

Edition 1.0 2013-07

# INTERNATIONAL STANDARD

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Semiconductor devices – Micro-electromechanical devices – Part 11: Test method for coefficients of linear thermal expansion of free-standing materials for micro-electromechanical systems

Dispositifs à semiconducteurs – Dispositifs microélectromécaniques – Partie 11: Méthode d'essai pour les coefficients de dilatation thermique linéaire des matériaux autonomes pour systèmes microélectromécaniques





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### IEC 62047-11:2013

Dispositifs à semiconducteurs - Dispositifs microélectromécaniques -Partie 11: Méthode d'essai pour les coefficients de dilatation thermique linéaire des matériaux autonomes pour systèmes microélectromécaniques

INTERNATIONAL ELECTROTECHNICAL COMMISSION

COMMISSION ELECTROTECHNIQUE INTERNATIONALE

PRICE CODE CODE PRIX



ICS 31.080.99

ISBN 978-2-8322-0965-3

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## CONTENTS

FOF	REWC	)RD	3			
1	Scop	e	5			
2	Norm	ative References	5			
3	Symbols and designations 5					
4	Test	piece	6			
	4.2	Shape of test piece				
	4.3	Test piece thickness	6			
	4.4	In-plane type test piece	7			
	4.5	Out-of-plane type test piece	7			
5	Testing method and test apparatus					
	5.1	Measurement principle	7			
		5.1.1 General	7			
		5.1.2 In-plane method	8			
		5.1.3 Out-of-plane method	8			
	5.2	Test apparatus	9			
		5.2.1 General	9			
		5.2.2 In-plane method	9			
		5.2.3 Out-of-plane method DARD PKEVIEW	9			
	5.3	Temperature measurement	9			
	5.4	In-plane test piece handling	9			
	5.5	Thermal strain measurement <u>IEC 62047-11:2013</u>	10			
	5.6	Heating SREP. Standards. iteh.ai/catalog/standards/sist/5de28455-3d05-48ef-9e73	10			
	5.7	Data analysis	10			
		5.7.1 General	10			
		5.7.2 Terminal-based calculation	10			
6	Test	report	10			
0 restreport						
Ann		(informative) Test piece labitation	12			
Ann	Iex B		13			
Ann	ex C	(informative) Test piece releasing process	14			
Ann	ex D	(informative) Out-of-plane test setup and test piece example	15			
Annex E (informative) Data analysis example in in-plane test method16						
Annex F (informative) Data analysis example in out-of-plane test method17						
Bibl	iograp	phy	19			
Figu	iro 1	Thin film test piece	6			
Eigu		CLTE mosquroment aringiales				
Figu		- CETE measurement principles.	0			
Figure A.1 – Schematic test piece fabrication process						
Figu	Figure B.1 – Auxiliary jigs and a specimen example13					
Figu	Figure C.1 – Schematic illustration showing the test piece releasing process14					
Figu	Figure D.1 – Example of test setup and test piece15					
Figu	Figure E.1 – Example of CLTE measurement with an aluminium test piece					
Figure F.1 – Example of CLTE measurement with a gold test piece						
Table 1 Symbole and designations						
Table T – Symbols and designations						

#### INTERNATIONAL ELECTROTECHNICAL COMMISSION

### SEMICONDUCTOR DEVICES – MICRO-ELECTROMECHANICAL DEVICES –

### Part 11: Test method for coefficients of linear thermal expansion of free-standing materials for micro-electromechanical systems

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The text of this standard is based on the following documents:

FDIS	Report on voting
47F/154/FDIS	47F/161/RVD

Full information on the voting for the approval of this standard can be found in the report on voting indicated in the above table.

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## SEMICONDUCTOR DEVICES – MICRO-ELECTROMECHANICAL DEVICES –

### Part 11: Test method for coefficients of linear thermal expansion of free-standing materials for micro-electromechanical systems

#### 1 Scope

This part of IEC 62047 specifies the test method to measure the linear thermal expansion coefficients (CLTE) of thin free-standing solid (metallic, ceramic, polymeric etc.) micro-electro-mechanical system (MEMS) materials with length between 0,1 mm and 1 mm and width between 10  $\mu m$  and 1 mm and thickness between 0,1  $\mu m$  and 1 mm, which are main structural materials used for MEMS, micromachines and others. This test method is applicable for the CLTE measurement in the temperature range from room temperature to 30 % of a material's melting temperature.

#### 2 Normative References

The following documents, in whole or in part, are normatively referenced in this document and are indispensable for its application. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

#### IEC 62047-11:2013

IEC 62047-3, Semiconductor devices Micro-electromechanical devices – Part 3: Thin film standard test piece for tensile-testing 35edc38/iec-62047-11-2013

#### 3 Symbols and designations

Symbols and corresponding designations are given in Table 1.

