### TECHNICAL REPORT



First edition 1989-05-01

### Road vehicles – Anthropomorphic side impact dummy –

# iTeh Stateral abdominal impact response requirements to assess biofidelity of dummy (standards.iteh.ai)

Véhicules routiers 790 Manneguin anthropomorphe pour essai de choc latéral https://standards.iPartie 51a Caractéristiques de réponse de l'abdomén à un choc latéral permettant d'évaluer la biofidélité d'un manneguin





Reference number ISO/TR 9790-5 : 1989 (E)

#### Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The main task of ISO technical committees is to prepare International Standards. In exceptional circumstances a technical committee may propose the publication of a technical report of one of the following types:

 type 1, when the necessary support within the technical committee cannot be obtained for the publication of an International Standard, despite repeated efforts;

type 2, when the subject is still under technical development requiring wider exposure;
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- type 3, when a technical committee has collected data of a different kind from that which is normally published as an International Standard ("state of the art", for example).

Technical reports are accepted for publication directly by ISO Council. Technical reports of types 1 and 2 are subject to review within three years of publication, to 2000-4a8c-8d47-decide whether they can be transformed into International Standards. Technical reports of type 3 do not necessarily have to be reviewed until the data they provide are considered to be no longer valid or useful.

ISO/TR 9790-5, which is a technical report of type 3, was prepared by Technical Committee ISO/TC 22, *Road vehicles*.

ISO/TR 9790 consists of the following parts, under the general title *Road vehicles* – *Anthropomorphic side impact dummy*:

 Part 1: Lateral head impact response requirements to assess biofidelity of dummy

- Part 2: Lateral neck impact response requirements to assess biofidelity of dummy

 Part 3: Lateral thoracic impact response requirements to assess biofidelity of dummy

 Part 4: Lateral shoulder impact response requirements to assess biofidelity of dummy

- Part 5: Lateral abdominal impact response requirements to assess biofidelity of dummy

- Part 6: Lateral pelvic impact response requirements to assess biofidelity of dummy

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Printed in Switzerland

## Road vehicles — Anthropomorphic side impact dummy — Part 5 :

Lateral abdominal impact response requirements to assess biofidelity of dummy

1.0 INTRODUCTION

The impact response requirements presented in this Technical Report are the result of a critical evaluation of data selected from experiments agreed to by experts as being the best and most up-to-date information available.

#### 2.0 SCOPE AND FIELD OF APPLICATION iTeh STANDARD PREVIEW

This Technical Report is one **of six reports that des**cribe laboratory test procedures and impact response requirements suitable for assessing the impact biofidelity of side impact of assessing the provides information by to-tassessing the biofidelity of lateral abdominal impact response.

3.0 ISO REFERENCES

ISO DP 9790-1 Road Vehicles - Anthropomorphic Side Impact Dummy -Lateral Head Impact Response Requirements to Assess the Biofidelity of the Dummy.

ISO DP 9790-2 Road Vehicles - Anthropomorphic Side Impact Dummy -Lateral Neck Impact Response Requirements to Assess the Biofidelity of the Dummy.

ISO DP 9790-3 Road Vehicles - Anthropomorphic Side Impact Dummy -Lateral Thoracic Impact Response Requirements to Assess the Biofidelity of the Dummy.

ISO DP 9790-4 Road Vehicles - Anthropomorphic Side Impact Dummy -Lateral Shoulder Impact Response Requirements to Assess the Biofidelity of the Dummy. ISO DP 9790-6 Road Vehicles - Anthropomorphic Side Impact Dummy -Lateral Pelvis Impact Response Requirements to Assess the Biofidelity of the Dummy.

#### 4.0 REQUIREMENT

#### 4.1 Original Data

Researchers of the Association Peugeot-Renault subjected 11 unembalmed cadavers to lateral free falls onto simulated armrests (1)\*. The cadavers were instrumented to monitor accelerations of their 12th thoracic vertebrae and the lateral aspects of their 9th ribs. The simulated armrests were secured to load cells, providing measurements of the force applied to the impacted surface. The actual data traces for these tests were provided by APR (2) and are presented in the Appendix.

## 4.2 Response Requirements (standards.iteh.ai)

#### ISO/TR 9790-5:1989

The original impactntps/esponsetch.cunvleg/standthle/sist/peakafa-thoracsic8d43pine accelerations and peak impacted rib accelerations of the cadaver subjects were normalized using the technique suggested by Mertz (3). (See the Appendix for a description of the normalization process.) The normalized force-time curves of the cadaver subjects and proposed response corridors are shown in Figures 1 and 2 for the 1 and 2 meter free falls onto 4.1 cm rigid armrest, respectively. The normalized force-time curves of the dummy should lie within these corridors when subjected to the 1 and 2 meter impacts described under Test Setup. The normalized peak acceleration of T12 should lie between 29 and 35 G for the 1 meter impact and between 75 and 91 G for the 2 meter impact. The normalized peak impacted rib acceleration should lie between 100 and 125 G for the 1 meter impact and between 160 and 200 G for the 2 meter impact. For both the 1 and 2 meter impacts, the abdominal penetration should be at least 4.1 cm which is the height of the rigid simulated armrest.

