



Edition 1.2 2023-08 CONSOLIDATED VERSION

# INTERNATIONAL STANDARD

# NORME INTERNATIONALE



Power losses in voltage sourced converter (VSC) valves for high-voltage direct current (HVDC) systems – Part 2: Modular multilevel converters

Pertes de puissance dans les valves à convertisseur de source de tension (VSC) des systèmes en courant continu à haute tension (CCHT) – 9-aad7aea76431/iec-Partie 2: Convertisseurs multiniveaux modulaires





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# **REDLINE VERSION**

# **VERSION REDLINE**



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# CONTENTS

FOREW	/ORD	5					
1 Sc	ope	7					
2 No	rmative references	7					
3 Tei	3 Terms, definitions, symbols and abbreviated terms.						
3.1	Terms and definitions	8					
3.2	Symbols and abbreviated terms	9					
3.2	2.1 Valve and simulation data	9					
3.2	2.2 Semiconductor device characteristics	10					
3.2	2.3 Other component characteristics	10					
3.2	2.4 Operating parameters	10					
3.2	2.5 Loss parameters	11					
4 Ge	neral conditions	11					
4.1	General	11					
4.2	Principles for loss determination	12					
4.3	Categories of valve losses	12					
4.4	Loss calculation method	13					
4.5	Input parameters	13					
4.5	5.1 General	13					
4.5	5.2 Input data for numerical simulations	13					
4.5	5.3 Input data coming from numerical simulations	15					
4.5	5.4 Converter station data	15					
4.5	5.5 Operating conditions	16					
4.6	Contents and structure of valve loss determination report	16					
5 ht Conduction losses /catalog/standards/sist/02524bb0-191e-43c3-b209-aad7aea76431/ie							
5.1	General	16					
5.2	IGBT conduction losses	18					
5.3	Diode conduction losses	19					
5.4	Other conduction losses	20					
6 DC	voltage-dependent losses	21					
7 Losses in d.c. capacitors of the valve							
8 Sw	vitching losses	22					
0 0 1	Caparal	 					
0.1 8.2		22					
0.Z 8 3	Diode switching losses	22					
	ber losses	23					
0 1	Snubber eireuit lesses	20 					
9.1	Shubber circuit losses	Z3					
9.2		24 24					
9.2	2 Power supply from off state voltage across each IGBT	24 25					
9.2 0.0	P 2 Power supply from the dic capacitor	20					
9.2 10 Tot	tal valve losses ner HVDC substation	20 26					
	$\Delta (informative) Departmention of neuron land machanisms in MMO we have$	20					
Annex A	A (Informative) Description of power loss mechanisms in MMC valves	28					
A.1	Introduction to MMC Converter topology	28					
A.2	Valve voltage and current stresses	31					
A.2	2.1 Simplified analysis with voltage and current in phase	31					
A.2	2.2 Generalised analysis with voltage and current out of phase	32					

IEC 62751-2:2014+AMD1:2019 - 3 -+AMD2:2023 CSV © IEC 2023 A.2.3 A.3 A.3.1 A.3.2 Conduction losses in semiconductors ......40 A.3.3 A.3.4 Other conduction losses ......45 A.4 Switching losses ......45 A.4.1 A.4.2 Analysis of state changes during cycle ......46 A.4.3 Worked example of switching losses......47 A.5 A.5.1 A.5.2 A.5.3 Valve electronics power consumption ......53 A.6 A.6.1 A.6.2 A.6.3 Annex B (informative) Recommended data to be supplied with the loss calculation Bibliography......61

