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# INTERNATIONAL STANDARD

# NORME INTERNATIONALE

Optical amplifiers **– Test methods DARD PREVIEW** Part 10-1: Multichannel parameters – Pulse method using an optical switch and optical spectrum analyzer (Standards.Iten.al)

Amplificateurs optiques – Méthodes d'essai/ab8a7192-0094-47ac-a8f0-Partie 10-1: Paramètres à canaux multiples –1 Méthode d'impulsion utilisant un interrupteur optique et un analyseur de spectre optique





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# **INTERNATIONAL STANDARD**

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Optical amplifiers intest methods DARD PREVIEW Part 10-1: Multichannel parameters – Pulse method using an optical switch and optical spectrum analyzer

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# OPTICAL AMPLIFIERS – TEST METHODS –

# Part 10-1: Multichannel parameters – Pulse method using an optical switch and optical spectrum analyzer

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International Standard IEC 61290-10-1 has been prepared by subcommittee 86C: Fibre optic systems and active devices, of IEC technical committee 86: Fibre optics.

This second edition cancels and replaces the first edition published in 2003. It is a technical revision with updated references and cautions on proper use of the procedure.

This International Standard is to be read in conjunction with IEC 61291-1.

The text of this standard is based on the following documents:

CDV	Report on voting
86C/778/CDV	86C/809/RVC

Full information on the voting for the approval of this standard can be found in the report on voting indicated in the above table.

This publication has been drafted in accordance with the ISO/IEC Directives, Part 2.

A list of all parts of the IEC 61290 series, published under the general title *Optical amplifiers* – *Test methods*<sup>1)</sup> can be found on the IEC website.

The committee has decided that the contents of this publication will remain unchanged until the maintenance result date indicated on the IEC web site under "http://webstore.iec.ch" in the data related to the specific publication. At this date, the publication will be

- reconfirmed,
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The first editions of some of these parts were published under the general title Optical fibre amplifiers – Basic specification or Optical amplifier test methods.

# INTRODUCTION

This International Standard is devoted to the subject of optical fibre amplifiers. The technology of optical fibre amplifiers is still rapidly evolving, hence amendments and new editions to this standard can be expected.

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# OPTICAL AMPLIFIERS – TEST METHODS –

# Part 10-1: Multichannel parameters – Pulse method using an optical switch and optical spectrum analyzer

# 1 Scope and object

This part of IEC 61290 applies to optical amplifiers (OAs) using active fibres and waveguides, containing rare-earth dopants, currently commercially available.

The object of this standard is to establish uniform requirements for accurate and reliable measurements of the signal-spontaneous noise figure as defined in IEC 61291-1.

The test method independently detects amplified signal power and amplified spontaneous emission (ASE) power by launching optical pulses into the OA under test and synchronously detecting "on" and "off" levels of the output pulses by using an optical sampling switch and an optical spectrum analyzer (OSA).

Such measurement is possible because the gain response of the rare-earth doped OA is relatively slow, particularly in Er-doped OAs: However, since the OA gain dynamics vary with amplifier types, operating conditions and control schemes, the gain dynamics should be carefully considered when applying the present test method to various OA. The manufacturer of the OA should present data validating the required modulation frequency to limit the error to <1 dB. The measurements for obtaining this information are described in Annex C.

The test method is described basically for multichannel applications, which includes single channel applications as a special case of multichannel (wavelength-division multiplexed) applications.

NOTE All numerical values followed by (‡) are currently under study.

#### 2 Normative references

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

IEC 61291-1, Optical amplifiers – Part 1: Generic specification

#### 3 Abbreviated terms

For the purposes of this document, the following abbreviated terms apply:

AGC	automatic gain control
ALC	automatic level control
AOM	acousto-optic modulator
APC	automatic power control
ASE	amplified spontaneous emission
CW	continuous wave

DBR	distributed Bragg reflector (laser diode)
DC	direct current
DFB	distributed feed-back (laser diode)
ECL	external cavity laser (diode)
EDFA	erbium-doped fibre amplifier
ER	erbium
FWHM	full width at half maximum
LED	light emitting diode
LD	laser diode
NF	noise figure
OA	optical amplifier
OSA	optical spectrum analyzer
SW	switch

# 4 Apparatus

The basic measurement set-up is given in Figure 1.



Figure 1 – Typical arrangement of the optical pulse test method

The test equipment needed, with the required characteristics, is listed below.

 a) Optical pulse source: Two arrangements of the optical pulse source are possible as shown in Figure 2. Optical pulse source a (Figure 2a) consists of CW optical sources with an external optical switch and attenuator(s). Optical pulse source b (Figure 2b) consists of directly modulated optical sources and attenuator(s).



