



Test Methods for Destructive Shear Testing of Ball Bonds¹

This standard is issued under the fixed designation F 1269; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ε) indicates an editorial change since the last revision or reapproval.

ε¹ NOTE—Keywords were added editorially in June 1995.

1. Scope

1.1 These test methods cover tests to determine the shear strength of a series of ball bonds made by either thermal compression or thermosonic techniques.

NOTE 1—Common usage at the present time considers the term “ball bond” to include the enlarged spheroidal or nailhead portion of the wire, (produced by the flameoff and first bonding operation in the thermal compression and thermosonic process, or both,) the underlying bonding pad, and the ball bond-bonding pad interfacial-attachment area or weld interface.

1.2 These test methods cover ball bonds made with small diameter (from 18 to 76-μm (0.0007 to 0.003-in.)) wire of the type used in integrated circuits and hybrid microelectronic assemblies.

1.3 These test methods can be used only when the ball height and diameter are large enough and adjacent interfering structures are far enough away to allow suitable placement and clearance (above the bonding pad and between adjacent bonds) of the shear test ram.

1.4 These test methods are destructive. They are appropriate for use in process development or, with a proper sampling plan, for process control or quality assurance.

1.5 A nondestructive procedure is possible;² although it may be contra indicated due to the possible interference with adjacent wire bonds and microcircuit components.

1.6 The values stated in SI units are to be regarded as the standard. The values given in parentheses are for information only.

1.7 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use. Fig. 1 Fig. 2 Fig. 3 Fig. 4 Fig. 5 Fig. 6 Fig. 7 Fig. 8 Fig. 9*

2. Referenced Documents

2.1 ASTM Standards:

¹ These test methods are under the jurisdiction of ASTM Committee F-1 on Electronics and is the direct responsibility of Subcommittee F01.07 on Wire Bonding.

Current edition approved Dec. 29, 1989. Published March 1990.

² Panousis, N. T., and Fischer, M. W., “Nondestructive Shear Testing of Ball Bonds”, *International Journal of Hybrid Microelectronics*, Vol 6, No. 1, 1983, p. 142.

F 458 Practice for Nondestructive Pull Testing of Wire Bonds³

F 459 Test Methods for Measuring Pull Strength of Micro-electronic Wire Bonds³

2.2 NIST Document:

NBS Handbook 105-1 Specification and Tolerances for Reference Standards and Field Standards, Weights and Measures⁴

IOLM Class M2-Circular 547-1 Precision Laboratory Standards of Mass and Laboratory Weights⁴

2.3 Military Standard:

MIL-STD 883C, Method 2010⁵

3. Terminology

3.1 Definitions of Terms Specific to This Standard:

3.1.1 *ball lift*—a separation of the ball bond at the bonding pad interface with little or no residual (less than 25 % of the bond deformation area) ball metallization remaining on the bonding pad (that remains essentially intact). In the case of gold ball bonds on aluminum pad metallization, a ball lift is defined as a separation of the ball bond at the bonding pad interface with little or no intermetallic formation either present or remaining (area of intermetallic less than 25 % of the bond deformation area).

3.1.1.1 *Discussion*—intermetallic refers to the aluminum gold alloy formed at the ball bond pad metallization interfacial area where a gold ball bond is attached to an aluminum pad metallization.

3.1.2 *ball shear (weld interface separation)*—an appreciable intermetallic (in the case of the aluminum-gold system) and ball metallization, or both, (in the case of the gold-to-gold system) remains on the bonding pad (area of remaining metal or intermetallic greater than 25 % of the bond deformation area).

3.1.3 *bonding pad lift (substrate metallization removal)*—a separation between the bonding pad and the underlying substrate. The interface between the ball bond and the residual pad metallization attached to the ball remains intact.

³ *Annual Book of ASTM Standards*, Vol 10.04.

⁴ Available from the National Technical Information Service, 5285 Port Royal Rd., Springfield, VA 22161.