# tandards.iten.ai)

Figure 1 – Two basic versions of MMC building block designs	16
Figure 2 – Conduction paths in MMC building blocks	17
Figure A.1 – Phase unit of the modular multi-level converter (MMC) in basic half- bridge, two-level arrangement, with submodules	/ <u>1</u> ec- 29
Figure A.2 – Phase unit of the cascaded two-level converter (CTL) in half-bridge form	30
Figure A.3 – Basic operation of the MMC converters	31
Figure A.4 – MMC converters showing composition of valve current	32
Figure A.5 – Phasor diagram showing a.c. system voltage, converter a.c. voltage and converter a.c. current	33
Figure A.6 – Effect of 3 <sup>rd</sup> harmonic injection on converter voltage and current	34
Figure A.7 – Two functionally equivalent variants of a "half-bridge", two-level MMC building block	35
Figure A.8 – Conducting states in "half-bridge", two-level MMC building block	36
Figure A.9 – Typical patterns of conduction for inverter operation (left) and rectifier operation (right), based on the submodule configuration of Figure A.7 a)	37
Figure A.10 – Example of converter with only one MMC building block per valve to illustrate switching behaviour	38
Figure A.11 – Inverter operation example of switching events	38
Figure A.12 – Rectifier operation example of switching events	39
Figure A.13 – Valve current and mean rectified valve current	41
Figure A.14 – IGBT and diode switching energy as a function of collector current	46
Figure A.15 – Valve voltage, current and switching behaviour for a hypothetical MMC valve consisting of 5 submodules	48
Figure A.16 – Power supply from IGBT terminals	53

	- 4 -	IEC 62751-2:2014+AMD1:2019 +AMD2:2023 CSV © IEC 2023
Figure A.17 – Power supply from IGBT t	terminals in cell	54
Figure A.18 – Power supply from d.c. ca	apacitor in submo	dule55
Figure A.19 – One "full-bridge", two-leve	el MMC building b	lock56
Figure A.20 – Four possible variants of t	three-level MMC I	building block57
Table 1 – Contributions to valve losses i	in different operat	ing modes27
Table A.1 – Hard switching events		45
Table A.2 – Soft switching events		
Table A 3 – Summary of switching event	to from Eiguro A	15 40
rabio / Cannary of Switching System	is nom Figure A.	15
Table B.1 – Valve loss data		

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# POWER LOSSES IN VOLTAGE SOURCED CONVERTER (VSC) VALVES FOR HIGH-VOLTAGE DIRECT CURRENT (HVDC) SYSTEMS –

# Part 2: Modular multilevel converters

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In this Redline version, a vertical line in the margin shows where the technical content is modified by amendments 1 and 2. Additions are in green text, deletions are in strikethrough red text. A separate Final version with all changes accepted is available in this publication. International Standard IEC 62751-2 has been prepared by subcommittee 22F: Power electronics for electrical transmission and distribution systems, of IEC technical committee 22: Power electronic systems and equipment.

- 6 -

This publication has been drafted in accordance with the ISO/IEC Directives, Part 2.

A list of all parts in the IEC 62751series, published under the general title *Power losses in voltage sourced converter (VSC) valves for high-voltage direct current (HVDC) systems*, can be found on the IEC website.

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# POWER LOSSES IN VOLTAGE SOURCED CONVERTER (VSC) VALVES FOR HIGH-VOLTAGE DIRECT CURRENT (HVDC) SYSTEMS –

# Part 2: Modular multilevel converters

# 1 Scope

This part of IEC 62751 gives the detailed method to be adopted for calculating the power losses in the valves for an HVDC system based on the "modular multi-level converter", where each valve in the converter consists of a number of self-contained, two-terminal controllable voltage sources connected in series. It is applicable both for the cases where each modular cell uses only a single turn-off semiconductor device in each switch position, and the case where each switch position consists of a number of turn-off semiconductor devices in series (topology also referred to as "cascaded two-level converter"). The main formulae are given for the two-level "half-bridge" configuration but guidance is also given in Annex A as to how to extend the results to certain other types of MMC building block configuration.

The standard is written mainly for insulated gate bipolar transistors (IGBTs) but may also be used for guidance in the event that other types of turn-off semiconductor devices are used.

Power losses in other items of equipment in the HVDC station, apart from the converter valves, are excluded from the scope of this standard.

This standard does not apply to converter valves for line-commutated converter HVDC systems.

