

### **IEC TR 63127**

Edition 1.1 2024-04 CONSOLIDATED VERSION

# TECHNICAL REPORT



Guideline for the system design of HVDC converter stations with linecommutated converters

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IEC TR 63127:2019

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### CONTENTS

FOREWORD......6

| 11 | NTRODU | JCTION   | 8                     |  |
|----|--------|--|-----------------------|--|
| 1  | Scop   | oe   | 9                     |  |
| 2  | Norn   | native references  | 9                     |  |
| 3  | Term   | Terms and definitions  |                       |  |
| 4  | Svm    | 10   |                       |  |
|    | 4.1    | bols   |                       |  |
|    | 4.2    | Subscripts   |                       |  |
| 5  |        | view of HVDC system design                                   |                       |  |
|    | 5.1    | General  |                       |  |
|    | 5.2    | Formulation of system design                                 |                       |  |
|    | 5.2.1  | · · · · · · · · · · · · · · · · · · ·                        |                       |  |
|    | 5.2.2  | - ,  |                       |  |
|    | 5.2.3  | •  |                       |  |
|    | 5.2.4  |  |                       |  |
|    | 5.2.5  |  |                       |  |
|    | 5.2.6  |  |                       |  |
|    | 5.2.7  | -  |                       |  |
|    | 5.3    | System studies and simulations                               |                       |  |
| 6  | Dete   | rmination of design conditions and requirements              |                       |  |
|    | 6.1    | Environmental conditions and requirements                    |                       |  |
|    | 6.2    | DC transmission line (cable) and earth electrode             |                       |  |
|    | 6.2.1  |  |                       |  |
|    | 6.2.2  |  |                       |  |
|    | 6.2.3  |  |                       |  |
|    | 6.3    | AC system conditions   | ec-tr-63127-201<br>18 |  |
|    | 6.3.1  | -  |                       |  |
|    | 6.3.2  |  |                       |  |
|    | 6.3.3  | Relevant AC system protection                                | 19                    |  |
|    | 6.3.4  |  |                       |  |
|    | 6.3.5  | Short-circuit current or capacity                            | 20                    |  |
|    | 6.3.6  | AC bus voltage   | 21                    |  |
|    | 6.3.7  | AC system frequency  | 21                    |  |
|    | 6.3.8  | Pre-existing harmonic and negative sequence voltage          | 22                    |  |
|    | 6.4    | Requirements for HVDC systems arising from AC/DC interaction | 22                    |  |
|    | 6.5    | AC system equivalents  | 23                    |  |
|    | 6.5.1  | General  | 23                    |  |
|    | 6.5.2  | Equivalent for AC/DC system dynamic or transient simulation  | 23                    |  |
|    | 6.5.3  | Impedance equivalent for AC filter design                    | 24                    |  |
|    | 6.5.4  | System equivalent for low order harmonic resonance study     | 26                    |  |
| 7  | Main   | Main circuit design  |                       |  |
|    | 7.1    | Ratings  | 26                    |  |
|    | 7.1.1  | Rated power  | 26                    |  |
|    | 7.1.2  | Rated voltage  | 27                    |  |
|    | 7.1.3  | Rated current  | 28                    |  |
|    | 7.2    | Configurations   | 28                    |  |