Symbol	Unit	Designation
g	μm	Gauge length
L <sub>0</sub>	μm	Initial length of a test piece
$L_{T}$	μm	Length of a test piece at temperature T
Т	°C	Temperature
t	μm	Thickness of a test piece
W	μm	Width of a test piece
$lpha_{av}$	1/°C	Average coefficient of thermal expansion of a test piece
$\alpha_{ m S}$	1/°C	Average coefficient of thermal expansion of a substrate
$\delta_{T}$	μm	Thermal deformation
ε <sub>T</sub>	1	Thermal strain

#### Table 1 – Symbols and designations

#### 4.1 General

The test piece shall be prepared in accordance with the IEC 62047-3. It should be fabricated through the same processes used for the device where the thin film is applied. It should have dimensions in the same order of that of the objective device component in order to minimize the size effect. There are many fabrication methods depending on the applications. A typical test piece fabrication method based on MEMS processes is shown in Annex A.

#### 4.2 Shape of test piece

The dimensions of a test piece, such as thickness (*t*), width (*w*), and initial length ( $L_0$ ), in Figure 1 should be designed to be the same order of the device. The dimensions shall be specified within the accuracy range of  $\pm 1$  % of the corresponding length scale. The cross sections along the line *A*-*A*' are indicated as cross-hatching in Figure 1. The gauge length in Figure 1 shall be measured from centre to centre of the gauge marks.



#### Key

- 1 holes for die fixing, tying a yarn or wire for the weight hanging
- 2 free-standing test piece
- 3 gauge marks to define a gauge length
- 4 substrate to accommodate a test piece
- 5 portions to be separated before testing to make a test piece free-standing

NOTE Imaginary line "a": The support straps "5" can be separated by cutting those along this line.

#### Figure 1 – Thin film test piece

#### 4.3 Test piece thickness

Each test piece thickness shall be measured and the thickness should be recorded in the report. Each test piece thickness should be measured directly with calibrated equipment (for example scanning electron microscope, ellipsometer, etc.). However, the film thickness evaluated from step height (by scanning probe microscope, white light interferometric microscope, or surface profilometer, etc.) along the line B-B' in Figure 1 can be used as the thickness of a test piece.

#### 4.4 In-plane type test piece

The internal stress of the test piece should have proper values in order not to cause curling of the test piece. Gauge marks should be formed in the middle of a test piece. The gauge marks should not restrict the elongation of the test piece and should have small influence on test result. The stiffness of the gauge mark should be less than  $\pm$  1 % of that of the test piece. The symmetry in the thickness direction should be maintained in order to avoid the curling of the test piece. A dummy part shall be attached to a test piece as shown in Figure C.1.

#### 4.5 Out-of-plane type test piece

An out-of-plane type test piece may be used if the free-standing test piece has thickness below 1  $\mu$ m or has low strength to hang a weight. The holes and gauge marks in Figure 1 are not necessary in case of out-of-plane type test. The supporting straps don't need to be separated. The test piece should be buckled concavely or convexly before measurement.

#### Testing method and test apparatus 5

#### **Measurement principle** 5.1

#### 5.1.1 General

The average CLTE value shall be obtained by linearly correlating the thermal strain change  $(\Delta \varepsilon_{T})$  by the corresponding temperature change  $(\Delta T)$ . **iTeh STANDARD PREVIEW** 

## (stand ar € Ariteh.ai) (1)

The thermal strains shall be obtained with two kinds of test methods as shown in Figure 2.

In-plane test method shall be preferred to out-of-plane method in the view points of accuracy and uncertainties. If there is no test setup as shown in Figure 2 a) and Figure C.1, out-ofplane method shall be used as an alternative because the out-of-plane method needs a furnace and measuring equipment.



#### Key

- 1 heating furnace equipped with a hatch
- 2 viewport to observe and measure deformation of a test piece PREVIEW
- <sup>3</sup> metal wire or yarn to hang a weight (standards.iteh.ai)
- 4 weight
- 5 translational stage to hold and release a weight 62047-11:2013
- 6 bolt to fix a die to the test/die holder hai/catalog/standards/sist/5dc28455-3d05-48cf-9c73-
- 7 free-standing test piece 845fa35edc38/iec-62047-11-2013
- 8 test die
- 9 test die holder
- 10 dummy part for the symmetry of a test piece

#### Figure 2 – CLTE measurement principles

#### 5.1.2 In-plane method

The thermal deformation ( $\delta_{T}$ ) shall be measured directly as a function of temperature by using a noncontact in-plane displacement measurement technique (laser interferometry, 2-D digital image correlation, etc.). The specimen should be in a furnace as shown in Figure 2a). The weight should be hung to a test piece in order to make it flattened. The elastic modulus should be independent of temperature in the range of measurement. The plastic deformation due to weight (yielding) or temperature (creep) should be avoided. The thermal strain shall be calculated by dividing the elongation by the gauge length.

