

# INTERNATIONAL STANDARD

# NORME INTERNATIONALE



**Photovoltaic devices –**  
**Part 5: Determination of the equivalent cell temperature (ECT) of photovoltaic (PV) devices by the open-circuit voltage method**

**Dispositifs photovoltaïques –**  
**Partie 5: Détermination de la température de cellule équivalente (ECT) des dispositifs photovoltaïques (PV) par la méthode de la tension en circuit ouvert**



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### PHOTOVOLTAIC DEVICES –

#### **Part 5: Determination of the equivalent cell temperature (ECT) of photovoltaic (PV) devices by the open-circuit voltage method**

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**IEC 60904-5 edition 2.1 contains the second edition (2011-02) [documents 82/595/CDV and 82/626/RVC] and its amendment 1 (2022-11) [documents 82/2069/FDIS and 82/2082/RVD].**

**In this Redline version, a vertical line in the margin shows where the technical content is modified by amendment 1. Additions are in green text, deletions are in strikethrough red text. A separate Final version with all changes accepted is available in this publication.**

International Standard IEC 60904-5 has been prepared by IEC technical committee 82: Solar photovoltaic energy systems.

This second edition constitutes a technical revision.

The main technical changes with regard to the previous edition are as follows:

- added and updated normative references;
- added reporting section;
- added method on how to extract the input parameters;
- rewritten method on how to calculate ECT;
- reworked formulae to be in line with IEC 60891.

A list of all parts of IEC 60904 series, under the general title *Photovoltaic devices*, can be found on the IEC website.

This publication has been drafted in accordance with the ISO/IEC Directives, Part 2.

The committee has decided that the contents of the base publication and its amendment will remain unchanged until the stability date indicated on the IEC web site under [webstore.iec.ch](http://webstore.iec.ch) in the data related to the specific publication. At this date, the publication will be

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IEC 60904-5:2011

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## INTRODUCTION

When temperature sensors, such as thermocouples, are used to determine the cell temperature of PV devices under natural or simulated steady-state irradiance, two main problems arise. First, a considerable spread of temperature can be observed over the area of the module. Second, as the solar cells are usually not accessible, sensors are attached to the back of the module and the measured temperature thus is influenced by the thermal conductivity of the encapsulant and back materials. These problems are aggravated when determining the equivalent cell temperature for on-site measurements of array performance where all cells have slightly different temperatures and one cannot easily determine the average cell temperature.

The equivalent cell temperature (ECT) is the average temperature at the electronic junctions of the device (cells, modules, arrays of one type of module) which equates to the current operating temperature if the entire device were operating uniformly at this junction temperature.

For modules with large thermal inertia such as glass-glass construction for BIPV applications, measurements become even more challenging with increased temperature difference between the cell and module external temperatures during transient conditions. In addition, for bifacial PV modules the temperature sensors may shade an active cell, potentially even creating local hotspots where sensors are located on effective cell areas.

NOTE 1 NMOT is defined as the equilibrium mean solar cell junction temperature within an open-rack mounted module operating near peak power, in the following standard reference environment:

- Tilt angle:  $(37 \pm 5)^\circ$ .
- Total irradiance:  $800 \text{ W/m}^2$ .
- Ambient temperature:  $20 \text{ }^\circ\text{C}$ .
- Wind speed:  $1 \text{ m/s}$ .
- Electrical load: A resistive load sized such that the module will operate near its maximum power point at STC or an electronic maximum power point tracker (MPPT).

NOTE 2 NMOT is similar to the former NOCT except that it is measured with the module under maximum power rather than in open circuit. Under maximum power conditions (electric) energy is withdrawn from the module, therefore less thermal energy is dissipated throughout the module than under open-circuit conditions. Therefore NMOT is typically a few degrees lower than the former NOCT.

## PHOTOVOLTAIC DEVICES –

### Part 5: Determination of the equivalent cell temperature (ECT) of photovoltaic (PV) devices by the open-circuit voltage method

#### 1 Scope and object

This part of IEC 60904 describes the preferred method for determining the equivalent cell temperature (ECT) of PV devices (cells, modules and arrays of one type of module), for the purposes of comparing their thermal characteristics, determining NOCT (nominal operating cell temperature) or alternatively NMOT (nominal module operating temperature), and translating measured I-V characteristics to other temperatures.

