



Standard Test Method for Measuring Heat-Transfer Rate Using a Thermal Capacitance (Slug) Calorimeter¹

This standard is issued under the fixed designation E 457; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ϵ) indicates an editorial change since the last revision or reapproval.

1. Scope

1.1 This test method describes the measurement of heat transfer rate using a thermal capacitance-type calorimeter which assumes one-dimensional heat conduction into a cylindrical piece of material (slug) with known physical properties.

1.2 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

1.3 The values stated in SI units are to be regarded as the standard.

NOTE 1—For information see Test Methods E 285, E 422, E 458, E 459, and E 511.

2. Referenced Documents

2.1 ASTM Standards:

E 285 Test Method for Oxyacetylene Ablation Testing of Thermal Insulation Materials²

E 422 Test Method for Measuring Heat Flux Using a Water-Cooled Calorimeter²

E 458 Test Method for Heat of Ablation²

E 459 Test Method for Measuring Heat Transfer Rate Using a Thin-Skin Calorimeter²

E 511 Test Method for Measuring Heat Flux Using a Copper-Constantan Circular Foil, Heat-Flux Gage²

3. Summary of Test Method

3.1 The measurement of heat transfer rate to a slug or thermal capacitance type calorimeter may be determined from the following data:

3.1.1 Density and specific heat of the slug material,

3.1.2 Length or axial distance from the front face of the cylindrical slug to the back-face thermocouple,

3.1.3 Slope of the temperature—time curve generated by the back-face thermocouple, and

3.1.4 Calorimeter temperature history.

3.2 The heat transfer rate is thus determined numerically by

multiplying the density, specific heat, and length of the slug by the slope of the temperature—time curve obtained by the data acquisition system (see Eq 1).

3.3 The technique for measuring heat transfer rate by the thermal capacitance method is illustrated schematically in Fig. 1. The apparatus shown is a typical slug calorimeter which, for example, can be used to determine both stagnation region heat transfer rate and side-wall or afterbody heat transfer rate values. The annular insulator serves the purpose of minimizing heat transfer to or from the body of the calorimeter, thus approximating one-dimensional heat flow. The body of the calorimeter is configured to establish flow and should have the same size and shape as that used for ablation models or test specimens.

3.3.1 For the control volume specified in this test method, a thermal energy balance during the period of initial linear temperature response can be stated as follows:

$$\text{Energy Received by the Calorimeter (front face)} \quad (1)$$

$$= \text{Energy Conducted Axially Into the Slug}$$

$$q_c = \rho C_p l (\Delta T / \Delta \tau) = (MC_p / A) (\Delta T / \Delta \tau)$$

where:

q_c = calorimeter heat transfer rate, W/m^2 ,

ρ = density of slug material, kg/m^3 ,

C_p = average specific heat of slug material during the temperature rise (ΔT), $\text{J/kg}\cdot\text{K}$,

l = length or axial distance from front face of slug to the thermocouple location (back-face), m,

ΔT = $(T_f - T_i)$ = calorimeter slug temperature rise during exposure to heat source (linear part of curve), K,

$\Delta \tau$ = $(\tau_f - \tau_i)$ = time period corresponding to ΔT temperature rise, s,

M = mass of the cylindrical slug, kg,

A = cross-sectional area of slug, m^2 .

In order to determine the steady-state heat transfer rate with a thermal capacitance-type calorimeter, Eq 1 must be solved by using the known properties of the slug material³ (for example, density and specific heat)—the length of the slug, and the slope (linear portion) of the temperature—time curve obtained during

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² *Annual Book of ASTM Standards*, Vol 15.03.

³ “Thermophysical Properties of High Temperature Solid Materials,” TPRC, Purdue University, or “Handbook of Thermophysical Properties,” Tolukian and Goldsmith, MacMillan Press, 1961.

