date, the publication will be

- reconfirmed;
- withdrawn;
- replaced by a revised edition, or
- amended.

____

Page 3

CONTENTS

Replace, on page 7, the title of Annex N by the following new title:

Page 9

Add:

Delete the titles of Figures N.1, N.2 and N.3.

Page 11

Add:

Table 14 – Test requirements

Table 15 – Required currents for short-circuit tests

Delete the titles of Tables N.1, N.2 and N.3.

Page 51

6.11 Short circuit

Replace the text of this subclause by the following:

An arrester for which a short-circuit rating is claimed by the manufacturer shall be subjected to a short-circuit test according to 8.7 to show that the arrester will not fail in a manner that causes violent shattering of the housing and that self-extinguishing of open flames (if any) occurs within a defined period of time.

6.12.1 Disconnector withstand

Add to this subclause the following third dashed item:

– for surge arresters to be installed in overhead lines with system voltages exceeding 52 kV, test of the lightning impulse discharge capability (see Annex N).

Page 53

Add, after 6.16, the following new subclause:

6.17 Lightning impulse discharge capability

For surge arresters to be installed in overhead lines with system voltages exceeding 52 kV, the lightning impulse discharge capability shall be demonstrated by the tests and procedures of Annex N.

Page 57

Table 3 – Arrester type tests

Delete all references to Annex N.

Page 75

Add, after 8.5.2.2, on page 77, the following new subclauses:

8.5.2.3 Test procedure for resistor elements stressed at or above the reference voltage

If U_{ct} is close to or above the reference voltage, it may not be possible to perform an accelerated ageing test at U_{ct}, due to the extreme voltage dependence for the power losses and stability of available voltage source. If $U_{ct} \geq 0{,}95*U_{ref}$ and if it is not possible to perform an accelerated ageing test according to 8.5.2.1, this alternative test procedure shall apply and replaces 8.5.2.1 and 8.5.2.2.

NOTE To provide an overview and to serve as an aid to understanding the procedure, the steps required are as follows.

1) Calculate power loss, P_{ct}, for the highest stressed resistor (at T_a = 40 °C and $U = U_c$).
2) Determine the steady-state temperature, T_{st}, for the highest stressed part of the arrester by using one of the three alternative procedures of 8.5.2.3.1.
3) At a voltage U_{ct}, determine the ratio, k_x, of power loss at 115 °C to power loss at T_{st} for the type of resistor elements used.
4) Perform an accelerated ageing test at constant power loss, $k_x * P_{ct}$.
5) Interrupt the test for a short time and take measurements of power loss at specified time intervals.
6) If T_{st} > 60 °C, increase test temperature or test time.
7) Evaluate the power losses of step 5) according to 8.5.2.3.3.

8.5.2.3.1 Determination of test parameters

Calculate the power losses, P_{ct}, per resistor element at the maximum ambient temperature of 40 °C with the arrester energized at U_c, for the highest voltage stressed resistor according to Annex L including the effect of the resistive current.

NOTE 1 For dead-front and liquid-immersed arresters, 65 °C and 95 °C, respectively, apply as maximum ambient temperatures.

Select one of the three following test procedures to determine the steady-state temperature, T_{st}, of the most stressed part of the arrester at maximum ambient temperature.

NOTE 2 The test procedures are considered to be conservative in increasing order from 1 to 3.

1. At an ambient temperature of 25 °C ± 10 K, energize the complete arrester at the claimed U_c until steady-state temperature conditions have been attained. The temperature shall be measured on resistor elements, at five points as evenly spaced as possible over the most highly stressed 20 % portion of the length of each column of the arrester. If this 20 % portion contains less than five resistor elements, the number of measuring points may be limited to one point on each resistor element. The average temperature rise above ambient of the resistor elements shall be added to the maximum ambient temperature to obtain the temperature T_{st}.
2. At the maximum ambient temperature, energize a thermally pro-rated section representative for the arrester type at a voltage level, which results in the same power losses per resistor element as determined above. Keep the power losses constant by adjusting the voltage if necessary. Measure the temperature of the resistors in steady-state condition and calculate the average steady-state temperature, which is set equal to T_{st}.
3. At an ambient temperature of 25 °C ± 10 K, energize a thermally pro-rated section representative for the arrester type at a voltage level which results in the same power losses per resistor element as determined above. Keep the power losses constant by adjusting the voltage if necessary. Measure the temperature of the resistors in steady-state condition and calculate the average steady-state temperature rise, ΔT_{st}, above ambient. Determine the temperature, T_{st}, by adding ΔT_{st} to the maximum ambient temperature.

The prorated section shall represent the steady-state thermal behaviour of the complete arrester.

NOTE 3 The section may not necessarily be the same as that used for the operating duty test.

At a voltage U_{ct}, determine the ratio, k_x, of power losses at 115 °C to power losses at T_{st} for the type of resistor elements used. For this test the voltage source shall fulfil the requirements according to 8.5.1.