Figure 2a – Arrangement with external optical switch



Figure 2b – Arrangement with directly modulated optical source

#### Figure 2 – Two arrangements of the optical pulse source

Unless otherwise specified, the full width at half maximum (FWHM) of the output spectrum of optical pulse source *a* or *b* shall be narrower than 0,1 nm ( $\ddagger$ ) so as not to cause any interference to adjacent channels. In the case of a single-channel source, it shall be narrower than 1 nm ( $\ddagger$ ). Distributed feedback (DFB) lasers, distributed Bragg reflection (DBR) lasers, and external cavity lasers (ECLs), for example, are applicable. The suppression ratio of the side modes of these DFB lasers shall be higher than 30 dB ( $\ddagger$ ). The output power fluctuation shall be less than 0,05 dB ( $\ddagger$ ), which may be more easily attainable with an optical isolator placed at the output port of each source.

Optical pulse source a simultaneously pulsates wavelength-division multiplexed light with an optical switch, where the switching time is common to all the channels; timing adjustment is not needed. Moreover, frequency chirping and spontaneous emission can be minimum; the extinction ratio of the "on" versus "off" stages can be uniquely determined at a high level if a high extinction-ratio switch is used. An acousto-optic modulator (AOM) is typically used as the switch.

For optical pulse source *b*, the leakage power at the off-state should be as small as possible to minimize the measurement error, although calibration is possible by subtracting the leaked power. This may demand a zero-bias operation of laser diode sources. Moreover, care must be taken in synchronizing optical pulses because the pulse timing may differ from one source to another.

- b) Variable optical attenuator: The attenuation range and stability shall be over 40 dB (‡) and better than ± 0,1 dB (‡), respectively. The reflectance from this device shall be smaller than -40 dB (‡) at each port. The variable optical attenuator may be incorporated in the optical pulse source.
- c) Optical switch: This device shall have a polarization sensitivity less than ± 0,1 dB (‡), static isolation better than 65 dB (‡), transition time less than 50 ns (‡), and switching delay time less than 2 ms (‡). The reflectance from this device shall be smaller than -40 dB (‡) at each port. Figure 3 defines the optical switch static isolation. The optical switch is not required for optical pulse source b.



Figure 3 – Static isolation of an optical switch

d) Pulse generator: This device is used to drive optical pulse sources and the optical sampling switch. When using an internally modulated optical pulse source, an independent pulse generator is not required. Pulse train(s) shall be generated with a pulse interval of, typically, 1 μs to 2 μs (‡). The pulse widths shall be adjustable from 100 ns to 2 ms (‡) with a step of 5 ns or finer. The delay shall be adjustable at least from 100 ns to 4 μs (‡) in steps of 5 ns or

finer. The rise time and fall time,  $t_r$  and  $t_f$ , of the output optical pulse shall be less than 10 ns (‡). Definitions of  $t_r$  and  $t_f$  are given in Figure 4.



Figure 4 – Definitions of rise time and fall time,  $t_r$  and  $t_f$  of optical pulses

- e) Optical spectrum analyzer: This device shall have polarization sensitivity less than 0,1 dB (‡), stability better than ±0,1 dB (‡), wavelength accuracy better than ±0,5 nm (‡), and wavelength reproducibility better than 0,01 nm (‡). The device shall have a measurement range at least from -75 dBm to +20 dBm (‡) with a resolution better than 0,1 nm (‡). The reflectance from this device shall be smaller than -40 dB (‡) at its input port.
- f) Optical power meter: This device shall have a measurement accuracy better than ±0,2 dB (‡), irrespective of the state of the input light polarization, within the operational wavelength band of the OA and within a power range from -40 dBm to +20 dBm (‡).
- g) Optical connectors: The connection loss repeatability shall be better than ±0,1 dB (‡). The reflectance from this device shall be smaller than ±0,1 dB (‡).
- h) Optical fibre jumpers: The mode field diameter of the optical fibre jumpers shall be as close as possible, so as not to cause excessive loss and reflectance, to that of fibres used as input and output ports of the OA. The reflectance from optical fibre jumpers shall be smaller than -40 dB (‡), and the device length shall be short (<2 m).</li>

## 5 Test sample

The OA shall operate at nominal operating conditions. If the OA is likely to cause laser oscillations due to unwanted reflections, optical isolators should be used to bracket the OA under test. This will minimize the signal instability and the measurement inaccuracy.

Care shall be taken in the state of polarization of the input light during the measurement. Changes in the polarization state of the input light may result in input optical power changes because of the slight polarization dependency expected from all the optical components used, leading to measurement errors.

# 6 Procedure

The test procedure consists of four parts:

- a) initial system setting and calibration;
- b) sampling window adjustment;
- c) OA measurement and
- d) calculation.

The measurement flow is given in Figure 5. This procedure enables self-consistent calculation of not only OA noise factor but also ASE power and signal gain.



Figure 5 – Measurement flow chart

## 6.1 Calibration

## 6.1.1 Calibration of OSA power measurement

Calibrate the OSA power measurement by using a calibrated power meter.

NOTE The calibrated optical power meter detects all the optical power including source spontaneous emission, whereas the OSA measurement detects just the optical power within the resolution bandwidth of the OSA. Therefore, use of an optical filter with a FWHM passband of 1 nm to 3 nm is recommended at the output of the optical pulse source to increase the calibration accuracy.