This standard applies to linear devices with logarithmic  $V_{OC}$  dependence on irradiance and in stable conditions. It may be used for all technologies but one has to verify that there is no preconditioning effect influencing the measurement.

#### 2 Normative references

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

IEC 60891, *Photovoltaic devices – Procedures for temperature and irradiance corrections to measured I-V characteristics*

IEC 60904-1, *Photovoltaic devices – Part 1: Measurement of photovoltaic current-voltage characteristics*

IEC TS 60904-1-2:2019, *Photovoltaic devices – Part 1-2: Measurement of current-voltage characteristics of bifacial photovoltaic (PV) devices*

IEC 60904-2, *Photovoltaic devices – Part 2: Requirements for reference solar devices*

IEC 60904-3, *Photovoltaic devices – Part 3: Measurement principles for terrestrial photovoltaic (PV) solar devices with reference spectral irradiance data*

IEC 60904-7, *Photovoltaic devices – Part 7: Computation of the spectral mismatch correction for measurements of photovoltaic devices*

IEC 60904-10, *Photovoltaic devices – Part 10: Methods of linearity measurement*

IEC 61215, *Crystalline silicon terrestrial photovoltaic (PV) modules – Design qualification and type approval*

IEC 61829, *Crystalline silicon photovoltaic (PV) array – On-site measurement of I-V characteristics*

~~ISO/IEC 17025, General requirements for competence of testing and calibration laboratories~~

### 3 Measurement principle and requirements

#### 3.1 Principle

~~The method described below is based on the fact that the open-circuit voltage ( $V_{OC}$ ) of a solar cell changes with temperature in a predictable fashion. If the open-circuit voltage of the device at standard test conditions is known, together with its temperature coefficient, the equivalent temperature of all the cells in the device can be determined. The open-circuit voltage is also slightly affected by the irradiance, so an additional correction may be required as outlined in IEC 60891.~~ Experience shows that the equivalent cell temperature can be determined more precisely by the method described herein than by any alternative technique [1]<sup>1</sup>. However, ~~as the temperature coefficient  $\beta$  drops rapidly~~ increased variability and errors have been observed at irradiances below ~~200~~ 400 W/m<sup>2</sup>, so this method should only be used at irradiances above this threshold.

#### 3.2 General measurement requirements

a) Use of the ECT method requires calibration of the device to be measured.

NOTE It is not sufficient to use calibration of another device of the same type, because even small differences in parameters between a calibrated device and a similar one can lead to significant errors (e.g. 0,3 % variation in module  $V_{OC}$  leads to 1 °C impact on ECT temperature).

ab) The device under test needs to match the following criteria:

- 1) The variation of  $V_{OC}$  needs to be linear as defined in IEC 60904-10 with respect to temperature.
- 2) The variation of  $V_{OC}$  with respect to irradiance needs to ~~follow a logarithmic dependence with irradiance~~ have a quadratic dependence on the logarithm of irradiance.
- 3) ~~It needs to have an ohmic series resistance as otherwise there will be different ECT-coefficients for different temperature regions.~~
- 4) ~~The shunt resistances of the device need to be reasonably high, as for the majority of commercially available devices, as otherwise there will be different ECT-coefficients for different temperature regions.~~

bc) The irradiance measurements shall be made using a PV reference device packaged and calibrated in conformance with IEC 60904-2 or a pyranometer. ~~The PV reference device shall either be spectrally matched to the test specimen, or a spectral mismatch correction shall be performed~~ Either use a PV reference device that is spectrally matched to the device under test (DUT), or perform a spectral mismatch correction and report in conformance with IEC 60904-7. The reference device shall be linear in short-circuit current as defined in IEC 60904-10 over the irradiance range of interest.