\*Numbers in parentheses denote papers listed in References, Section 5.0.



FIGURE 2. NORMALIZED LATERAL ABDOMINAL FORCE-TIME CURVES AND PROPOSED CORRIDOR FOR A 2 METER DROP ONTO A 4.1 CM RIGID ARMREST.

#### 4.3 Test Setup

The simulated armrest is constructed of rigid hardwood. The armrest is 7 cm in width and of sufficient height to protrude 4.1 cm above the surrounding surface. The length must be sufficient to prevent the dummy from striking the ends. The top edges are rounded with a 1 cm radius. The dummy is to be suspended above the impact surface with its midsagittal plane horizontal and its abdominal region including the "area of the 9th rib" in line with the top surface of the simulated armrest. A quick-release mechanism is to be used to drop the dummy the prescribed distance (1 or 2 meters).

#### 4.4 Instrumentation

The dummy should be instrumented to monitor the acceleration of the spine at the level of the 12th thoracic vertebral body and the acceleration of the impacted side rib at the level of the 9th rib. The simulated armrest is to be mounted on a 16ad cell. Load and acceleration measurements are to meet SAE Channel Class 180 filter requirements. High speedtacamenah.acoverage.dais/sirequined20to4adetermine abdominal penetration.

#### 4.5 Normalization Procedure

Determine the impulse and change in velocity by integrating the force-time curve and the T12 acceleration-time curve, respectively. Calculate the effective mass from the following equation.

$$M_{e} = \left[ \int_{0}^{l} Fdt \right] / (Tg + \Delta V)$$
 (1)

The mass ratio is calculated from the following equation,

$$R_{\rm m} = 16.4 \text{ kg/M}_{\rm e}$$
 (2)

It is assumed that the lateral impact dummy has the same abdominal stiffness as the standard subject, and the stiffness ratio,  $R_k$ , is equal to 1.

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The normalizing factors for force, time, and acceleration are given by,

$$R_{f} = (R_{m} R_{k})^{\frac{1}{2}}$$
 (3)

$$R_{t} = (R_{m})^{\frac{1}{2}} (R_{k})^{-\frac{1}{2}}$$
(4)

$$R_{a} = (R_{k})^{\frac{1}{2}} (R_{m})^{-\frac{1}{2}}$$
(5)

Normalize the force-time curve by multiplying each force value by its normalizing factor and each time value by its normalizing value. Normalize the peak spinal acceleration and peak impacted side rib acceleration by multiplying the peak values by the acceleration normalizing factor. Compare the normalized responses to their respective requirements.

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Abdominal penetration is def**ined as the overtical dis**placement of the thoracic spine relative to the armrest measured from the time of first ISO/TR 9790-5:1989 contact of the abdominal sunface with the armrest peafa-20e0-4a8c-8d47-

#### 5.0 REFERENCES

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- 1. Walfisch, G., Fayon, A., Tarriere, C., Rosey, J., Guillon, F., Got, C., Patel, A., and Stalnaker, R., "Designing of a Dummy's Abdomen for Detecting Injuries in Side Impact Collisions", Fifth International Conference on the Biomechanics of Impacts, September, 1980.
- 2. Bendjellal, F., Walfisch, G., Fayon, A., and Tarriere, C., "APR Biomechanical Data," Nanterre, France, Jan., 1984.
- Mertz, H. J., "A Procedure for Normalizing Impact Response Data," SAE 840884, Warrendale, PA, May, 1984.

#### APPENDIX

#### ANALYSIS OF ASSOCIATION PEUGEOT - RENAULT LATERAL ABDOMINAL IMPACT DATA

This appendix describes the application of the normalization techniques of Mertz (3) to the lateral abdominal impact data provided by the Association Peugeot-Renault (2).

#### A.1 ORIGINAL DATA

Researchers of the Association Peugeot-Renault subjected eleven unembalmed cadavers to lateral free falls onto simulated armrests (1). The cadavers were perfused and accelerometers were attached to the 12th thoracic vertebral body and the 9th rib on the left and right sides. The cadavers were at room temperature during the test. The simulated armrest consisted of a rigid hardwood impact surface secured to a supporting material. The hardwood section was 7 cm wide and 2.5 cm thick, with rounded the edges and in the componiting is material owas so either rigid hardwood, polystyrene, or phenespan." The thickness of the supporting material ranged from .6 cm to 3.0 cm. The armrest was secured to a piezoelectric load cell. Initially, the cadavers were suspended 1 or 2 meters above the top surface of the armrest, as shown in Figure 1. The cadavers were positioned such that their right sides would impact the armrest at the level of their 9th ribs ensuring involvement of their livers. Their right arms were raised so as not to impact the armrest. Following each test, the cadaver was autopsied for rib fractures and injuries to the liver.