⁵ Available from Standardization Documents Order Desk, Bldg. 4 Section D, 700 Robbins Ave., Philadelphia, PA 19111-5094, Attn: NPODS.

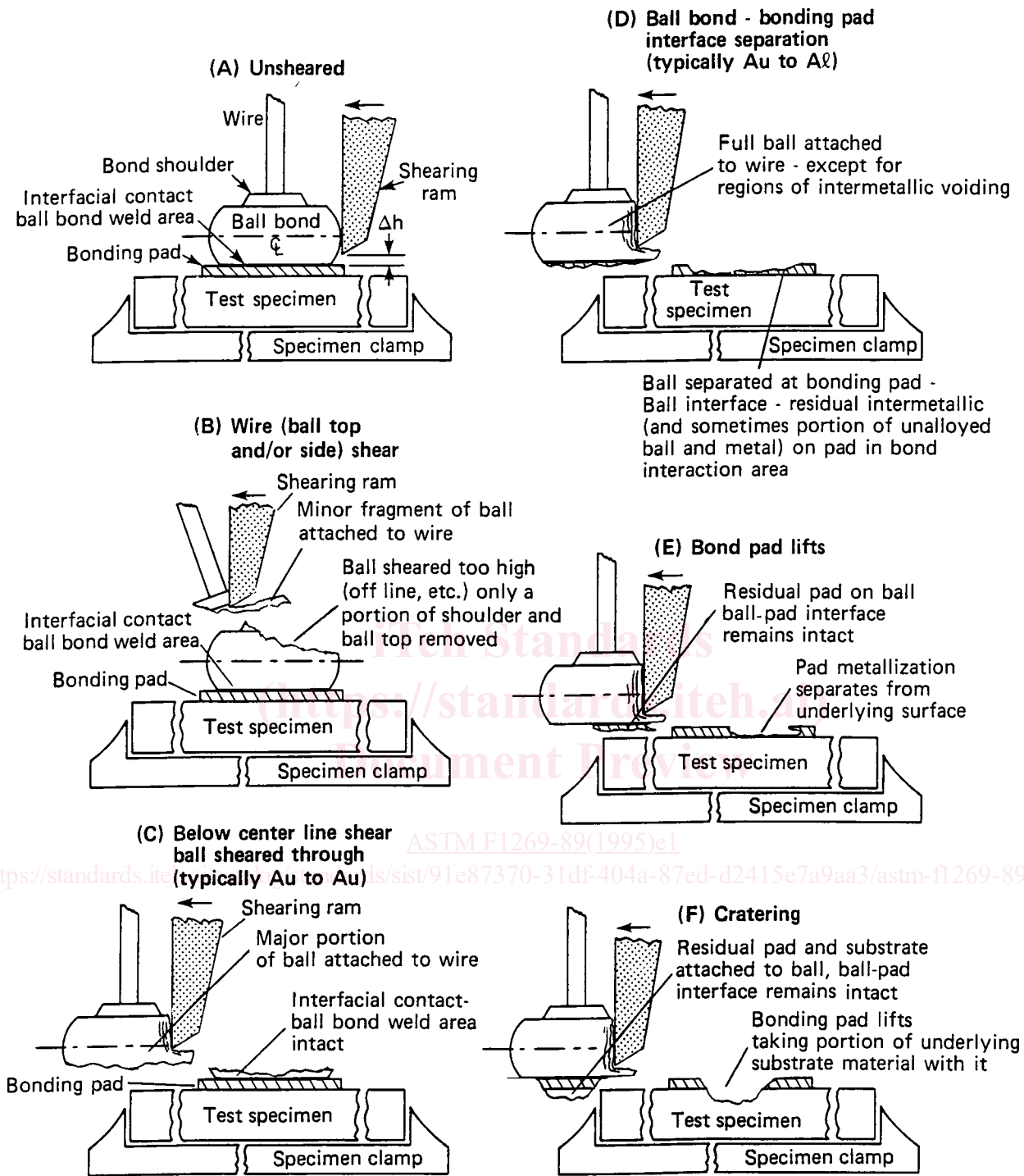


FIG. 1 Ball Shear Failure Modes

3.1.4 *cratering*—bonding pad lifts taking a portion of the underlying substrate material with it. Residual pad and substrate material are attached to the ball. The interface between the ball and this residual material remains intact.

