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Elektromagnetna združljivost (EMC) - 4-3. del: Preskusne in merilne tehnike -Preskušanje odpornosti proti sevanim radiofrekvenčnim elektromagnetnim poljem

Electromagnetic compatibility (EMC) - Part 4-3: Testing and measurement techniques - Radiated, radio-frequency, electromagnetic field immunity test

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### 77B/530/CDV



#### COMMITTEE DRAFT FOR VOTE (CDV) PROJET DE COMITÉ POUR VOTE (CDV)

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Also of interest to the following committees				Supersedes document			
Intére	sse également les comités suivant	Remplace le document					
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Titre : Amendement 1 à la CEI 61000-4-3 édition Title : Amendment 1 to IEC 61000-4-3 edition 3: 3: Etalonnage des sondes de champs Calibration of E-field probes électriques

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#### SIST EN 61000-4-3:2006/A1:2008

#### Note d'introduction https://standards.iteh.ai/catalog/staIntroductory.noteo74e6a-8a1b-4363-9297-

Pour des fréquences supérieures à plusieurs centaines de MHz jusqu'à la gamme des GHz, l'utilisation d'antennes cornet à gain standard, dans le but d'établir un champ standard à l'intérieur d'une chambre anéchoïque, est une des méthodes les plus largement répandue afin d'étalonner des sondes pour des applications selon la CEI 61000-4-3. Cependant, il y a un manque de méthode établie pour la validation de l'environnement d'essai pour les étalonnages des sondes de champ.

En utilisant cette méthode, des différences ont été observées entre laboratoires d'étalonnage, au-delà des incertitudes de mesure qu'ils rapportent également.

Les étalonnages entre 80 MHz et quelques centaines de MHz de sondes de champ qui sont habituellement réalisés dans des guides d'onde TEM sont généralement plus reproductibles.

L'Annexe informative L à la CEI 61000-4-3 se concentre par conséquent sur l'amélioration des

For frequencies above several hundreds megahertz to gigahertz range, using standard gain horn antennas to establish a standard field inside an anechoic chamber is one of the most widely used method for calibrating probes for IEC 61000-4-3 applications. However, there is a lack of established method for validating the test environment for field probe calibrations.

In using this method, differences have been observed between calibration laboratories, also beyond their reported measurement uncertainties.

Field probe calibrations in 80 MHz to a few hundred megahertz that are usually carried out in TEM waveguides are generally found to be more reproducible.

Informative Annex L to IEC 61000-4-3 therefore concentrates in improving the probe calibration procedures with horn antennas in anechoic chambers to which a comprehensive calibration procedure is depicted.

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procédures d'étalonnage de sondes, avec des antennes cornet dans des chambres anéchoïques, pour lesquelles une procédure d'étalonnage complète est décrite.

Pour plus de complétude, l'Article L.5 a été ajouté afin de décrire brièvement d'autres méthodes comme celle concernant les cellules TEM. Cependant, les détails des procédures et de validation de l'environnement ne sont pas incluses, du fait que les méthodes de test établies les utilisant, n'ont pas été considérées comme présentant le même intérêt. For the sake of completeness, Clause L.5 has been added to briefly describe other methods such as that concerning TEM cells. However, the details in procedures and validation of the environment are not included as the established test methods using them have not been found to be of such concern.

#### ATTENTION VOTE PARALLÈLE CEI – CENELEC

L'attention des Comités nationaux de la CEI, membres du CENELEC, est attirée sur le fait que ce projet de comité pour vote (CDV) de Norme internationale est soumis au vote parallèle.

Un bulletin de vote séparé pour le vote CENELEC leur sera envoyé par le Secrétariat Central du CENELEC.

ATTENTION IEC – CENELEC PARALLEL VOTING IEC National Committe

The attention of IEC National Committees, members of CENELEC, is drawn to the fact that this Committee Draft for Vote (CDV) for an International Standard is submitted for parallel voting. A separate form for CENELEC voting will be sent to them by the CENELEC Central Secretariat.