Table 1 provides a summary of the weights of the cadavers and their abdominal widths measured at the level of the 9th rib. Also given are the total armrest height and type of supporting material used for each test. The force-time plots for the load applied to the cadavers' abdomens by the simulated armrest are shown in Figures 2 through 5. The acceleration-time plots for the spine at the level of T12 are





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|             | Cada                 | ver Data                   |                       | Test Condition         | Ø                         | Test R        | esults                         | Effect         | tve Mass                             | Charac                     | teristic<br>Latios                        |                | Normal:<br>Facto | Lz İng<br>Drs          |
|-------------|----------------------|----------------------------|-----------------------|------------------------|---------------------------|---------------|--------------------------------|----------------|--------------------------------------|----------------------------|---|----------------|------------------|------------------------|
| Test<br>No. | Body<br>Mass<br>(kg) | Abdominal<br>Depth<br>(cm) | Drop<br>Height<br>(m) | Supporting<br>Material | Armrest<br>Height<br>(cm) | Impulse<br>Ns | Change in<br>Velocity<br>(m/s) | M<br>e<br>(kg) | Percent of<br>Body Mass<br>(%)       | Mass<br>R<br>m             | Stiffness<br>R<br>x                       | Time<br>R<br>t | Force L          | vcceleration<br>R<br>a |
| 205         | 32                   | 13.5                       | 1                     | hardwood               | 3.1                       | 29.9          | 4.7                            | 6.36           | 19.9                                 | 2.58                       | 1.85                                      | 1,18           | 2.18             | .85                    |
| 219         | 52                   | 18.5                       | <b>F</b>              | hardwood               | 4.1                       | 52.3          | 7.4                            | 11.89          | 22.9                                 | 1.38                       | 1.35                                      | 1.01           | 1.36             | 66.                    |
| 206         | 82                   | 24                         | 1                     | hardwood               | 5.1                       | 107.4         | 5.1                            | 21.02          | 25.6                                 | .78                        | 1.04                                      | .87            | 06.              | 1.15                   |
| 215         | 53                   | 20.5                       | 2                     | hardwood               | 3.1                       | 9.9           | 6.4                            | 15.55          | 29.3                                 | 1.05                       | 1.22                                      | .93            | 1.13             | 1.08                   |
| 216         | 67                   | 20.7                       | 2                     | hardwood               | 5.1                       | 77.6          | 6.6                            | 11.82          | 24.1                                 | 1.39                       | 1.21                                      | 1.07           | 1.30             | .93                    |
| 210         | 11                   | 26.3                       | 1                     | polystyrene            | 5.1                       | 77.2          | 3c-8d47-<br>0•5                | 120e0-4a8      | 11rds/sist/d449ea<br>1-tr-9790-5-198 | alog/standa<br>136fab9/isc | lards, iteh, ai/cat<br><b>56</b> 5 123 b1 | tps://stand    | 1.00 µ           | .95                    |
| 211         | 43                   | 18.5                       | Ч                     | phenespan              | 5.3                       | 52.3          | 6.3                            | 8.30           | 6861:5-06<br>19.3                    | 86 • I<br>ISO/TR 97        | 1.35                                      | 1.21           | 1.63             | .83                    |
| 212         | 45                   | 21                         | 1                     | polystyrene            | 5.5                       | 41.4          | 5.4                            |                | KU PK<br>ls.iteh.a                   | andarc                     | h STAI                                    | 1.34<br>0      | 1.59             | . 75                   |
| 213         | 17                   | 24.5                       | 2                     | polystyrene            | 5.5                       | 91.3          | 8.5                            | 10.75          | 14.0                                 | 1.53                       | 1.02                                      | 1.22           | 1.25             | .82                    |
|             |                      |                            |                       | •<br>•                 |                           |               |                                |                |                                      |                            |   |                |                  |                        |

Note: Average Percent Body Mass = 21.6%

Table 1 - Cadaver Characteristics and Test Conditions for the Lateral Abdominal Impact Tests Performed by the ilt (2) and Normalization Factors for the Abdominal Force-Time Data. +-Do. D Acordation

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FIGURE 2. LATERAL ABDOMINAL FORCE-TIME CURVES FOR CADAVERS SUBJECTED TO 1 METER DROPS ONTO RIGID IMPACT SURFACES (2).



FIGURE 3. LATERAL ABDOMINAL FORCE-TIME CURVES FOR CADAVERS SUBJECTED TO 2 METER DROPS ONTO RIGID IMPACT SURFACES (2).

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- FIGURE 4. LATERAL ABDOMINAL FORCE-TIME CURVES FOR CADAVERS SUBJECTED TO 1 METER DROPS ONTO CRUSH-ABLE IMPACT SURFACES (2).
- FIGURE 5. LATERAL ABDOMINAL FORCE-TIME CURVE FOR A CADAVER SUBJECTED TO A 2 METER DROP ONTO A CRUSHABLE IMPACT SURFACE (2).