3.1.4.1 *Discussion*—It should be noted that cratering can be caused by several factors including the ball bonding operation, the post-bonding processing, and even the act of shear testing itself. If cratering occurs, chemically etch off the ball bonds and bond pads of untested units and microscopically check for

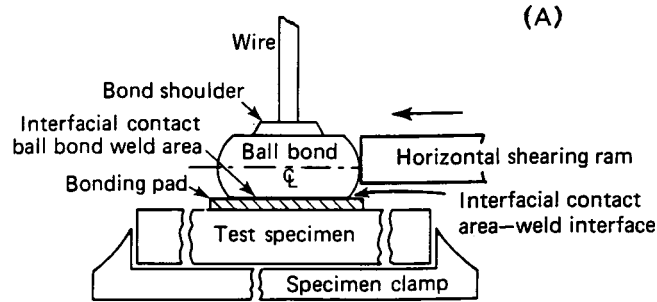
cratering. Cratering caused prior to the shear test operation is unacceptable.

Various aspects of the failure mode definitions are illustrated in Fig. 1.

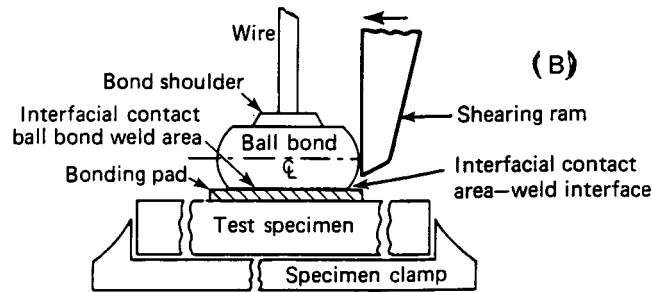
4. Summary of Test Methods

4.1 The microelectronic device with the ball bond (wire bond (see Practice F 458 and Test Methods F 459)) to be tested is held firmly in an appropriate fixture. A shearing ram is

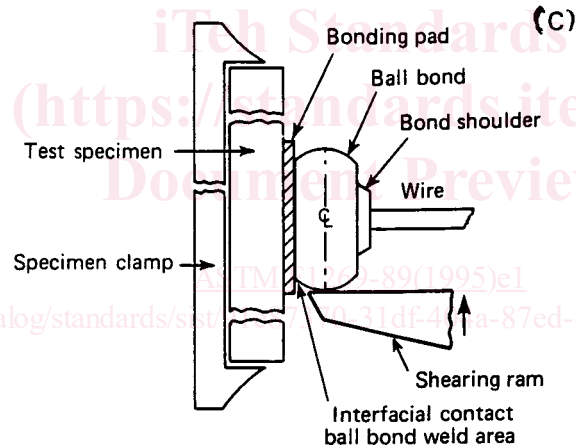
• HORIZONTAL RAM



• VERTICAL RAM



• VERTICAL SAMPLE HOLDER



NOTE 1—Schematic diagrams of the ball shear test. (A) Horizontal sample and horizontal ram. (B) Horizontal sample and vertical ram. (C) Vertical sample and vertical ram. The bonded (welded) area may be less than the interfacial contact area (area of intimate contact as observed optically.) Typical dimensions with 25- μm (1-mil) diameter wire are: ball diameter 75 to 110 μm (3.0 to 4.5 mil) and ball height 25 μm (1 mil) or less.