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# 2 Normative references

The following documents, in whole or in part, are normatively referenced in this document and are indispensable for its application. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

IEC 60633, Terminology for high-voltage direct-current (HVDC) transmission

IEC 61803, Determination of power losses in high-voltage direct current (HVDC) converter stations

IEC 62747, Terminology for voltage-sourced converters (VSC) for high-voltage direct current (HVDC) systems

IEC 62751-1:2014, Power losses in voltage sourced converter (VSC) valves for high-voltage direct current (HVDC) systems – Part 1: General requirements

ISO/IEC Guide 98-3, Uncertainty of measurement – Part 3: Guide to the expression of uncertainty in measurement (GUM:1995)

# 3 Terms, definitions, symbols and abbreviated terms

For the purposes of this document, the terms and definitions given in IEC 60633, IEC 62747, IEC 62751-1, as well as the following apply.

## 3.1 Terms and definitions

# 3.1.1

# modular multi-level converter

## ММС

multi-level converter in which each VSC valve consists of a number of MMC building blocks connected in series

Note 1 to entry: This note applies to the French language only.

# 3.1.2

## MMC building block

self-contained, two-terminal controllable voltage source together with d.c. capacitor(s) and immediate auxiliaries, forming part of a MMC

# 3.1.3

## **IGBT-diode pair**

arrangement of IGBT and free-wheeling diode connected in inverse parallel

## 3.1.4

#### switch position

semiconductor function which behaves as a single, indivisible switch

Note 1 to entry: A switch position may consist of a single IGBT-diode pair or, in the case of the cascaded two level converter, a series connection of multiple IGBT-diode pairs.

## 3.1.5

# cascaded two-level converter and and siteh.al)

CTL

modular multi-level converter in which each switch position consists of more than one IGBT-diode pair connected in series IEC 62751-22014

Note 1 to entry: This note applies to the French language only.

# 3.1.6

#### submodule

MMC building block where each switch position consists of only one IGBT-diode pair

# 3.1.7

#### cell

MMC building block where each switch position consists of more than one IGBT-diode pair connected in series

#### 3.1.8

#### turn-off semiconductor device

controllable semiconductor device which may be turned on and off by a control signal, for example an IGBT

# 3.1.9

# insulated gate bipolar transistor

#### IGBT

turn-off semiconductor device with three terminals: a gate terminal (G) and two load terminals emitter (E) and collector (C)

Note 1 to entry: This note applies to the French language only.

# 3.1.10 operating state

condition in which the HVDC substation is energized and the converters are de-blocked

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Note 1 to entry: Unlike line-commutated converter, VSC can operate with zero active/reactive power output.

#### 3.1.11

#### no-load operating state

condition in which the HVDC substation is energized but the IGBTs are blocked and all necessary substation service loads and auxiliary equipment are connected

Note 1 to entry: In the no-load state, in principle no switching should occur as the valve is blocked. However, in some designs, it may be necessary to make occasional switching operations to balance voltages between different parts of the converter. Here, some losses may occur and need to be accounted for. The integration time over which such losses are averaged might need to be longer than during normal operation, so as to obtain the correct weighted average of the losses while blocked and the losses while switching.

#### 3.1.12

#### idling operating state

condition in which the HVDC substation is energized and the IGBTs are de-blocked but with no active or reactive power output at the point of common connection to the a.c. network

Note 1 to entry: The "idling operating" and "no-load" conditions are similar but from the no-load state, several seconds may be needed before power can be transmitted, while from the idling operating state, power transmission may be commenced almost immediately (less than 3 power frequency cycles).

Note 2 to entry: In the idling operating state, the converter is capable of actively controlling the d.c. voltage, in contrast to the no-load state where the behavior of the converter is essentially "passive".

Note 3 to entry: Losses will generally be slightly lower in the no-load state than in the idling operating state, therefore this operating mode is preferred where the arrangement of the VSC system permits it.

#### 3.1.13

#### modulation index of PWM converters

М

ratio of the peak line to ground a.c. converter voltage, to half of the converter d.c. terminal to terminal voltage

https://standards.iteh.ai/catalog/standards/jst/
$$M_{c1}^{=0.2751-2:2014}$$
  
 $M_{c275}^{=0.2751-2:2014}$   
 $M_{c10}^{=0.2751-2:2014}$ 

#### where

 $U_{c1}$  is the r.m.s value of the fundamental frequency component of the line-to-line voltage  $U_{c}$ ;

- $U_{\rm c}$  is the output voltage of one VSC phase unit at its a.c. terminal;
- $U_{\rm dc}$   $\;$  is the output voltage of one VSC phase unit at its d.c. terminals.

