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**Izračun efektivnih parametrov magnetnih sestavnih delov (IEC 60205:2006)**

Calculation of the effective parameters of magnetic piece parts (IEC 60205:2006)

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English version

**Calculation of the effective parameters of magnetic piece parts  
(IEC 60205:2006)**

Calcul des paramètres effectifs  
des pièces ferromagnétiques  
(CEI 60205:2006)

Berechnung der effektiven Kernparameter  
magnetischer Formteile  
(IEC 60205:2006)

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Up-to-date lists and bibliographical references concerning such national standards may be obtained on application to the Central Secretariat or to any CENELEC member.

This European Standard exists in two official versions (English and German). A version in any other language made by translation under the responsibility of a CENELEC member into its own language and notified to the Central Secretariat has the same status as the official versions.

CENELEC members are the national electrotechnical committees of Austria, Belgium, Cyprus, the Czech Republic, Denmark, Estonia, Finland, France, Germany, Greece, Hungary, Iceland, Ireland, Italy, Latvia, Lithuania, Luxembourg, Malta, the Netherlands, Norway, Poland, Portugal, Romania, Slovakia, Slovenia, Spain, Sweden, Switzerland and the United Kingdom.

**CENELEC**

European Committee for Electrotechnical Standardization  
Comité Européen de Normalisation Electrotechnique  
Europäisches Komitee für Elektrotechnische Normung

**Central Secretariat: rue de Stassart 35, B - 1050 Brussels**

## Foreword

The text of document 51/848/FDIS, future edition 3 of IEC 60205, prepared by IEC TC 51, Magnetic components and ferrite materials, was submitted to the IEC-CENELEC parallel vote and was approved by CENELEC as EN 60205 on 2006-05-01.

This European Standard supersedes EN 60205:2001.

This European Standard includes the following significant technical changes with respect to EN 60205:2001:

- a) unit of angles through the text are described by using “radian”;
- b) new words are added in 2.1 “All angles are in radians”;
- c) replacement, in 3.9, of the equation  $\frac{l_2}{A_2} = \frac{\ln d_2 g / d_3}{D\pi(h_1 - h_2)}$  by  $\frac{l_2}{A_2} = \frac{\ln d_2 g / d_3}{D\pi(h_1 - h_2)/2}$ ;
- d) new cores “EL, ER, PQ, EFD and E planar” are added in this edition.

The following dates were fixed:

- latest date by which the EN has to be implemented at national level by publication of an identical national standard or by endorsement (dop) 2007-02-01
- latest date by which the national standards conflicting with the EN have to be withdrawn (dow) 2009-05-01

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**Endorsement notice**

The text of the International Standard IEC 60205:2006 was approved by CENELEC as a European Standard without any modification.

# INTERNATIONAL STANDARD

# IEC 60205

Third edition  
2006-04

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## Calculation of the effective parameters of magnetic piece parts

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International Electrotechnical Commission  
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## INTERNATIONAL ELECTROTECHNICAL COMMISSION

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**CALCULATION OF THE EFFECTIVE PARAMETERS  
OF MAGNETIC PIECE PARTS**
**FOREWORD**

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International Standard IEC 60205 has been prepared by IEC technical committee 51: Magnetic components and ferrite materials.

This third edition cancels and replaces the second edition published in 2001, corrigendum 1 (2001). This edition constitutes a technical revision.

This edition includes the following significant technical changes with respect to the previous edition:

- a) unit of angles through the text are described by using "radian";
- b) new words are added in 2.1 "All angles are in radians";
- c) replacement, Clause 3.9, of the equation  $\frac{l_2}{A_2} = \frac{\ln d_2 g / d_3}{D\pi(h_1 - h_2)}$  by  $\frac{l_2}{A_2} = \frac{\ln d_2 g / d_3}{D\pi(h_1 - h_2) / 2}$ ;
- d) new cores "EL, ER, PQ, EFD and E planar" are added in this edition.

The text of this standard is based on the following documents:

FDIS	Report on voting
51/848/FDIS	51/857/RVD

Full information on the voting for the approval of this standard can be found in the report on voting indicated in the above table.

This publication has been drafted in accordance with the ISO/IEC Directives, Part 2.

The committee has decided that the contents of this publication will remain unchanged until the maintenance result date indicated on the IEC web site under "<http://webstore.iec.ch>" in the data related to the specific publication. At this date, the publication will be

- reconfirmed;
- withdrawn;
- replaced by a revised edition, or
- amended.

A bilingual version of this publication may be issued at a later date.

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## CALCULATION OF THE EFFECTIVE PARAMETERS OF MAGNETIC PIECE PARTS

### 1 Scope

This International Standard lays down uniform rules for the calculation of the effective parameters of closed circuits of ferromagnetic material.

### 2 Basic rules

The following basic rules are applicable to this standard.

**2.1** All results shall be expressed in units based on the millimetre, shall be accurate to three significant figures, but to derive  $l_e$ ,  $A_e$ , and  $V_e$  the values of  $C_1$  and  $C_2$  shall be calculated to five significant figures. All angles are in radians.