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#### Annex L (Informative)

#### Calibration method for E-field probes

#### L.1 Introduction

E-field probes with broad frequency range and large dynamic response are extensively used in the field uniformity calibration procedures in accordance to IEC 61000-4-3. Among other aspects, the quality of the field probe calibration directly impacts the uncertainty budget of a radiated immunity test.

Generally, probes are subject to relatively low field strengths, e.g. 1 V/m - 30 V/m, during the field uniformity calibration in accordance with IEC 61000-4-3. Therefore a calibration of the E-field probes used within IEC 61000-4-3 shall take the intended frequency and dynamic ranges into consideration.

Currently probe calibration results may show differences when the probe is calibrated in different calibration laboratories. Therefore environment and method for field probe calibration are to be specified. This annex gives the chamber validation procedures to be used for probe calibration and provides relevant information on calibration of probes to be used in the IEC 61000-4-3 field uniformity measurements in order to limit these differences in calibration results.

#### L.2 Probe calibration requirements

#### L.2.1 General

The calibration of E-Field probes intended to be used for UFA calibration procedure as defined in IEC 61000-4-3 shall satisfy the following requirements.

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L.2.2 Calibration Frequency Range atalog/standards/sist/77b74e6a-8a1b-4363-9297-

The frequency range shall normally cover 80 MHz to 6 GHz but it may be limited to the frequency range required by the tests.

#### L.2.3 Frequency steps

To be able to compare test results between different calibration laboratories, it is necessary to use fixed frequencies for the calibration.

80 MHz to 1 GHz: Use the following frequencies for the calibration of E-field probes (typically 50 MHz step width) 80, 100, 150, 200,..., 950, 1000 MHz

1 GHz to 6 GHz:

Use the following frequencies for the calibration of E-field probes (200 MHz step width) 1000, 1200, 1400,..., 5800, 6000 MHz

#### L.2.4 Field Strength

The field strength at which a probe is calibrated should be based on the field strength required for the immunity test. As the preferred method for uniformity field calibration is carried out at field strength of at

The National Committees are requested to note that for this publication the maintenance result date is 2009.

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least 1,8 times the field strength to be applied to the EUT, it is recommended that the probe calibration be carried out at twice the test field strength which also covers the 1 dB compression requirement of the power amplifier.

Calibration Level	Calibration Field Strength				
1	2 V/m				
2	6 V/m				
3	20 V/m				
4	60 V/m				
Х	Y V/m				
NOTE - X,Y is an open calibration level. This level may be given in the product specification or test laboratory.					

#### Table L1 - Calibration field strength level

#### L.3 Requirements for calibration instrumentation

#### L.3.1 Harmonics and Spurious Signals

Any harmonics or spurious signals from the power amplifiers shall be at least 20 dB below the level at the carrier frequency. This is required for all field strength levels used during calibration and linearity check. Since the harmonic content of power amplifiers is usually worse at higher power levels, the harmonic measurement may be performed only at the highest calibration field strength. The harmonic measurement can be performed using a calibrated spectrum analyzer which is connected to the amplifier output through an attenuator, or through a directional coupler.

Calibration laboratories shall perform a measurement to validate that the harmonic and/or spurious signals from the amplifier satisfy the requirements for all measurement setups. This may be done by connecting a spectrum analyzer to Port 3 of the directional coupler (replacing the power meter sensor with the spectrum analyzer input – see Figure L.2).

Note - It should be assured that the power level does not exceed the maximum allowable input power of the spectrum analyzer. An attenuator may be used.

The frequency span shall cover at least the third harmonic of the intended frequency. The validation measurement shall be performed at the power level that will generate the highest intended field strength.

Harmonic suppression filters may be used to improve the spectrum purity of the power amplifier(s) (see Annex K).