$$\varepsilon_{\rm T} = \frac{\delta_{\rm T}}{g} \tag{2}$$

#### 5.1.3 Out-of-plane method

The entire profile of a specimen along the length direction should be measured as a function of temperature by an accurate out-of-plane displacement measurement method (white light interferometric microscope, laser Doppler interferometer, 3-D digital image correlation, etc) as shown in Figure 2b). A test piece should be initially buckled. The initial length ( $L_0$ ) at room temperature and successive lengths ( $L_T$ ) at different temperatures of a specimen shall be calculated with the profiles measured. The thermal deformation ( $\delta_T$ ) shall be the difference

between  $L_{T}$  and  $L_{0}$ . The thermal strain shall be calculated by dividing the deformation by the initial length.

$$\varepsilon_{\rm T} = \frac{\delta_{\rm T}}{L_0} = \frac{L_{\rm T} - L_0}{L_0} \tag{3}$$

The CLTE of a substrate should be considered to calculate the accurate CLTE of the test piece because both experience the same amount of temperature change. The substrate effect shall be considered by adding the CLTE of the substrate to the average CLTE value from measurement. The CLTE of the substrate should be measured by using a test standard [1, 2, 3]<sup>1</sup> if there is no certified CLTE value for the substrate.

$$\alpha_{\rm av} = \frac{\Delta \varepsilon_{\rm T}}{\Delta T} + \alpha_{\rm S} \tag{4}$$

#### 5.2 Test apparatus

#### 5.2.1 General

5.2.2

The test piece should be seated in a furnace. The temperature of the furnace should be controlled within  $\pm$  1 °C by the feedback control.

# In-plane method

A test apparatus shall be equipped with basic components shown in Figure 2a). A transparent window like a glass shall be used as a viewport. The hatch of a furnace should be closed and a predetermined weight should be hung to 2the yam or metal wire to make a test piece flat enough but not to the point where it could yield si A Stest piece should be in a free-standing state before heating it up. See Annexes B and C62047-11-2013

#### 5.2.3 Out-of-plane method

A furnace having a view port is only needed to heat up a test piece. A test piece should be in a free-standing state before heating it up. See Annex D.

#### 5.3 Temperature measurement

The method of temperature measurement should be sufficiently sensitive and reliable. Temperature measurements should be made with a calibrated thermometer. Contact (thermocouple, etc.) or noncontact (infrared thermometers, optical pyrometers, etc.) thermometers shall be used. The temperature sensor that enables to measure  $\pm$  0,5 % of the maximum temperature accuracy shall be used and should be calibrated periodically. The temperature sensing points should be located very near to a test piece to measure the temperature accurately. The temperature distribution in the length direction should be doubly checked by a noncontact sensor like an IR thermometer.

#### 5.4 In-plane test piece handling

A metal wire or yarn should be tied around a right hole in Figure 1 for the later weight hanging. The supporting portions in Figure 1 should be separated by cutting those before setting it up to the furnace. The test piece should be handled with special care after separating the supporting portions. This step can be skipped if a test piece is robust enough to handle easily. See Annex B.

<sup>&</sup>lt;sup>1</sup> Figures in square brackets refer to the bibliography.

(5)

#### 5.5 Thermal strain measurement

A displacement measurement method that enables to measure 0,01 % strain value shall be used. Displacement should be measured at every 1 °C during a test to adequately define the temperature-strain curve.

### 5.6 Heating speed

The thermal strains should be recorded as a function of temperature while raising the temperature below the rate of 1  $^{\circ}$ C/min to avoid thermal inertia.

#### 5.7 Data analysis

#### 5.7.1 General

The average CLTE shall be calculated by using one of the following methods.

#### 5.7.2 Terminal-based calculation

The average linear CLTE value shall be calculated by dividing the thermal strain difference  $(\Delta \varepsilon_{\rm T})$  by the corresponding temperature difference  $(\Delta T)$ . The temperature-strain curve should be linear in the range of interest.

### 5.7.3 Slope calculation by linear least squares method

The linear least squares method shall be used to fit the thermal strain ( $\varepsilon_{T}$ ) versus temperature (*T*) data. The average CLTE ( $\alpha_{av}$ ) shall be the slope of the linearly fitted curve. The intercept on the thermal strain axis ( $\varepsilon_{T0}$ ) does not affect the result at all. The coefficient of correlation shall be over 0,95 to ensure the linearity. See Annexes E and F.

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## 6 Test report

The test report shall contain at least the following information.

- a) reference to this international standard;
- b) identification number of the test piece;
- c) displacement measuring equipment;
  - type;
  - sensitivity and accuracy;
- d) test piece material;
  - in case of single crystal: crystallographic orientation;
  - in case of polycrystal: texture and grain size;
- e) shape and dimension of test piece;
  - type (in-plane or out-of-plane)
  - picture;
  - gauge length (in-plane method only);
  - thickness;
  - width;
- f) test piece fabrication method and its detail;
  - deposition method;

- fabrication condition;
- g) weights and stresses induced (in-plane method only);
- h) temperature measurement method and its accuracy;
- i) measured properties and results;
  - thermal strain curve;
  - average linear coefficient of thermal expansion;
  - calculation methods (terminal-based or least squares method);
  - temperature range.

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