# 6.1.2 Calibration of the pulse duty ratio

Follow the steps below to calibrate the pulse duty ratio.

- a) Activate any one channel of the optical pulse source at CW and the specified power and wavelength.
- b) Set the pulse width  $T_{\text{source}}$  and the pulse interval *T* of the optical pulse source output as specified in the product specification.  $T_{\text{source}}$  and *T* shall be sufficiently shorter than the gain-response time of the OA under test. For EDFAs,  $T_{\text{source}}$  and *T* are typically 0,4 µs (‡)

and 1  $\mu s$  (‡), respectively. These values, however, depend on the amplifier saturation condition.

NOTE Measurement accuracy versus pulse rates is given in informative Annex B. EDFA output waveforms for various EDFAs are given in informative Annex A.

- c) Measure the average output power,  $P_{pulse-ave}$ , with a power meter.
- d) Drive the optical pulse source with 100 % duty pulse (DC drive), and measure the output power,  $P_{\text{DC}}$ , with a power meter.
- e) Calculate the equivalent duty ratio by using Equation (1).

$$DR_{\text{source}} = \frac{P_{\text{pulse-ave}}}{P_{\text{DC}}}$$
(1)

NOTE For the optical pulse source using an external optical switch, the calibration result is applicable to the other channels.

For the optical pulse source using direct modulation, the calibration shall be repeated for all the channels, because the optical-pulse shape generated by each source can be different.

#### 6.1.3 Calibration of the sampling module

Follow the steps below to calibrate the sampling module.

a) Arrange the optical pulse source, sampling SW, OSA and calibrated power meter as shown in Figure 6.





- b) Activate the optical pulse source to emit CW light at a channel wavelength to be tested.
- c) Set the OSA optical bandwidth, *B*<sub>o</sub>, in a way to accommodate the spectral bandwidth of the pulse signal.
- d) Adjust the OSA centre wavelength to the wavelength selected at step b).
- e) Set the sampling pulse width,  $T_{\text{sampler}}$ , as specified in the product specification. The sum of the duty ratios, the source duty ratio plus sampler duty ratio, shall be less than 100 % while still keeping some margin, e.g., 80 % to 90 %.  $T_{\text{sampler}}$  shall be smaller than  $T_{\text{source}}$ . Measure the average output power,  $P_{\text{OSA-pulse-ave}}$  with the OSA.
- f) Drive the sampling switch with a 100 % duty pulse (DC drive).
- g) Measure  $P_{OSA-DC}$  with the OSA.
- h) Calculate the equivalent sampling switch duty ratio by using Equation (2).

$$DR_{\text{sampler}} = \frac{P_{\text{OSA-pulse-ave}}}{P_{\text{OSA-DC}}}$$
(2)

NOTE The value of  $DR_{sampler}$  thus obtained at one channel wavelength is applicable to the other channel wavelengths.

- i) Measure the input power to the sampling switch, *P*<sub>CW-calibd</sub>, with a calibrated power meter.
- j) Activate the optical pulse source to emit CW light at the next channel wavelength to be tested. Repeat steps g) through i) for the next channel wavelength to be measured.
- k) Calculate the calibration factor,  $CAL(\lambda_k)$ , of the sampler including the OSA by using Equation (3).

$$CAL(\lambda_{\rm k}) = \frac{P_{\rm OSA-DC}}{P_{\rm CW-calibd}}$$
(3)

#### 6.1.4 Calibration of dynamic isolation

#### 6.1.4.1 Timing adjustment of the sampling switch (SW)

Follow the steps below for timing adjustment of the sampling switch.

 a) Connect the optical pulse source and the sampling switch plus OSA with a fibre cord as shown in Figure 7, in which optical pulse source *a* is illustrated as the optical pulse source. Optical pulse source *b* is also applicable here.



#### Figure 7 – Arrangement for timing adjustment

b) Activate the optical pulse source to emit light at all channel wavelengths.

NOTE Although the delay time can be determined by using just one channel, the present test procedure activates all the channels at this stage so that the multichannel optical pulse source can be better stabilized for later stages of the measuring procedure.

- c) Adjust the OSA centre wavelength to one arbitrary channel wavelength.
- d) Set the drive pulse timing for the optical pulse source and the sampling switch as shown in Figure 8.  $DR_{sampler}$  shall be smaller than  $DR_{source}$ .
- e) Find the delay time, *T*<sub>d-min</sub>, that minimizes the received optical power with the OSA by tuning the CH2 delay time *T*<sub>d</sub>.
- f) Calculate the delay time  $T_{d-max}$  that maximizes the received optical power with the OSA by using Equation (4).

$$T_{d-max} = T_{d-min} - \frac{T_{p}}{2}$$
(4)

NOTE The delay time thus obtained at one channel wavelength is applicable to the other channel wavelengths.