INTERNATIONAL STANDARD

ISO 9400

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Nickel-based alloys — Determination of resistance to intergranular corrosion

iTeh Salliages à base de nickel R Détermination de la résistance à la corrosion intergranulaire (standards.iteh.ai)

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Foreword

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Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75% of the member bodies casting a vote.

International Standard ISO 9400 was prepared by **Technical Committee** ISO/TC 156, *Corrosion of metals and alloys*.

Annex A of this International Standard is for information4001990

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International Organization for Standardization

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Nickel-based alloys — Determination of resistance to intergranular corrosion

Section 1: General

NOTE 1

ISO 6372-1[2].

1.3 Apparatus

1.1 Scope

This International Standard specifies four methods for determination of the susceptibility of nickelbased alloys to intergranular corrosion.

These methods are for laboratory testing of susceptibility only, and a direct correlation with inter-OS. Extended apparatus is shown in figure 1. The cold-finger type of condenser with standard The cold-finger type of condenser with standard Extended apparatus is shown in figure 1. The cold-finger type of condenser with standard method D. The cold-finger type of condenser with standard method D.

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The methods covered are as follows: 6b4ba4

- Method A: iron(III) sulfate sulfuric acid test (section 2);
- Method B: copper copper-sulfate 16 % sulfuric acid test (section 3);
- **Method C:** hydrochloric acid test (section 4);
- Method D: nitric acid test (section 5);

The appropriate method for use with a given alloy, the selection of sensitizing treatment, and the acceptance criteria to be used in any evaluation have to be agreed between the buyer and seller of the alloy. As a guide, the methods specified in this International Standard should be applicable to those nickel-based alloys used for corrosion service and listed in ISO 6207[1].

1.2 Definition

For the purposes of this International Standard, the following definition applies.

nickel-based alloy: An alloy which includes nickel as the predominant element.

6b4ba4cf0b79/iso-94103.1990Four-bulb Allihn or Soxhlet condenser with 45/50 ground glass joint.

This definition is consistent with that given in

1.3.2 Erlenmeyer flask, capacity 1 dm³, with 45/50 ground glass joint.

NOTE 2 The use of round flasks with a heating jacket is also acceptable.

1.3.3 Glass cradle or other equivalent means of specimen support, such as glass hooks or stirrups. The cradle should have three or four holes in it, to increase circulation of the test solution around the specimen (see figure 1).

1.3.4 Boiling chips to promote uniform boiling and to prevent bumping.

For method A, these boiling chips should be made of pure alundum.

1.3.5 Silicone grease for application to the ground glass joint of the condenser and flask.

A PTFE sleeve for the joint is also acceptable.

1.3.6 Heating device such as an electrically heated hot-plate, for continuous boiling of the test solution.

1.3.7 Analytical balance capable of weighing to at least the nearest 1 mg (if mass loss is to be determined).

1.3.8 Stereoscopic microscope capable of magnification of $5 \times$ to $20 \times$, with a good light source, for examination of the tested specimen (for method B).

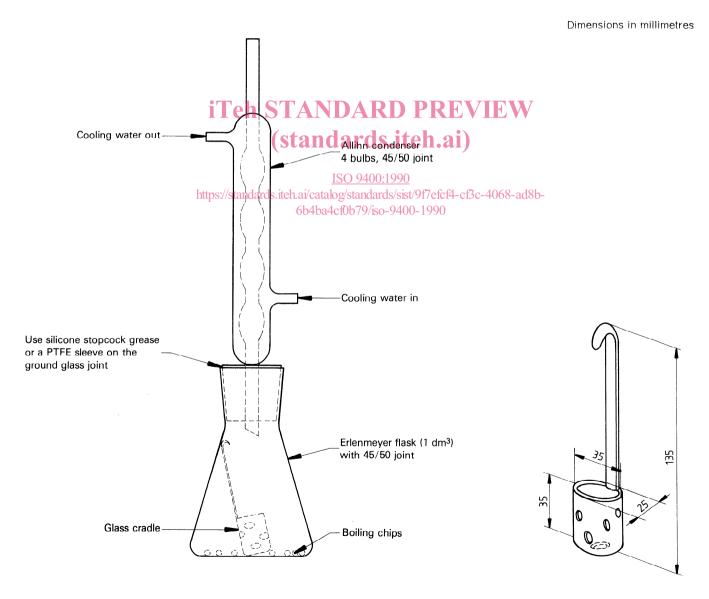
1.4 Preparation of test specimens

The following requirements for the preparation of test specimens are common to all four test methods. Additional requirements are given, where necessary, in the section describing the particular method.