| ○         | o _ o             |   |                          |
|-----------|-------------------|---|--------------------------|
| 7         | 7.2.1             | Pole and return path  | 28                       |
| 7         | 7.2.2             | Converter topology  | 29                       |
| 7         | 7.2.3             | DC switchyard configuration   | 30                       |
| 7         | 7.2.4             | Reactive power equipment  | 38                       |
| 7.3       | 3 Det             | ermination of main circuit parameters   | 38                       |
| 7         | 7.3.1             | General   | 38                       |
| 7         | 7.3.2             | Control strategy  | 39                       |
| 7         | 7.3.3             | Tolerances and errors   | 40                       |
| 7         | 7.3.4             | Determination of converter transformer impedance  | 40                       |
| 7         | 7.3.5             | Relative inductive voltage drop $(d_{XN})$ and relative resistive voltage drop $(d_{rN})$ | 40                       |
| -         | 7.3.6             | Ideal no-load DC voltage  |                          |
|           | 7.3.7             | DC voltage and DC current   |                          |
| -         | 7.3.8             | Rated capacity of converter transformer   |                          |
|           | 7.3.9             | Converter transformer taps  |                          |
|           | 7.3.10            | Inductance of smoothing reactor   |                          |
| 8 I       | Insulation        | n coordination  |                          |
|           |                   | sign  |                          |
| 9.        |                   | neral   |                          |
| 9.<br>9.2 |                   |   |                          |
| 9.2       | 2 AC              | filter design   | 45<br>45                 |
| 9.4       |                   | ver line carrier (PLC) filters  |                          |
| 9.        | 5 Pa              | dio frequency interference (RFI)  | 46                       |
|           |                   |   |                          |
| 10 1      | 1 000             | power compensation and controlneral   | 47                       |
|           |                   |   |                          |
|           | 10.2.1            | active power consumption  |                          |
|           |                   | Maximum reactive power consumption4547-949-9407-3339-432/iec-tr-                          | 47<br>631 <b>70</b> -201 |
|           | 10.2.3            | Minimum reactive power consumption  |                          |
|           |                   | rermination of reactive power equipment capacity  |                          |
|           | 7.5 Det<br>10.3.1 | General   |                          |
|           | 10.3.1            | Capacity of reactive power supply equipment   |                          |
|           | 10.3.2            | Capacity of reactive power absorption equipment   |                          |
|           | 10.3.4            | Sizing of reactive power sub-bank   |                          |
|           | 10.3.4            | Sizing of reactive power sub-bank   |                          |
|           |                   | active power control  |                          |
|           | 7.4 Rea<br>10.4.1 | General   |                          |
|           | 10.4.1            | Reactive power exchange control/voltage control   |                          |
|           | 10.4.2            | Voltage limitation  |                          |
|           |                   | nporary overvoltage control   |                          |
|           |                   | rameters of main equipment  |                          |
|           | •                 | neral   |                          |
|           |                   |   |                          |
|           |                   | rverter valves  |                          |
|           | 11.2.1            | General   |                          |
|           | 11.2.2            | Valve hall environment  |                          |
|           | 11.2.3            | Current rating  |                          |
|           | 11.2.4            | Voltage rating  |                          |
|           | 11.2.5            | Losses of converter valves  |                          |
| •         | 11.2.6            | Testing requirements  | 53                       |