Note 1 to entry: Some sources define modulation index in a different way such that a modulation index of 1 refers to a square-wave output, which means that the modulation index can never exceed 1. The modulation index according to that definition is given simply by  $M \cdot (\pi/4)$ . However, that definition is relevant mainly to two-level converters using PWM.

#### 3.2 Symbols and abbreviated terms

#### 3.2.1 Valve and simulation data

- *N*<sub>tc</sub> number of MMC building blocks per valve
- *N*<sub>c</sub> number of series-connected semiconductor devices per switch position
- $N_{\rm sr}$  total number of series resistive elements contributing to conduction losses in the valve, other than in the IGBTs and diodes
- *N*<sub>cv</sub> number of d.c. capacitors in the valve
- $N_{\rm s}$  number of switching cycles (on or off) experienced by each VSC value level during the integration time  $t_{\rm i}$
- N<sub>pr</sub> total number of parallel resistive elements contributing to d.c. voltage dependent losses in the valve

- *N*<sub>sn</sub> number of snubber circuits per valve
- *t*<sub>i</sub> integration time used in the simulation

## 3.2.2 Semiconductor device characteristics

- $V_{\rm 0T}$  average IGBT threshold voltage for the relevant operating conditions
- $R_{0T}$  average IGBT slope resistance for the relevant operating conditions, valid at the device terminals
- $V_{0\mathrm{D}}$  average diode threshold voltage for the relevant operating conditions
- $R_{0\mathrm{D}}$  average diode slope resistance for the relevant operating condition, valid at the device terminals
- $E_{\rm on}$  average turn-on energy dissipated in the IGBT for the relevant operating conditions
- $E_{\rm off}$  average turn-off energy dissipated in the IGBT(s) for the relevant operating conditions
- $E_{\text{on},\text{T1}_{j,k}}$  turn-on energy dissipated in IGBT T1 in the *j*<sup>th</sup> MMC building block for the *k*<sup>th</sup> turn-on event for the relevant operating conditions (voltage, current and junction temperature)
- $E_{\text{on,T2}_{j,k}}$  turn-on energy dissipated in IGBT T2 in the  $j^{\text{th}}$  MMC building block for the  $k^{\text{th}}$  turn-on event for the relevant operating conditions (voltage, current and junction temperature)
- $E_{\text{off,T1}_{j,k}}$  turn-off energy dissipated in IGBT T1 in the  $j^{\text{th}}$  MMC building block for the  $k^{\text{th}}$  turn-off event for the relevant operating conditions (voltage, current and junction temperature)
- $E_{\text{off},\text{T2}_j,k}$  turn-off energy dissipated in IGBT T2 in the *j*<sup>th</sup> MMC building block for the *k*<sup>th</sup> turn-off event for the relevant operating conditions (voltage, current and junction temperature)
- $E_{\text{rec,D1}_{j,k}}$  diode recovery energy dissipated in diode D1 in the  $j^{\text{th}}$  MMC building block for the  $k^{\text{th}}$  diode turn-off event for the relevant operating conditions (voltage, current and junction temperature) 62751-2-2014
- $E_{\text{rec},\text{D2}_{j,k}}$  diode recovery energy dissipated in diode D2 in the *j*<sup>th</sup> MMC building block for the *k*<sup>th</sup> diode turn-off event for the relevant operating conditions (voltage, current and junction temperature)

### 3.2.3 Other component characteristics

- $R_{s_k}$  total resistance of the  $k^{th}$  series resistive elements in the valve contributing to other conduction losses
- $R_{dc k}$  resistance of the  $k^{th}$  parallel resistive component in the valve
- $R_{\text{ESR}}$  i average equivalent series resistance of the  $j^{\text{th}}$  d.c. capacitor
- $E_{\text{sn,on}_{j,k}}$  energy dissipated in the snubber resistor of the  $j^{\text{th}}$  snubber circuit for the  $k^{\text{th}}$  turnon event for the relevant operating conditions (voltage, and current where relevant to the design of the snubber)
- $E_{\text{sn,off}_{j,k}}$  energy dissipated in the snubber resistor of the  $j^{\text{th}}$  snubber circuit for the  $k^{\text{th}}$  turnoff event for the relevant operating conditions (voltage, and current where relevant to the design of the snubber)