A specimen having a total surface area of 20 cm^2 to 30 cm^2 is recommended. As-welded specimens

should be cut so that no more than a 13 mm width of unaffected base metal is included on either side of the weld and heat-affected zone.

It is intended to test a specimen representing as nearly as possible the surface of the material used in service. Surface finishing should be performed only as required to remove foreign material and obtain a standard, uniform finish to represent the appropriate surface, while maintaining reasonable specimen size for convenience in testing. Normally, removal of more material than necessary will have little influence on the test results. However, in the special case of surface carburization (sometimes encountered, for instance, in tubing when carbonaceous lubricants are employed), it may only be possible to remove the carburized layer completely by heavy grinding or machining. Such treat-



a) Assembled apparatus





ment of non-carburized test specimens is not permissible, except in tests undertaken to demonstrate specific surface effects. When samples are cut by shearing, the deformed metal shall be removed by grinding or machining prior to testing.

Prior to testing, the test specimens shall be degreased with a chlorine-free solvent and rinsed.

1.5 Sensitization of test specimens

1.5.1 Specimens to be given a thermal treatment prior to testing shall be clean of carbonaceous material prior to the thermal treatment. Otherwise, carburization may invalidate the test results. A light surface grinding or pickling followed by washing and rinsing in a non-chlorinated solvent should provide a clean surface. It is recommended that the effect

of the pickling bath on the specimen be tested prior to the environmental exposure.

1.5.2 Specimens of alloys to be given a sensitization treatment prior to testing shall be placed in a furnace at the required temperature and for the required time, and shall then be water quenched. The use of a sensitization treatment shall be agreed upon between buyer and seller.

1.5.3 Specimens of alloys that are not given a sensitization treatment shall be tested in a condition simulating end-use conditions. Specimens from material that is intended to be welded or heat treated shall be welded or heat treated in nearly the same manner as the material will experience in fabrication or service. The specific treatment shall be agreed upon between buyer and seller.

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Section 2: Method A — Iron(III) sulfate — Sulfuric acid test

Scope 2.1

This section describes the procedure for conducting the boiling iron(III) sulfate - sulfuric acid test to determine the susceptibility of nickel-based alloys to intergranular attack.

2.2 Iron(III) sulfate - sulfuric acid test solution

Prepare 600 cm³ of test solution as follows.

Measure 400 cm³ of distilled water into a 500 cm³ araduated cylinder and pour into the Erlenmeyer flask (1.3.2).

Measure 236 cm³ of reagent grade 95 to 98 % (m/m) sulfuric acid into a 250 cm³ graduated cylinder. Add the acid slowly to the water in the Erlenmeyer flask to avoid boiling by the heat evolved. (Loss of vapour results in an increase in the acid concentration.) i'l'eh S'l'Al

Weigh 25 g of reagent grade iron(III) sulfate nonahydrate [$Fe_2(SO_4)_3.9H_2O$, containing about ar 75 % $Fe_2(SO_4)_3$], and add it to the sulfuric acid solution. A trip balance may be used.

ISO 9400: No changes in the test solution are necessary during

Drop several boiling chips (1.3.4) into the flask 654/1614 (1.5.4) boiling chips (1.3.4) into the flask 654/1614 (1.5.4) boltone flask 654/1614 (1.5.4) bol

Lubricate the ground glass joint with silicone grease (1.3.5)

Fit the flask to the condenser (1.3.1) and circulate cooling water.

Boil the solution until all the iron(III) sulfate is dissolved.

Preparation of test specimens 2.3

See clause 1.4.