| 11.3.  | Converter transformers  | 53   |
|--|---|--|
|  | 1 General   | 53   |
| 11.3.  | 2 Current rating  | 54   |
| 11.3.  | 3 Voltage rating  | 54   |
| 11.3.  | 4 Other rating  | 54   |
| 11.3.  | 5 Rated loss  | 54   |
| 11.3.  | 6 Test requirements   | 55   |
| 11.4   | Smoothing reactor   | 55   |
| 11.4.  | 1 General   | 55   |
| 11.4.  | 2 Current ratings   | 55   |
| 11.4.  | 3 Voltage rating  | 56   |
| 11.4.  | 4 Other ratings   | 56   |
| 11.4.  | 5 Losses  | 56   |
| 11.4.  | -   |  |
|  | Wall bushings   | 56   |
| 11.5.  |   |  |
| 11.5.  | 3   |  |
| 11.5.  | 5 5   |  |
| 11.5.  | 5 1   |  |
|  | AC and DC filter equipment  |  |
| 11.7   | PLC filter equipment  |  |
| 11.8   | Other equipment in DC yard  | 57   |
|  | informative) Typical control, measurement and equipment manufacturing in HVDC systems | 5.9  |
|  | D A D   |  |
| •  | informative) Technical parameters for equipment specification                         |  |
| B.1  | Converter valve   |  |
| D 0  |   |  |
| B.2  | Converter transformer   | 61   |
| ://stB.3ard  | Smoothing reactor   | 61<br>62-2                                     |
| ://stB.3ard  |   | 61<br>62-2                                     |
| ://s(B.3ard<br>Bibliograp  | Smoothing reactor   | 61<br>62 2<br>63                               |
| Bibliograp   | Smoothing reactor   | 61<br>162-2<br>63                              |
| Bibliograp   | Smoothing reactor   | 61<br>162-2<br>63                              |
| Bibliograp  Figure 1 -  Figure 2 -   | Smoothing reactor   | 61<br>62-2<br>63<br>12                         |
| Bibliograph<br>Figure 1 -<br>Figure 2 -<br>Figure 3 -  | Smoothing reactorhy   | 61<br>62-2<br>63<br>12<br>22<br>25             |
| Figure 1 - Figure 2 - Figure 3 - Figure 4 -  | Smoothing reactor   | 61<br>62-2<br>63<br>12<br>22<br>25             |
| Figure 1 - Figure 3 - Figure 4 - Figure 5 -  | Smoothing reactor   | 61<br>62-2<br>63<br>12<br>22<br>25<br>25       |
| Figure 1 - Figure 3 - Figure 4 - Figure 5 - Figure 6 -   | Smoothing reactor   | 61<br>62-2<br>63<br>12<br>25<br>25<br>26<br>30 |
| Figure 1 - Figure 2 - Figure 3 - Figure 4 - Figure 5 - Figure 6 - Figure 7 -   | Smoothing reactor   | 61<br>62-2<br>63<br>12<br>22<br>25<br>26<br>30 |
| Figure 1 - Figure 2 - Figure 3 - Figure 5 - Figure 6 - Figure 7 - Figure 8 -   | Smoothing reactor   | 6162-263122525263033                           |
| Figure 1 - Figure 2 - Figure 3 - Figure 5 - Figure 6 - Figure 7 - Figure 8 - Figure 9 -  | Smoothing reactor   | 6163122525303333                               |
| Figure 1 - Figure 2 - Figure 3 - Figure 5 - Figure 6 - Figure 7 - Figure 8 - Figure 9 - Figure 10                              | Smoothing reactor   | 6162-263122525303334                           |
| Figure 1 - Figure 2 - Figure 3 - Figure 5 - Figure 6 - Figure 7 - Figure 8 - Figure 9 - Figure 10                              | Smoothing reactor   | 6162-263122525303334                           |
| Figure 1 - Figure 2 - Figure 3 - Figure 5 - Figure 6 - Figure 8 - Figure 9 - Figure 10 Figure 11                               | Smoothing reactor   | 616312252530333434                             |
| Figure 1 - Figure 2 - Figure 3 - Figure 5 - Figure 6 - Figure 7 - Figure 8 - Figure 9 - Figure 10 Figure 11 Figure 12          | Smoothing reactor   | 6162-2631225263033343435                       |
| Figure 1 - Figure 2 - Figure 3 - Figure 5 - Figure 6 - Figure 8 - Figure 9 - Figure 10 Figure 11 Figure 12 Figure 13           | Smoothing reactor   | 6163122525303334343535                         |
| Figure 1 - Figure 2 - Figure 3 - Figure 5 - Figure 6 - Figure 7 - Figure 9 - Figure 10 Figure 11 Figure 12 Figure 13 Figure 14 | Smoothing reactor   | 6162-263122525303334353536                     |

| IEC TR 63127:2019+AMD1:2024 CSV<br>© IEC 2024 | <b>-</b> 5 <b>-</b> | REDLINI              | E VERSION |
|---|---------------------|----------------------|-----------|
| Table 1 – Studies and simulations in HVD      | C system desigr     | 1                    | 15        |
| Table 2 – Preferred rated voltages for ove    | erhead line HVD0    | C power transmission | 27        |
| Table 3 – Preferred rated voltages for sub    | marine HVDC p       | ower transmission    | 28        |
| Table A.1 – Tolerance for main circuit calc   | culation            |                      | 58        |
| Table A.2 – Control parameters for main of    | circuit calculation | ١                    | 58        |