In accordance with IEC 60904-2, to be considered spectrally matched, a reference device shall be constructed using the same cell technology and encapsulation package as the ~~test device under test. Otherwise the spectral mismatch will have to be reported.~~

NOTE Some devices might have a significant spectral dependency in the open-circuit voltage. In such a case, a spectroradiometer would be needed to ensure stable incident spectrum.

d) Some devices, in particular multi-junction, might have a spectral dependency of the open-circuit voltage [2]. For these devices, the spectral irradiance shall be determined with a spectroradiometer.

ee) The active surface of the ~~specimen~~ device under test shall be coplanar within  $\pm 2^\circ$  of the active surface of the reference device.

df) ~~Voltages shall be measured to an accuracy of  $\pm 0,2\%$  of the open-circuit voltage using independent leads from the terminals of the specimen and keeping them as short as possible. The measurement ranges of the data acquisition should be carefully chosen. If the test specimen is a module, the 4-wire connection should start at the terminals or connectors. If the test specimen is a cell, the 4-wire connection should start at the bus~~

<sup>1</sup> Numbers in square brackets refer to the Bibliography.

~~bars.~~ For appropriate connection method and measurement of voltages refer to IEC 60904-1.

## 4 Apparatus

In addition to the general measurement requirements of Clause 3 the following equipment is required to perform I-V characteristic measurements:

- a) A PV reference device that meets the conditions stated in 3 ac).
- b) Equipment to measure the open-circuit voltage to an ~~precision~~ instrumental measurement uncertainty better than  $\pm 0,2$  %.
- c) Equipment to measure temperature to an ~~precision~~ instrumental measurement uncertainty of  $\pm 1$  K.

## 5 Determination of required input parameters

The procedure requires a number of input parameters. These are:

- ~~• Temperature coefficient of the open circuit voltage,  $\beta$ . This shall be determined from cell or module measurements of representative samples in accordance with IEC 60891.~~
- ~~• Open circuit voltage ( $V_{OC1}$ ) at a reference condition ( $G_1, T_1$ ) in accordance with IEC 60904-1 for a cell or module or in accordance with IEC 61829 for a PV array. The reference condition is often chosen to be the standard test conditions as defined in IEC 61215, i.e.  $G_{STC} = 1\,000$  W/m<sup>2</sup> and  $T_{STC} = 25$  °C.~~
- ~~• The procedure requires a constant,  $a$ , which is also interpreted as the thermal diode voltage. The determination of this requires the measurement of the open circuit voltage at two different irradiance levels  $G_3$  and  $G_4$ , one of which may be the point  $G_1, T_1$ .~~
- Relative temperature coefficient of open circuit voltage,  $\beta_{rel}$ . This shall be determined from cell or module measurements of representative samples in accordance with IEC 60891.

For bifacial modules, the temperature coefficient only needs to be determined from front side measurements.

- Open-circuit voltage ( $V_{OC1}$ ) at a reference condition ( $G_1, T_1$ ) in accordance with IEC 60904-1 or IEC TS 60904-1-2 for a cell or module or in accordance with IEC 61829 for a PV array. The reference condition is often chosen to be the standard test conditions, i.e.  $G_{STC} = 1\,000$  W/m<sup>2</sup> and  $T_{STC} = 25$  °C with a reference spectral irradiance distribution as defined in IEC 60904-3.
- When outdoor measurement ( $G_1, T_1$ ) is carried out, it is recommended to apply insulating thermal tape, e.g. polyethylene foam, 1 mm thickness, with mass density less than 0,03 g/cm<sup>3</sup>, to cover the temperature sensor which is fixed by either aluminium or polyimide tape. If the temperature around the module is subjected to spatial and temporal variability, use of insulating thermal tape shields the temperature sensor from influence of environmental factors such as wind, allowing more accurate measurements.

NOTE A method to determine the mass density can be found in ISO 7214[4].

- The procedure requires the irradiance correction factors,  $B_1$  and  $B_2$ .  $B_1$  is linked to the thermal diode voltage and  $B_2$  accounts for non-linearity of  $V_{OC}$  with irradiance scaling. The determination of these constants requires the measurement of the module I-V characteristic in accordance with IEC 60891 under at least five different irradiance levels.

## 6 Procedure

### 6.1 General

The procedure can be carried out either in a controlled environment or by taking measurements at arbitrary irradiances and correcting to the reference irradiance  $G_1$ .