2.4 Procedure

Measure the dimensions of the specimen to the nearest 0,5 mm, including the inner dimensions of any holes, and calculate the total exposed surface area.

Degrease the specimen using a non-chlorinated solvent, dry and then weigh to the nearest 1 mg.

Place the specimen in a glass cradle (1.3.3) and immerse it in boiling test solution (clause 2.2).

Testing of a single specimen in a flask is preferred. However, several specimens may be tested simultaneously. The number is limited only by the number of glass cradles that can be fitted into the flask (usually three or four). In no case shall different allovs be tested together. Each specimen shall be in a separate cradle so that the specimens do not touch

Mark the liquid level on the flask with a heatresistant marker to provide a check on vapour loss. If there is an appreciable change in the level, repeat the test with fresh solution and a new specimen.

Continue immersion of the specimen for a period of 24 h or 120 h, then remove the specimen, rinse in water and acetone, and dry. For alloys containing less than 18 % chromium the exposure time is typically 24 h. For alloys containing more than 18 % chromium the exposure time is 120 h.

Weigh the specimen and subtract the mass from the original mass.

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3 No intermediate weighings are usually necessary. The tests can be run without interruption; however, if prelimi-nary results are desired, the specimen can be removed at any time for weighing.

5 Additional iron(III) sulfate inhibitor may have to be

added during the test if the corrosion rate is unusually high, as evidenced by a change in the colour of the solution. More iron(III) sulfate has to be added if the total mass loss of all specimens exceeds 2 g [during the test, iron(III) sulfate is consumed at a rate of approximately 10 g for each 1 g of dissolved metal].

6 During testing, there is some deposition of iron oxides on the upper part of the Erlenmeyer flask. This can be readily removed, after completion of the test, by boiling a 10 % (m/m) solution of hydrochloric acid in the flask.

2.5 **Evaluation**

2.5.1 The effect of the test solution on the material can be measured by determining the loss of mass of the specimen. Calculate the corrosion rate as follows:

corrosion rate =
$$\frac{k \times \Delta m}{A \times t \times \rho}$$

where

k is a constant (see note 7);

t is the exposure time, in hours;

- *A* is the exposed area, in square centimetres, of the specimen;
- Δm is the mass loss, in grams;
- ho is the density, in grams per cubic centimetre, of the specimen.

NOTE 7 Using the above units for t, A, Δm and ρ , the corrosion rate can be calculated in a variety of units using the appropriate value of k:

Value of k to be used
3,45 × 10 ⁶
3,45 × 10 ³
$2,85 \times 10^2$
8,76 × 10 ⁴

micrometres per year	· (μm/	'y)	8,76 ×	107
				-

picometres per second (pm/s) $2,78 \times 10^6$

2.5.2 The presence of intergranular attack is usually determined by comparing the calculated corrosion rate to that for properly annealed material. Even in the absence of intergranular attack, the rate of general or grain-face corrosion of properly annealed material will vary from one alloy to another. The corrosion rate considered acceptable shall be determined between buyer and seller.

2.5.3 As an alternative or in addition to calculating a corrosion rate from mass loss data, metallographic examination may be used to evaluate the degree of intergranular attack. The depth of attack considered acceptable shall be determined between buyer and seller.

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Section 3: Method B — Copper — Copper sulfate — 16 % sulfuric acid test

3.1 Scope

3.1.1 This section describes the procedure for conducting the copper – copper sulfate – 16 % sulfuric acid test to determine the susceptibility of certain nickel-based alloys to intergranular attack. This test detects susceptibility to intergranular attack associated with the precipitation of chromium carbides or nitrides.

3.1.2 This test may be used to evaluate the heat treatment accorded to as-received material. It may also be used to evaluate the effectiveness of stabilizing element additions (Nb, Ti, etc.) and reduction in interstitial content to aid in resistance to intergranular attack. It may be applied to all wrought products and weld metal.

3.1.3 This test does not detect susceptibility associated with chi-phase, sigma-phase, or titanium carbides or nitrides. For detecting susceptibility in environments known to cause intergranular attack and due to these phases use method D.