FIG. 2 Ball Shear Test Configurations

positioned parallel to the substrate and approximately 25 μm (1 mil) above the substrate metallization. A typical shearing configuration is shown in Fig. 2. The ram is then moved into the ball until the ball separates from the substrate. The force applied to the ram, in order to cause the failure of the ball bond, is recorded. The mode of failure (for example, ball lift, weld-interface separation, cratering, etc.) is observed and recorded.

NOTE 2—Bonds made with larger diameter wire may require that the ram be placed further above the substrate, but in all cases the ram should be located below the ball's horizontal centerline. The distance below the center should be at least half the distance between the center line and the substrate.

NOTE 3—Besides ball separation from the substrate, other modes of failure are possible and will be described in Section 6.

5. Significance and Use

5.1 Failure of microelectronic devices is often due to the failure of an interconnection bond. A common type of interconnection bond is the thermo compression or thermosonic gold wire bond. A very important element of this interconnection is the first bond or ball bond. These test methods can assist in maintaining control of the process for making ball bonds. They can be used to distinguish between weak and nonadherent ball bonds, of both, and bonds that are acceptably strong.

5.2 These test methods are appropriate for on-line use in process control, for process development, for purchase specifications, and for research in support of improved yield and reliability. Since the ball shearing method tests only the first bond in a microelectronic wire bond interconnection system, it