## 6.2 Operating in a controlled environment

- a) Mount the radiation sensor coplanar with the test device to an agreement better than  $\pm 2^\circ$ .
- b) Set the irradiance to be equal to that of the reference condition  $G_1$  using the reference device.
- c) For bifacial modules, a non-irradiated background is required as described in IEC TS 60904-1-2.
- d) Take simultaneous readings of the open-circuit voltage of the ~~test~~ device under test  $V_{OC2}$  and the incident irradiance ( $G_2$ ). Should there be any variation in the irradiance, treat as a measurement in arbitrary irradiance conditions as given in 6.3 and carry out the appropriate correction. An irradiance correction should be carried out if the scatter in the determined ECT is more than 1 K.
- e) Calculate the ECT as described in Clause 7.

## 6.3 Taking measurements under arbitrary irradiance conditions

- a) Mount the radiation sensor coplanar with the ~~test~~ device under test to an agreement better than  $\pm 2^\circ$ .
- b) For bifacial modules, two different setups are recommended for the measurement:

Method 1: use a low reflectivity black cover material to reduce back-to-front irradiance ratio to  $< 1\%$ , in order to minimize the rear irradiance contribution. The cover should be mounted behind the module in a way to limit interference with the module natural convective heat dissipation as much as possible.

Method 2: measure the plane-of-array irradiance on front side  $G_{f_i}$  and the average irradiance on the rear side  $G_{r_i}$  using PV reference devices compliant to IEC 60904-2.  $G_{r_i}$  is the average of at least 5 measurement points located per the requirements of IEC TS 60904-1-2:2019, 6.3.2. The equivalent irradiance  $G_E$  on the bifacial module is then determined by:

$$G_{E_i} = G_{f_i} + \varphi \times G_{r_i} \quad (1)$$

where  $\varphi$  is the module bifaciality coefficient as determined in accordance with IEC TS 60904-1-2.

NOTE 1 Decision on which method to use is left to the user, on consideration of the targeted measurement uncertainty budget. Method 1 is expected to enable lower uncertainty when applied to NOCT or NMOT measurements, and for translating field measured I-V characteristics to standard test conditions.

NOTE 2 When applying method 2, particularly for bifacial systems, proper selection of the modules to be tested has to consider thermal and irradiance non-uniformities at the system level. IEC 61829 provides some guidance on the selection of typical modules within a PV array, recommending in particular to avoid selecting modules at ends of rows.

- b)c) Take simultaneous readings of the open-circuit voltage of the ~~test~~ device under test  $V_{OC2}$  and the incident plane-of-array irradiance  $G_2$  (method 1), or alternatively of the irradiance on front side  $G_{f_2}$  and average irradiance on the rear side  $G_{r_2}$  (method 2).
- d) Carry out a correction of  $V_{OC2}$  to an irradiance equal to  $G_1$ .
- e) Calculate the ECT as described in Clause 7.

## 7 Calculation of equivalent cell temperature

The equivalent cell temperature ECT is derived from the single diode equations describing the current voltage characteristic.

~~Solving the equation for  $V_2 = V_{OC2}$ , with  $V_1 = V_{OC1}$  and  $I_2 = I_1 = 0$  results in the following dependence of the open circuit voltage:~~

$$V_{OC2} = V_{OC1} + V_{OC1} \left[ \beta(T_2 - T_1) + a \ln \frac{G_2}{G_1} \right] \quad (1)$$

where

$V_{OC1}$  is the open-circuit voltage measured in Clause 5 at the irradiance  $G_1$  and module temperature  $T_1$ ;

$V_{OC2}$  is the open-circuit voltage measured in Clause 6 at irradiance  $G_2$  and module temperature  $T_2$ ;

the temperature coefficient of the open-circuit voltage  $\beta$  has also been measured as part of Clause 5 in accordance with IEC 60891;

the parameter,  $a$ , is the thermal diode voltage, which can be determined from measurements at different light intensities but identical temperatures as:

$$a = \frac{V_{OC4} - V_{OC3}}{V_{OC3} \ln(G_4/G_3)} \quad (2)$$

where  $V_{OC3}$  and  $V_{OC4}$  are the voltages measured in Clause 5 at the same module temperatures but at different irradiances  $G_3$  and  $G_4$ , respectively.