NOTE The purpose of specifying this degree of accuracy is only to ensure that parameters calculated at different establishments are identical and it is not intended to imply that the parameters are capable of being determined to this accuracy.

**2.2**  $A_{\min}$  is the nominal value of the smallest cross-section. All the dimensions used to calculate  $A_{\min}$  shall be the mean values between the tolerance limits quoted on the appropriate piece part drawing.

**2.3** Calculations are only applicable to the component parts of a closed magnetic circuit.

**2.4** All dimensions used for the purpose of calculations shall be the mean value within the tolerance limits quoted on the appropriate piece part drawing.

**2.5** All irregularities in the outline of the core, such as small cut-outs, notches, chamfers, etc. shall be ignored unless otherwise described.

**2.6** When the calculation involves the sharp corner of a piece part, then the mean length of flux path for that corner shall be taken as the mean circular path joining the centres of area of the two adjacent uniform sections, and the cross-sectional area associated with that length shall be taken as the average area of the two adjacent uniform sections.

Calculation of effective parameters  $l_e$ ,  $A_e$  and  $V_e$ .

The effective parameters can be defined as

$$l_e = C_1^2 / C_2 \quad A_e = C_1 / C_2 \quad V_e = l_e A_e = C_1^3 / C_2^2$$

where

$l_e$  is the effective magnetic length of the core (mm);

$A_e$  is the effective cross-sectional area (mm<sup>2</sup>);

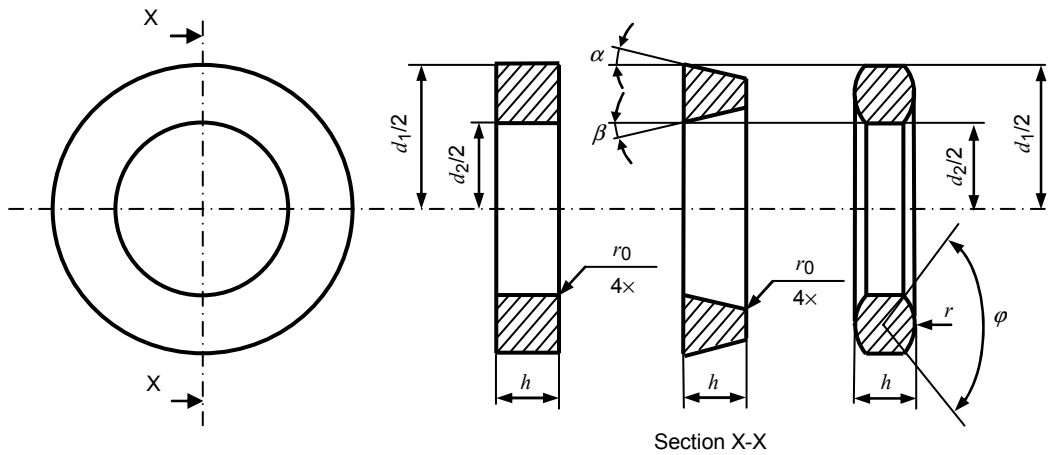
$V_e$  is the effective volume (mm<sup>3</sup>);

$C_1$  is the core constant (mm<sup>-1</sup>);

$C_2$  is the core constant (mm<sup>-3</sup>).

### 3 Formulae for the various types of cores

#### 3.1 Ring cores



IEC 584/06

$$C_1 = \frac{2\pi}{h_e \ln(d_1/d_2)}$$

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$$C_2 = \frac{4\pi(1/d_2 - 1/d_1)}{h_e^2 \ln^3(d_1/d_2)}$$

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##### 3.1.1 For ring cores of rectangular cross-section with sharp corners

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$$h_e = h$$

##### 3.1.2 For ring cores of rectangular cross-section with an appreciable average rounding radius $r_0$

$$h_e = h(1 - k_1) \quad k_1 = \frac{1,7168r_0^2}{h(d_1 - d_2)}$$

##### 3.1.3 For ring cores of trapezoidal cross-section with sharp corners

$$h_e = h(1 - k_2) \quad k_2 = \frac{h(\tan \alpha + \tan \beta)}{d_1 - d_2}$$

##### 3.1.4 For ring cores of trapezoidal cross-section with an appreciable average rounding radius $r_0$

$$h_e = (1 - k_1 - k_2)$$

##### 3.1.5 For ring cores of cross-section with circular arc frontal sides

$$h_e = h - \frac{d_1 - d_2}{4 \sin^2(\varphi/2)} \left( 2 \sin \frac{\varphi}{2} - \frac{\sin \varphi}{2} - \frac{\varphi}{2} \right)$$