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### INTERNATIONAL ELECTROTECHNICAL COMMISSION

## GUIDELINE FOR THE SYSTEM DESIGN OF HVDC CONVERTER STATIONS WITH LINE-COMMUTATED CONVERTERS

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IEC TR 63127 edition 1.1 contains the first edition (2019-06) [documents 115/195/DTR and 115/203/RVDTR] and its amendment 1 (2024-04) [documents 115/361/DTR and 115/364/RVDTR].

In this Redline version, a vertical line in the margin shows where the technical content is modified by amendment 1. Additions are in green text, deletions are in strikethrough red text. A separate Final version with all changes accepted is available in this publication.

**-7-**

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IEC TR 63127, which is a Technical Report, has been prepared by IEC technical committee 115: High Voltage Direct Current (HVDC) transmission for DC voltages above 100 kV.

This document has been drafted in accordance with the ISO/IEC Directives, Part 2.

The committee has decided that the contents of this document and its amendment will remain unchanged until the stability date indicated on the IEC website under webstore.iec.ch in the data related to the specific document. At this date, the document will be

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### INTRODUCTION

HVDC is an established technology that has been in commercial use for more than 60 years. With the changes in demands due to evolving environmental needs, installation of HVDC systems has increased dramatically in the last 30 years and almost more than half of HVDC projects were commissioned after the year 2000. HVDC has become a common tool in the design of future global transmission systems.

HVDC systems transmit more electrical power over longer distances than a similar alternating current (AC) transmission system, which means fewer transmission lines are needed, saving both money and land and simplifying permissions. In addition to significantly lowering electrical losses over long distances, HVDC transmission is also very stable and easily controlled, and can stabilize and interconnect AC power networks that are otherwise incompatible. Typically line-commutated converter (LCC) HVDC systems provide unique or superior capabilities in the following aspects:

- long distance bulk power transmission;
- asynchronous interconnections;
- · long distance cable;
- · controllability;
- lower losses;
- environmental concerns;
- limitation of short-circuit currents.

Simply due to these technical merits, the market demand for HVDC transmission technology is spreading widely over the world. There are many HVDC power transmission systems with a DC voltage from 50 kV up to 660 1 100 kV in different countries. In addition, there are several ±800 kV HVDC power transmission systems which have been built or operated or which are under construction in China, India and Brazil. In 2016, one ±1 100 kV HVDC power transmission system project was started in China.

The fast development of the HVDC power transmission and distribution industry has been accompanied by IEC standardization work. More than 40 IEC documents, from DC equipment to DC systems, have been published. Among these, the IEC TR 60919 series, IEC 60633, IEC 60071-5, the IEC TR 62001 series and the IEC 60700 series provide essential information for the design and operation of HVDC power transmission systems.

However, this document provides only a basic guide and refers to typical numbers and examples. Other points and values may also be valid in particular cases and should also be considered accordingly.

### GUIDELINE FOR THE SYSTEM DESIGN OF HVDC CONVERTER STATIONS WITH LINE-COMMUTATED CONVERTERS

### 1 Scope

System design is the basis of construction and operation of HVDC systems. It defines the overall philosophy for the HVDC transmission system and enables the ratings and specifications for the equipment integrated in the project.

This document focuses on the system design of converter stations. It is applicable to point-to-point and back-to-back HVDC systems based on line-commutated converter (LCC) technology.

This document provides guidance and supporting information on the procedure for system design and the technical issues involved in the system design of HVDC transmission projects for both purchaser and potential suppliers. It can be used as the basis for drafting a procurement specification and as a guide during project implementation.