8.5.2.3.2 Test procedure

Three resistor samples shall be subjected to constant power losses equal to k_x*P_{ct} (tolerance $^{+30}_{0}$ %) for 1 000 h. During the test, the temperature shall be controlled to keep the surface temperature of the resistor at the required test temperature $T_t \pm 4$ K. The applied test voltage at the start of the test shall be not less than $0,95*U_{ct}$.

If the temperature, T_{st}, is equal to or below 60 °C, T_t shall be 115 °C. If T_{st} is above 60 °C, either the test temperature or the testing time shall be increased as follows.

a) Increase of the test temperature

$$T_t = 115 + (T_{st} - T_{a,max} - \Delta T_n)$$

where

T_t is the test temperature in °C;

T_{st} is the steady-state temperature of the resistors in °C;

$T_{a,max}$ is the maximum ambient temperature in °C;

ΔT_n = 20 K.

NOTE 1 For liquid-immersed arresters ΔT_n = 25 K, which results from the requirement that the operating duty test starting temperature for these arresters (120 °C) is 25 K above the maximum ambient temperature (95 °C), while for other arresters the difference between the operating duty test starting temperature and the maximum ambient temperature is 20 K.

b) Increase of the testing time

$$t = t_0 * 2,5^{\Delta T/10}$$

where

t is the testing time in h;

t_0 = 1 000 h;

ΔT is the temperature above 60 °C.

NOTE 2 For dead-front and liquid-immersed arresters, t_0 is 2 000 h and 7 000 h, respectively, and ΔT is the temperature above 85 °C and 120 °C, respectively.

8.5.2.3.3 Determination of elevated rated and continuous operating voltages

The three test samples shall be heated to $T_t \pm 4$ K and subjected to the constant power losses k_x*P_{ct}. One to two hours after the voltage application, the voltage is adjusted to a voltage in the range 0,95* U_{ct} to U_{ct} and the power losses, P_{1ct}, are measured. During the test, after 30 %, 50 % and 70 % of the testing time, the measurement of power losses is repeated under the same conditions with respect to temperature and voltage. The minimum power loss values at these times are designated as P_{3ct}. At the end of the ageing test, under the same conditions with regard to block temperature and at the same voltage, the power losses P_{2ct} are determined.

- If P_{2ct} is equal to or below 1,1 times P_{3ct}, then the test according to 8.5.4 and 8.5.5 shall be performed on new resistors:
  - if P_{2ct} is equal to or less than P_{1ct}, U_{sc} and U_{sr} are used without any modification;
  - if $P_{2ct} > P_{1ct}$, the ratio P_{2ct}/P_{1ct} is determined for each sample. The highest of these ratios is called K_{ct}. On three new resistors at ambient temperature, the power losses P_{1c} and P_{1r} are measured at U_{sc} and U_{sr}, respectively. Thereafter, the voltages are increased so that the corresponding power losses P_{2c} and P_{2r} fill the relation:

$$\frac{P_{2c}}{P_{1c}} = K_{ct} ; \qquad \frac{P_{2r}}{P_{1r}} = K_{ct}$$

  U_c* and U_r* are the highest of the three increased voltages obtained. As an alternative, aged resistors may also be used after agreement between the user and the manufacturer.

- If P_{2ct} is greater than 1,1 times P_{3ct}, and P_{2ct} is greater than or equal to P_{1ct}, then aged resistors shall be used for the following test of 8.5.4 and 8.5.5. New resistors with corrected values U_c* and U_r* can be used, but only after agreement between the user and the manufacturer.

Aged resistors are, by definition, resistors tested according to 8.5.2.3.2.

These cases are summarized in Table 7.

Where aged resistors are used in the operating duty test, it is recommended that the time delay between the ageing test and the operating duty test be not more than 24 h.

The measuring time should be short enough to avoid increased power loss due to heating.

Page 91

8.7 Short-circuit test procedure

Replace the title and contents of 8.7 by the following new title and text:

8.7 Short-circuit tests

8.7.1 General

Arresters, for which a short-circuit rating is claimed by the manufacturer, shall be tested in accordance with this subclause. The test shall be performed in order to show that an arrester failure does not result in a violent shattering of the arrester housing, and that self-extinguishing of open flames (if any) occurs within a defined period of time. Each arrester type is tested with four values of short-circuit currents. If the arrester is equipped with some other arrangement as a substitute for a conventional pressure relief device, this arrangement shall be included in the test.

The frequency of the short-circuit test current supply shall be between 48 Hz and 62 Hz.

With respect to the short-circuit current performance, it is important to distinguish between two designs of surge arresters.

- “Design A” arresters have a design in which a gas channel runs along the entire length of the arrester unit and fills ≥50 % of the internal volume not occupied by the internal active parts.
- “Design B” arresters are of a solid design with no enclosed volume of gas or having an internal gas volume filling <50 % of the internal volume not occupied by the internal active parts.