Instead of the irradiances  $G_1$  and  $G_2$ , one can also use the ratio of short circuit currents, which then is called self-reference. This requires short circuit current to be linear according to IEC 60904-10. This simplifies the measurements to be taken significantly as one essentially eliminates the requirement for measuring the irradiance and the dependence on the spectrally matched devices.

The relation between the different values of  $V_{OC}$  can then be rewritten to calculate the equivalent ECT as:

$$ECT = T_2 = T_1 + \frac{1}{\beta} \left[ \frac{V_{OC2}}{V_{OC1}} - 1 - a \ln \left( \frac{G_2}{G_1} \right) \right] \quad (3)$$

NOTE This assumes that the spatial and thermal non-uniformity between the two  $V_{OC}$  is identical. For non-uniform temperature or illumination there will be a small error in ECT because the equivalent circuit model assumes uniform temperature and illumination.

In the case of base measurements described in Clause 5 being taken at standard test conditions, the ECT can be determined as:

$$ECT = 25^\circ\text{C} + \frac{1}{\beta} \left[ \frac{V_{OC2}}{V_{OC,STC}} - 1 - a \ln \left( \frac{G_2}{1\,000} \right) \right] \quad (4)$$

This equation is closely related to the formulation of method 1 in the standard for temperature and irradiance corrections (IEC 60891). The factor  $a$  is linked to the number of cells (junctions) in series in the module ( $n_s$ ) as well as the thermal voltage  $D$  as defined in IEC 60891. Thus one can write the ECT in terms of this standard as:

$$ECT = T_2 = T_1 + \beta^{-1} \left[ \frac{V_{OC2}}{V_{OC1}} - 1 + D \times n_s \times \ln \left( \frac{G_2}{G_1} \right) \right] \quad (5)$$

Solving the equation for  $V_2 = V_{OC2}$ , with  $V_1 = V_{OC1}$  and  $I_2 = I_1 = 0$  results in the

following dependence of the open circuit voltage:

$$f(G_1, G_2) = 1 + B_1 \times \ln \frac{G_1}{G_2} + B_2 \times \ln^2 \left( \frac{G_1}{G_2} \right)$$

$$V_{oc2} = \frac{V_{oc1} \times \left[ 1 + \beta_{rel} \times (T_2 - T_1) \times f^2(G_1, G_2) \right]}{f(G_1, G_2)}$$

where

$V_{OC1}$  is the open-circuit voltage measured in Clause 5 at the chosen reference conditions, irradiance  $G_1$  and module temperature  $T_1$ ;

$V_{OC2}$  is the open-circuit voltage measured in Clause 6 at irradiance  $G_2$  and module temperature  $T_2$ ;

the relative temperature coefficient of the open-circuit voltage  $\beta_{rel}$  and the irradiance correction factors  $B_1$  and  $B_2$  are determined in Clause 5.

NOTE These formulae are derived from the IEC 60891 correction procedure 2 [3].

For measurement of bifacial modules using method 2, the irradiance  $G_2$  has to be replaced by the equivalent irradiance  $G_{E2}$ .

$$f(G_1, G_{E2}) = 1 + B_1 \times \ln \frac{G_1}{G_{E2}} + B_2 \times \ln^2 \left( \frac{G_1}{G_{E2}} \right)$$

$$V_{oc2} = \frac{V_{oc1} \times \left[ 1 + \beta_{rel} \times (T_2 - T_1) \times f^2(G_1, G_{E2}) \right]}{f(G_1, G_{E2})}$$

The relation between the different values of  $V_{OC}$  can then be rewritten to calculate the equivalent ECT per the formulas given below, for monofacial (6) and bifacial (7) devices:

$$ECT = T_2 = T_1 + \frac{1}{\beta_{rel} \times f^2(G_1, G_2)} \times \left[ \frac{V_{OC2}}{V_{OC1}} \times f(G_1, G_2) - 1 \right]$$

$$ECT = T_2 = T_1 + \frac{1}{\beta_{rel} \times f^2(G_1, G_{E2})} \times \left[ \frac{V_{OC2}}{V_{OC1}} \times f(G_1, G_{E2}) - 1 \right]$$

In the case of base measurements described in Clause 5 being taken at standard