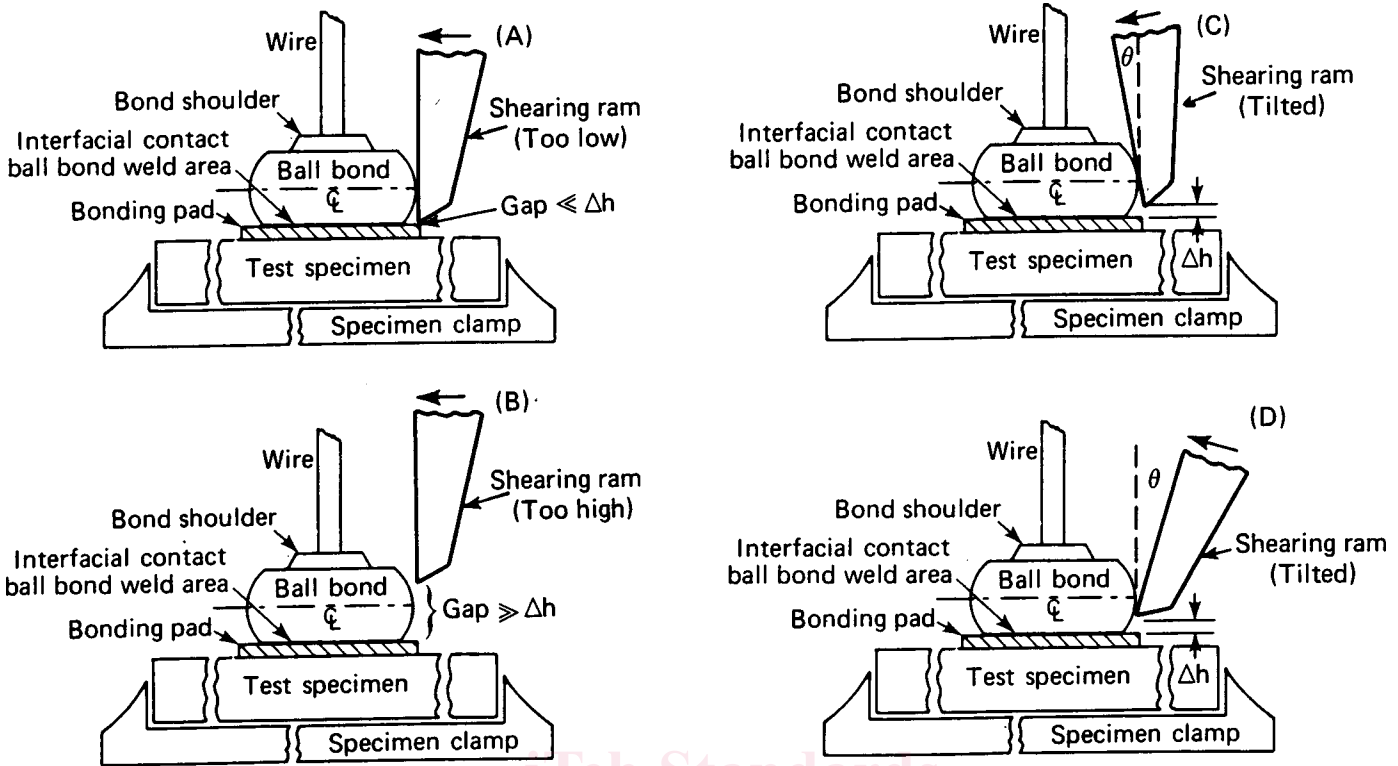


FIG. 3 Ball Shear Interferences

must be used in a complementary fashion^{6,7} with the wire bond pull test.³

6. Inferences

6.1 The most common interference is wire shear in which the ball is sheared too high or offline. Only a minor fragment of the ball is attached to the wire. The major portion of the ball remains on the pad with the bond-pad weld interface region intact. Wire shear is illustrated in Fig. 1, View B.

6.2 Many of the common interference modes (such as wire shear) are caused by improper positioning of the ram during the ball shear operation as shown in Fig. 3. Rams that are too high (Fig. 3, View B) or angled upward (Fig. 3, View D) result in lower than normal shear strength values. Rams that are angled downward (Fig. 3, View C) or positioned too low (Fig. 3, View A) will strike the bonding pad and the substrate, or both, (chip) and cause inordinately high shear strength as well as potentially damage the shearing ram.

6.3 Shearing gold ball bonds on gold metallization pads or substrates can lead to friction rewelding as illustrated in Fig. 4. As a strongly welded gold bond is sheared, the ball tends to tip away from the ram and contact the substrate as it moves. The ball smears against the pad metallization and rewelds itself often several times before it finally clears the metallization.

⁶ Charles, Jr., H. K., and Clatterbaugh, G. V., "Ball Bond Shearing—A Complement to the Wire Bond Pull Test", International Journal of Hybrid Microelectronics, Vol 6, No. 1, 1983, p. 171.

⁷ Harman, G. G. "The Microelectronic Ball-Bond Shear Test—A Critical Review and Comprehensive Guide to its Use", International Journal of Hybrid Microelectronics, Vol 6, No. 1, 1983, p. 127.

6.4 In bonding systems in which excessive intermetallic growth has formed around the ball bond, the shearing ram may contact the intermetallic rather than the ball bond and thus the shear readings can be in error (that is, weak ball bond shear is masked by the shear strength of the strong intermetallic wreath surrounding it).

7. Apparatus

7.1 *Ball Bond Shearing Machine*—Apparatus for measuring the ball bond shear strength are required with the following components:

7.1.1 *Shearing Ram*—Various shearing tools or rams have been recommended in the technical literature, but the ones that appear the most effective have a flat chisel shape with a shearing edge dimension equal to approximately 1 to 2-ball diameters as shown in Fig. 5. For 25.4- μ m (1-mil) diameter wire this dimension would be approximately 0.152 mm (6 mils).

7.1.2 *Shearing and Gaging Mechanism*—Mechanism for applying a measured vertical (or horizontal) force to the shearing is needed. The mechanism shall incorporate a means for recording maximum force applied and shall be capable of applying the shear force at a uniform rate of ram motion. Force application rate can be variable (either continuously or in fixed steps) to accommodate different shearing conditions and configurations, or both. In no case should the ram speed exceed 6.0 mm/s.

NOTE 4—It has been shown² that the shear force is independent of force application rate in the range from 0.25 to 6.0 mm/s.

NOTE 5—Electronic-strain gage-force reading mechanisms are preferred; however, the dynamometer type mechanisms known as "gram