NOTE 1 Typically, “Design A” arresters are porcelain-housed arresters, or polymer-housed arresters with a composite hollow insulator which are equipped either with pressure-relief devices, or with prefabricated weak spots in the composite housing which burst or flip open at a specified pressure, thereby decreasing the internal pressure.

Typically, “Design B” arresters do not have any pressure relief device and are of a solid type with no enclosed volume of gas. If the resistors fail electrically, an arc is established within the arrester. This arc causes heavy evaporation and possibly burning of the housing and/or internal material. These arresters’ short-circuit performance is determined by their ability to control the cracking or tearing-open of the housing due to the arc effects, thereby avoiding violent shattering.

NOTE 2 "Active parts" in this context are the non-linear, metal-oxide resistors and any metal spacers directly in series with them.

Depending on the type of arrester and test voltage, different requirements apply with regard to the number of test samples, initiation of short-circuit current and amplitude of the first short-circuit current peak. Table 14 shows a summary of these requirements which are further explained in the following subclauses.

NOTE 3 After agreement between the manufacturer and the purchaser, the test procedure can be modified to include, for example, a number of reclosing operations. For such special tests, the procedure and acceptance criteria should be agreed upon between the manufacturer and the purchaser.

8.7.2 Preparation of the test samples

For the high-current tests, the test samples shall be the longest arrester unit used for the design with the highest rated voltage of that unit used for each different arrester design.

For the low-current test, the test sample shall be an arrester unit of any length with the highest rated voltage of that unit used for each different arrester design.

NOTE 1 Figure 13 shows different examples of arrester units.

In case a fuse wire is required, the fuse wire material and size shall be selected so that the wire will melt within the first 30 electrical degrees after initiation of the test current.

NOTE 2 In order to have melting of the fuse wire within the specified time limit and create a suitable condition for arc ignition, it is generally recommended that a fuse wire of a low resistance material (for example copper, aluminium or silver) with a diameter of about 0,2 mm to 0,5 mm be used. Higher fuse-wire cross-sections are applicable to surge arrester units prepared for higher short-circuit test currents. When there are problems in initiating the arc, a fuse wire of larger size but with a diameter not exceeding 1,5 mm, may be used since it will help arc establishment. In such cases, a specially prepared fuse wire, having a larger cross-section along most of the arrester height with a short thinner section in the middle, may also help.

8.7.2.1 “Design A” arresters

The samples shall be prepared with means for conducting the required short-circuit current using a fuse wire. The fuse wire shall be in direct contact with the MO resistors and be positioned within, or as close as possible to, the gas channel and shall short-circuit the entire internal active part. The actual location of the fuse wire in the test shall be reported in the test report.

No differences with regard to polymer housings or porcelain housings are made in the preparation of the test samples. However, differences partly apply in the test procedure (see 8.7.4.2). In this case, "Design A" arresters with polymeric sheds which are not made of porcelain or other hollow insulators, and which are as brittle as ceramics, shall be considered and tested as porcelain-housed arresters.

8.7.2.2 "Design B" arresters

"Design B" arresters with polymeric sheds which are not made of porcelain or other mechanically supporting structures, and which are as brittle as ceramics, shall be considered and tested as porcelain-housed arresters.

8.7.2.2.1 Polymer-housed arresters

No special preparation is necessary. Standard arrester units shall be used. The arrester units shall be electrically pre-failed with a power frequency overvoltage. The overvoltage shall be run on completely assembled test units. No physical modification shall be made to the units between pre-failing and the actual short-circuit current test.

The overvoltage given by the manufacturer shall be a voltage exceeding 1,15 times U_c. The voltage shall cause the arrester to fail within (5 ± 3) min. The resistors are considered to have failed when the voltage across the resistors falls below 10 % of the originally applied voltage. The short-circuit current of the pre-failing test circuit shall not exceed 30 A.

The time between pre-failure and the rated short-circuit current test shall not exceed 15 min.

NOTE The pre-failure can be achieved by either applying a voltage source or a current source to the samples.

– Voltage source method: the initial current should typically be in the range 5-10 mA/cm². The short-circuit current should typically be between 1 A and 30 A. The voltage source need not be adjusted after the initial setting, although small adjustments might be necessary in order to fail the resistors in the given time range.

– Current source method: Typically a current density of around 15 mA/cm² with a variation of ±50 %, will result in failure of the resistors in the given time range. The short-circuit current should typically be between 10 A and 30 A. The current source need not be adjusted after the initial setting, although small adjustments might be necessary in order to fail the resistors in the given time range.

8.7.2.2.2 Porcelain-housed arresters

The samples shall be prepared with means for conducting the required short-circuit current using a fuse wire. The fuse wire shall be in direct contact with the MO resistors and be located as far away as possible from the gas channel and shall short-circuit the entire internal active part. The actual location of the fuse wire in the test shall be reported in the test report.

8.7.3 Mounting of the test sample

For a base-mounted arrester, the mounting arrangement is shown in Figures 14a and 14b. The distance to the ground from the insulating platform and the conductors shall be as indicated in Figures 14a and 14b.