### 2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

IEC 60633, High-voltage direct current (HVDC) transmission – Vocabulary

### 3 Terms and definitions

For the purposes of this document, the terms and definitions given in IEC 60633 apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- IEC Electropedia: available at http://www.electropedia.org/
- ISO Online browsing platform: available at http://www.iso.org/obp

### **Symbols**

| 4.1 Letter symbols for varia |
|------------------------------|
|------------------------------|

DC voltage between the pole and the neutral bus at the line side of the smoothing  $U_{\mathsf{d}}$ reactor DC voltage of pole line to ground at the measuring point  $U_{\mathsf{dl}}$  $I_{\mathsf{d}}$ DC current  $U_{\rm dmeas}$ measured DC voltage power setting at the line side of the smoothing reactor in the rectifier station  $P_{\mathsf{ref}}$ commutation reactance, including converter transformer reactance and other  $X_{\mathsf{t}}$ reactance in the commutation circuit that will affect the commutation process on-load losses of converter transformer and smoothing reactor when a six-pulse  $P_{II}$ converter is operating at rated capacity equivalent resistance of the voltage drop of the thyristor valve (current dependent  $R_{\mathsf{th}}$ resistance of the thyristors) ideal no-load DC voltage of six-pulse converter  $U_{\mathsf{dio}}$  $U_{\mathbf{k}}$ relative converter transformer inductive voltage drop (short-circuit reactance) relative voltage drop of AC PLC filter reactors  $U_{\mathsf{plc}}$ relative inductive DC voltage drop of converter  $d_{\mathsf{X}}$ relative resistance DC voltage drop of converter  $d_{\mathsf{r}}$ forward voltage drop of converter valve under conducting state  $U_{\mathsf{T}}$ total relative inductive DC voltage drop of converter – contains both commutation  $d_{\mathsf{xtotR}}$ circuit reactance and the system impedance converted onto valve side active power of converters  $P_{\mathsf{dc}}$ reactive power consumption of individual converter  $Q_{\mathsf{conv}}$ reactive power supplied by filters  $Q_{\mathsf{f}}$ short-circuit capacity of AC bus SSC total resistance of DC transmission line at each pole  $R_{\mathsf{d}}$ resistance of electrode  $R_{e}$  $R_{\mathsf{q}}$ resistance of electrode line rated capacity of a three-phase converter transformer connected to a six-pulse  $S_{\mathsf{n}}$ valve group rated capacity of a single-phase three-winding converter transformer connected  $S_{n3w}$ to a 12-pulse valve group rated capacity of a single-phase two-winding converter transformer connected to  $S_{\mathsf{n2w}}$ a 12-pulse valve group valve side line voltage of converter transformer  $U_{\mathbf{v}}$ valve side line current of converter transformer  $I_{\mathsf{V}}$ line voltage of line side of converter transformer  $U_{\mathsf{I}}$ rated ratio of converter transformer at normal tap position  $n_{\mathsf{nom}}$ needed OLTC range of converter transformer η step size of converter transformer OLTC Δη total inductance from DC side  $L_{\mathsf{d}}$ smoothing reactor inductance  $L_{\mathsf{dr}}$ 

converter transformer inductance per phase

overlap angle

 $L_{\mathsf{tr}}$ μ

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delay angle  $\alpha$ extinction angle γ  $Q_{\mathsf{total}}$ 

 $Q_{\mathsf{sb}}$ 

total reactive power supplied by AC filters and shunt capacitors at normal voltage

reactive power supplied by the largest AC filter or shunt capacitor sub-bank at

normal voltage

 $Q_{\mathsf{ac}}$ reactive power supplied by AC system (negative value means the capability to

supply reactive power by AC system)

reactive power consumption of converters  $Q_{\mathsf{dc}}$ 

voltage correction factor, normally 0,95 to 1,05  $K_{\mathsf{v}}$ 

total reactive power absorbed by the shunt reactors of converter station at normal  $Q_{\mathsf{r}}$ 