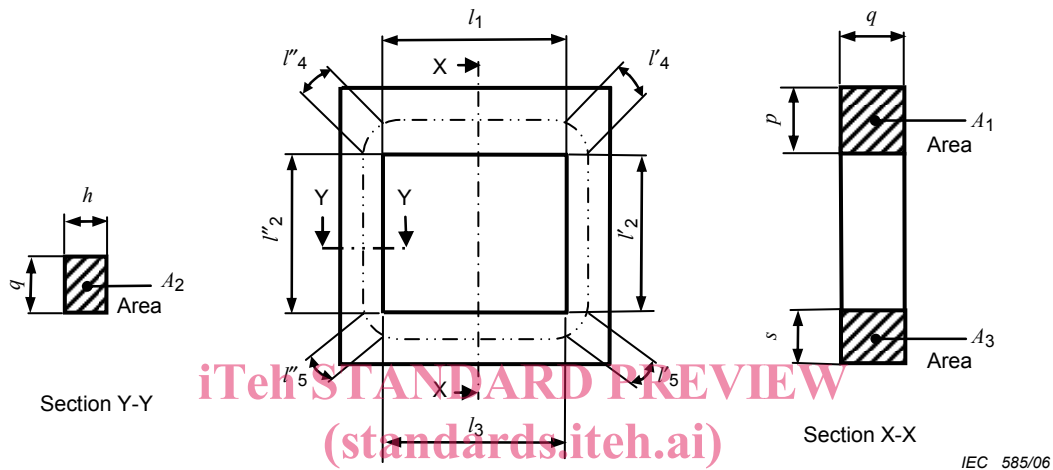
$$\varphi = 2 \arcsin \frac{d_1 - d_2}{4r}$$

NOTE When the winding is uniformly distributed over a ring core, it may be expected that, at all points inside the ring core, the flux lines will be parallel to its surface.

No leakage flux will therefore leave or enter the ring core. This justifies the use of a theoretically more correct derivation of the effective parameters which does not make use of the assumption that the flux is uniformly distributed over the cross-section.

### 3.2 Pair of U-cores of rectangular section

NOTE U + PLT (Plate)-cores use U core formulas



IEC 585/06

Length of flux path associated with area  $A_2$ :  
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 $l_2 = l'_2 + l''_2$

Mean length of flux paths at corners:

$$l_4 = l'_4 + l''_4 = \frac{\pi}{4}(p + h)$$

$$l_5 = l'_5 + l''_5 = \frac{\pi}{4}(s + h)$$

Mean areas associated with  $l_4$  and  $l_5$ :

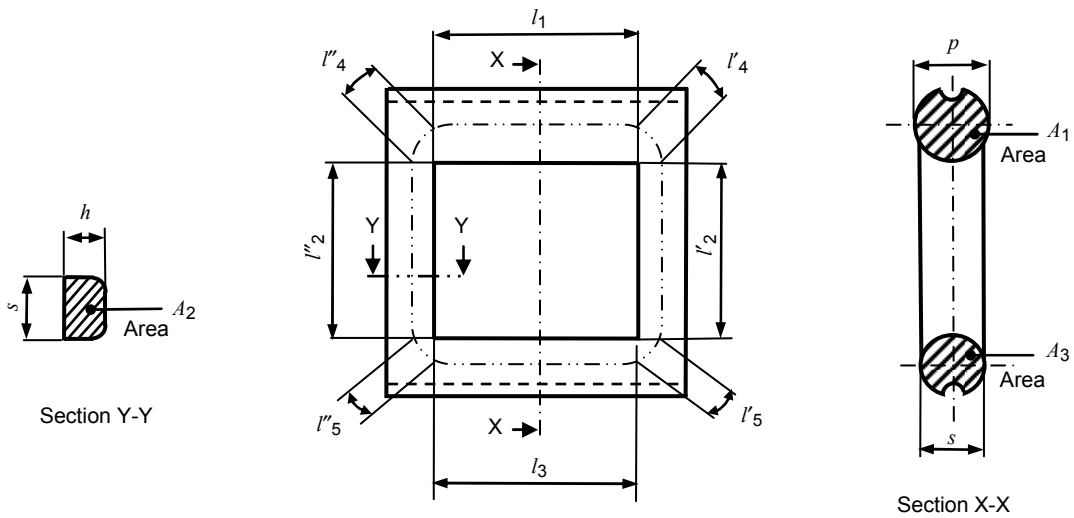
$$A_4 = \frac{A_1 + A_2}{2}$$

$$A_5 = \frac{A_2 + A_3}{2}$$

$$C_1 = \sum_{i=1}^5 \frac{l_i}{A_i} \quad C_2 = \sum_{i=1}^5 \frac{l_i}{A_i^2}$$

### 3.3 Pair of U-cores of rounded section

NOTE U + PLT (Plate)-cores use U core formulas.



IEC 586/06

In calculating  $A_2$  ignore any ridges introduced for the purpose of facilitating manufacture.

Length of flux path associated with area  $A_2$  :

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 $l_2 = l'_2 + l''_2$   
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Mean length of flux path at corners:

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 $l_4 = l'_4 + l''_4 = \frac{\pi}{4}(p+h)$

$$l_5 = l'_5 + l''_5 = \frac{\pi}{4}(s+h)$$

Mean areas associated with  $l_4$  and  $l_5$  :

$$A_4 = \frac{A_1 + A_2}{2}$$

$$A_5 = \frac{A_2 + A_3}{2}$$

$$C_1 = \sum_{i=1}^5 \frac{l_i}{A_i} \quad C_2 = \sum_{i=1}^5 \frac{l_i}{A_i^2}$$