# 3.2.4 Operating parameters

- $I_{T1av_j}$  mean current of IGBT T1 in the  $j^{th}$  MMC building block, averaged over an integration time  $t_i$
- $I_{\text{T2av}_j}$  mean current of IGBT T2 in the  $j^{\text{th}}$  MMC building block, averaged over an integration time  $t_i$
- $I_{\text{T1rms}_j}$  rms current of IGBT T1 in the  $j^{\text{th}}$  MMC building block, averaged over an integration time  $t_i$

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$I_{\text{T2rms}}$ i	rms	current	of	IGBT	Т2	in	the	j <sup>th</sup>	MMC	building	block,	averaged	over	an
1211110_)	integration time t <sub>i</sub>													

- $I_{D1av_j}$  mean current of diode D1 in the  $j^{th}$  MMC building block, averaged over an integration time  $t_i$
- $I_{\text{D2av}_j}$  mean current of diode D2 in the  $j^{\text{th}}$  MMC building block, averaged over an integration time  $t_i$
- $I_{D1rms_j}$  rms current of diode D1 in the  $j^{th}$  MMC building block, averaged over an integration time  $t_i$
- $I_{\text{D2rms}_j}$  rms current of diode D2 in the  $j^{\text{th}}$  MMC building block, averaged over an integration time  $t_i$
- $I_{\rm rms\_k}$  rms current flowing in the  $k^{\rm th}$  series resistive element for the relevant operating conditions
- $U_{
  m rms\_k}$  rms value (including d.c. component) of the voltage across the  $k^{
  m th}$  parallel resistive component in the valve
- $I_{\text{crms } i}$  rms current flowing in the  $j^{\text{th}}$  d.c. capacitor of the valve
- $P_{\text{GU}\ i,k}$  average power input to the power supply of  $k^{\text{th}}$  IGBT in  $j^{\text{th}}$  MMC building block
- $p_{\mathrm{GU}_{j,k}}(t)$  instantaneous power input to the power supply of  $k^{\mathrm{th}}$  IGBT in  $j^{\mathrm{th}}$  MMC building block
- $u_{\text{GU}_{j,k}}(t)$  instantaneous voltage input to the power supply of  $k^{\text{th}}$  IGBT in  $j^{\text{th}}$  MMC building block
- $i_{\text{GU}_{j,k}}(t)$  instantaneous current input to the power supply of  $k^{\text{th}}$  IGBT in  $j^{\text{th}}$  MMC building block

 $P_{\text{GU},i}$  average power input to the power supply in  $j^{\text{th}}$  MMC building block

- $p_{\text{GU}}(t)$  instantaneous power input to the power supply in  $j^{\text{th}}$  MMC building block
- $u_{\text{GU},i}(t)$  instantaneous voltage input to the power supply in *j*<sup>th</sup> MMC building block

 $i_{\rm GU}(t)$  /stan instantaneous current input to the power supply in j<sup>th</sup> MMC building block / icc-

# 3.2.5 Loss parameters

- $P_{\rm V2}$  diode conduction losses
- $P_{V3}$  other valve conduction losses
- *P*<sub>V4</sub> d.c. voltage-dependent losses
- $P_{\rm V5}$  d.c. capacitor losses
- P<sub>V6</sub> IGBT switching losses
- $P_{\rm V7}$  diode turn-off losses
- $P_{\rm V8}$  snubber losses
- $P_{V9}$  valve electronics power consumption
- $P_{\rm Vt}$  total valve losses

# 4 General conditions

# 4.1 General

Modular multi-level converters (MMC) are a family of converters in which each valve forms a controllable voltage source. The converter a.c. voltage is synthesized by switching large numbers of relatively small, self-contained, two-terminal controllable voltage sources at different times, thereby obtaining a high-quality converter waveform with low switching losses and therefore a high overall efficiency. The MMC building blocks from which the overall converter is built up may use multiple IGBT-diode pairs connected in series (in which case the converter is referred to as the "Cascaded two level converter", CTLC) or only a single IGBT-