AC voltage

capacity of the minimum filter combination which shall be switched in to meet the  $Q_{\mathsf{fmin}}$ 

harmonic performance requirement at normal AC voltage

 $\Delta U_{AC}$ dynamic voltage change because of sub-bank switching

reactive power capacity of the filter or shunt capacitor sub-bank to be switched  $Q_{\mathsf{filter}}$ 

reactive power capacity of the filter or shunt capacitor sub-banks in operation  $\sum Q_{\text{filter}}$ 

after switching

change of reactive power consumption of converters due to sub-bank switching.  $\Delta Q_{dc}$ 

which sometimes can be ignored

#### **Subscripts** 4.2

normal value of the variables Ν

value of rectifier side S://standards.iteh.ai) R

value of inverter side

ument Preview max maximum value of the variable minimum value of the variable min

### 5 Overview of HVDC system design

#### 5.1 General

In implementing HVDC projects, the purchaser or the supplier will do preliminary system design work to prepare the various required documents needed by the project. Specific studies and simulations are conducted during the system design to find the optimal project schemes and to demonstrate performance. As a minimum, the following main system features should be determined:

- **HVDC** system ratings;
- HVDC system operation configurations and control modes;
- reactive power compensation and control;
- harmonic filtering;
- AC/DC interaction and control;
- insulation coordination;
- environmental impacts, such as audible noise, electromagnetic fields, etc.

The system design may be conducted in several phases by different parties, such as purchaser or supplier, during planning, bidding, detailed design stages, for example, as shown in Figure 1. Different tools and models may be introduced in the system design because of different targets or designs at each stage. One should be very careful to adopt the tools and models in a coordinated manner.

A functional specification for the project is usually prepared by the purchaser before the detailed design. It may consist of project objectives and conditions, grid codes, targeted system performance requirements and operation regulations, etc. This functional specification should be treated as both providing inputs and the guide for the system design of an HVDC project. Because the final technology solution is undefined before the detail design stage, it is always necessary to reserve adequate space in the functional specification for further optimization. The owner will issue the specification as a document for bidding if this is a turn-key project. After evaluation of bidding for the specific technology solution, especially for HVDC control, the owner may choose the appropriate solution. Thus, the system features listed above will be studied in more detail based on the chosen technology solution and some additional studies and surveys usually need to be performed to finalize the system design. Finally, all the equipment ratings and specifications will be prepared.

The flowchart of an HVDC system design is summarized in Figure 1.

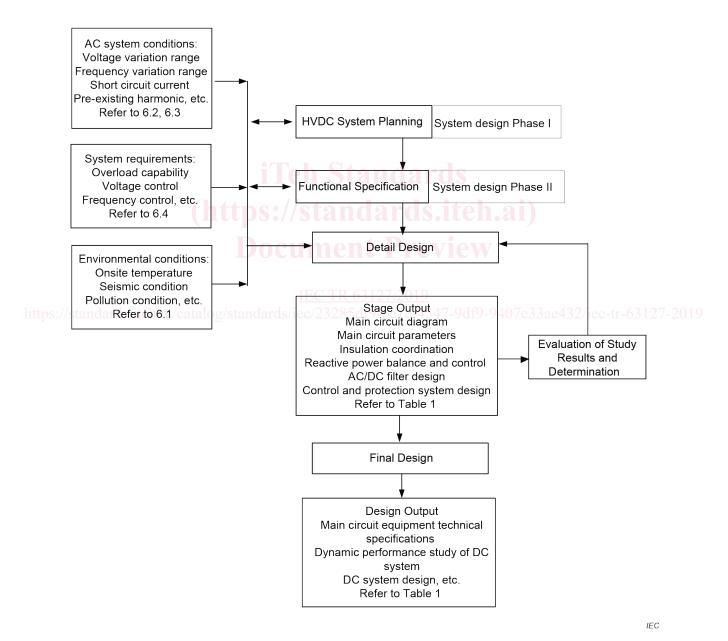


Figure 1 - System design in an HVDC project