3.5 Procedure

The volume of test solution (clause 3.2) used shall be sufficient to completely immerse the specimen(s) and provide a minimum ratio of solution volume to total specimen surface area of $8 \text{ cm}^3/\text{cm}^2$.

As many as three specimens can be tested in the same flask, provided that all of the specimens are of the same grade and that the ratio of solution volume to total specimen surface area is maintained.

The specimen(s) shall be immersed in the test solution. A sufficient quantity of copper shot or turnings (clause 3.3) shall be used to cover all surfaces of the specimen, whether it is in a vented cradle or embedded in a layer of copper shot or turnings on the bottom of the flask. The amount of copper used, provided that an excess of metallic copper is present, is not critical.

Heat the solution to boiling and maintain boiling throughout the test period. Begin timing the test period when the solution reaches the boiling point. Mark the liquid level on the flask with a heatresistant marker to provide a check on vapour loss. If there is an appreciable change in the level, repeat ISO 94the test with fresh solution and a new specimen.

3.2 Acidified copper sulfate test solution by the solution we have a should be the solution be the solution we have a should be the solution of the solution we have a should be the solution we have a should be the solution we have a should be the solution we have a solution we have a should be the solution of the solution we have a soli

Dissolve 100 g of copper(II) sulfate pentahydrate $(CuSO_4.5H_2O)$ in 700 cm³ of distilled water, add 100 cm³ of sulfuric acid $(H_2SO_4$, reagent grade ρ 1,84 g/cm³), and dilute to 1000 cm³ with distilled water. The solution will contain approximately 6 % (m/m) of anhydrous copper(II) sulfate $(CuSO_4)$ and 16 % (m/m) of H_2SO_4 .

3.3 Copper

Electrolytic grade copper shot or turnings may be used. Shot is preferred for its ease of handling before and after the test.

The copper shot or turnings may be reused if cleaned in warm water after each test.

3.4 Preparation of test specimens

See clause 1.4

Since the evaluation is done by bending, the shape of the test specimen shall be such as to allow bending to be accomplished with the original surface on the outside of the bend.

The test shall consist of a 24 h period. However, longer periods may be employed, in which case the exposure time shall be included in the test report. Fresh test solution is not needed for test periods up to 72 h. (If any adherent copper remains on the specimen, it may be removed by a brief immersion in concentrated nitric acid at room temperature. The sample is then rinsed in water and dried.)

3.6 Evaluation

3.6.1 The specimen shall be bent through 180° over a radius equal to twice the thickness of the specimen. In no case shall the specimen be bent over a smaller radius or through a greater angle than that specified in the product specification. In cases of material having low ductility, such as severely cold-worked material, a 180° bend may prove impractical. Determine the maximum angle of bend without causing cracks in such material by bending an untested specimen of the same configuration as the specimen to be tested.

Welded samples shall be bent in such a manner that the weld and heat-affected zone are strained.

Samples machined from thick sections shall have the original surface on the outside of the bend.

3.6.2 In the case of tubes up to 40 mm in outside diameter, the specimen shall be flattened. The distance between the platens after flattening, measured under load, shall not be greater than the following value, h, in millimetres:

$$h = \frac{1,09D\delta}{0,09D + \delta}$$

where

- δ is the specified wall thickness, in millimetres;
- *D* is the outside diameter of the tube, in millimetres.

In the case of welded tube, the weld shall be at the point of maximum flattening.

3.6.3 The bent or flattened specimen shall be examined using a stereoscopic microscope (1.3.8). The appearance of fissures or cracks indicates the presence of intergranular attack. Cracking that originates at the edge of the specimen should be disregarded. The appearance of deformation without accompanying cracks or fissures should also be disregarded.

3.6.4 When an evaluation is questionable or as an alternative to 3.6.3, the presence or absence of intergranular attack shall be determined by metallographic examination of the specimen.

NOTE 9 Cracks suspected of arising through poor ductility may be investigated by bending a similar specimen which was not exposed to the boiling test solution. A visual comparison between the exposed and unexposed specimens should assist in interpretation.

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