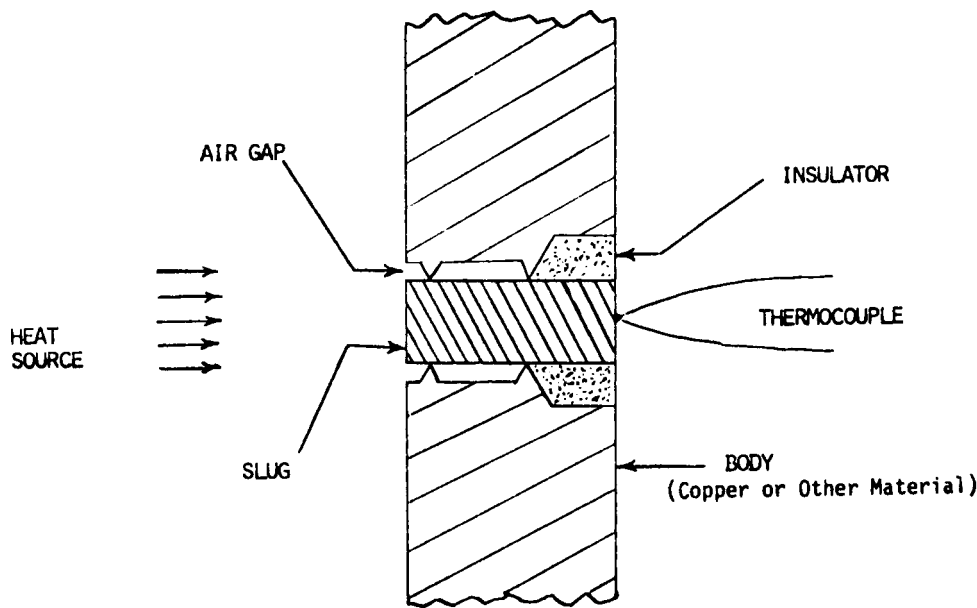


FIG. 1 Schematic of a Thermal Capacitance (Slug) Calorimeter

the exposure to a heat source. The initial and final temperature transient effects must be eliminated by using the initial linear portion of the curve (see Fig. 2).

3.3.2 In order to calculate the initial response time for a given slug, Eq 2 may be used.⁴

$$\tau_R = \frac{l^2 \rho C_p}{k \pi^2} \ln \left(\frac{2}{1 - \frac{q_{\text{indicated}}}{q_{\text{input}}}} \right) \quad (2)$$

where:

k = thermal conductivity of slug material, W/m·K

3.3.3 For maximum linear test time (temperature–time curve) within an allowed surface temperature limit, the relation shown as Eq 3 may be used for a calorimeter which is insulated by a gap at the back face.⁵

$$\tau_{\text{max,opt.}} = 0.48 \rho l C_p (\Delta T_{\text{front face}} / \dot{q}) \quad (3)$$

where:

$\Delta T_{\text{front face}}$ = the calorimeter final front face temperature minus the initial front face (ambient) temperature, T_o .

3.3.4 Eq 3 is based on the optimum length of the slug which can be obtained by applying Eq 4 as follows:

$$l_{\text{opt.}} = 3 k \Delta T_{\text{front face}} / 5 \dot{q}_c \quad (4)$$

3.4 To minimize side heating or side heat losses, the body is separated physically from the calorimeter slug by means of an insulating gap or a low thermal diffusivity material, or both. The insulating gap that is employed should be small, and recommended to be no more than 0.05 mm on the radius. Thus,

if severe pressure variations exist across the face of the calorimeter, side heating caused by flow into or out of the insulation gap would be minimized. Depending on the size of the calorimeter surface, variations in heat transfer rate may exist across the face of the calorimeter; therefore, the measured heat transfer rate represents an average heat transfer rate over the surface of the slug.

3.5 Since interpretation of the data obtained by this test method is not within the scope of this discussion, such effects as surface recombination and thermo-chemical boundary layer reactions are not considered in this test method.

3.6 If the thermal capacitance calorimeter is used to measure only radiative heat transfer rate or combined convective/radiative heat transfer rate values, the surface reflectivity of the calorimeter should be measured over the wavelength region of interest (depending on the source of radiant energy).

4. Significance and Use

4.1 The purpose of this test method is to measure the rate of thermal energy per unit area transferred into a known piece of material (slug) for purposes of calibrating the thermal environment into which test specimens are placed for evaluation. The calorimeter and holder size and shape should be identical to that of the test specimen. In this manner, the measured heat transfer rate to the calorimeter can be related to that experienced by the test specimen.

4.2 The slug calorimeter is one of many calorimeter concepts used to measure heat transfer rate. This type of calorimeter is simple to fabricate, inexpensive, and readily installed since it is not water-cooled. The primary disadvantages are its short lifetime and relatively long cool-down time after exposure to the thermal environment. In measuring the heat transfer rate to the calorimeter, accurate measurement of the rate of rise in back-face temperature is imperative.

4.3 In the evaluation of high-temperature materials, slug calorimeters are used to measure the heat transfer rate on

⁴ Ledford, R. L., Smotherman, W. E., and Kidd, C. T., "Recent Developments in Heat-Transfer Rate, Pressure, and Force Measurements for Hotshot Tunnels," AEDC-TR-66-228 (AD645764), January 1967.

⁵ Kirchhoff, R. H., "Calorimetric Heating-Rate Probe for Maximum-Response-Time Interval," *American Institute of Aeronautics and Astronautics Journal*, AIAA, Vol 2, No. 5, May 1964, pp. 966–67.