#### L.3.2 Linearity Check for Probe

The linearity of the probe which is used for the chamber validation according to L.4.2.5 shall be within  $\pm 0.5$  dB from an ideal linear response in the required dynamic range. Linearity shall be confirmed for all intended range settings if the probe has multiple ranges or gain settings.

In general probe linearity does not change significantly with frequency. Linearity checking can be performed at a spot frequency that is close to the central region of the intended use of frequency range, and where the probe response versus frequency is relatively flat. The selected spot frequency is to be documented in the calibration certificate.

The field strength for which the linearity of the probe is measured should be within -6 dB to +6 dB of the field strength which is used during the validation of the chamber, with a step size of 1 dB. Table L2 shows an example of the field strength levels to be checked for an 20 V/m application.



Table L2 - Example for the probe linearity check





#### L.3.3 Determination of the gain of the Standard Horn antennas

Far field gain of the standard pyramidal horn antennas can be determined fairly accurately (less than 0,1 dB of uncertainties have been reported in [1]). The far-field gain is typically valid for distances greater

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than  $8D^2/\lambda$  (where D is the largest dimension of the horn aperture, and  $\lambda$  is the wavelength). Calibrations of field probes at such distances may not be practical due to the large anechoic chamber and high power amplifiers required. Field probes are typically calibrated in the near field region of the transmitting antennas. The near-field gain of standard gain horn antennas have been determined by using equations such as those described in [2]. The gain is computed based on the physical dimensions of a standard pyramidal horn, and by assuming a quadratic phase distribution at the horn aperture. The gain determined in such a manner may be inadequate for use in performing the chamber VSWR test and the subsequent probe calibrations.

The equations (as given in [2]) were derived using aperture integration by assuming that no reflection occurs at the aperture of the horn and that the field incident on the aperture is a  $TE_{10}$  mode but with a quadratic phase distribution across the aperture. Some approximations were applied during the integration to obtain the close form result. Other effects such as multiple reflections from the horn edge, and higher order modes at the aperture are not accounted for. Depending on the frequency and horn design, the error is generally in the order of  $\pm$  0,5 dB, but can be larger.

For better accuracy, a numerical method using full wave integration can be used. For example, the uncertainties in the gain calculation by a numerical method can be reduced to less than 5 % <sup>[3]</sup>.

The gain of a horn antenna can also be determined experimentally. For example, the gain can be determined at reduced distances with a three-antenna method by an extrapolation technique, such as that described in [4], or some variations of the method.

It is recommended that the distance between the horn antenna and the probe under test be at least  $0.5D^2/\lambda$  during the calibration. Large uncertainties in determining gains can result from a closer distance. The standing waves between the antenna and the probe can also be large for closer distances, which again would result in large measurement uncertainties in the calibration.

### L.4 Field probe calibration in anechoic chambers<sup>1/77b74e6a-8a1b-4363-9297-</sup>

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#### L.4.1 Calibration environments

The probe calibration should be performed in a Fully Anechoic Room (FAR) or in a Semi-Anechoic Chamber with absorbers on the ground plane which satisfies the requirement of L.4.2.

When a FAR is used, the recommended minimum size of the FAR internal working volume for the probe calibration is 5 m (D) x 3 m (W) x 3 m (H). Note: For frequencies above several hundreds MHz, using standard gain horn antennas to establish a standard field inside an anechoic chamber is one of the most widely used methods for calibrating field probes for IEC 61000-4-3 applications. At lower frequencies, such as 80 MHz to several hundreds MHz, the use of an anechoic chamber may not be practical. So the field probe may be calibrated in other facilities also used for immunity tests against electromagnetic fields. Therefore, TEM waveguides etc. are included in this annex as alternative calibration environments for these lower frequencies.

The system and the environment used for probe calibration shall meet the following requirements.

#### L.4.2 Validation of anechoic chambers for field probe calibration

The probe calibration measurements assume a free space environment. A chamber VSWR test using a field probe shall be performed to determine whether it is acceptable for subsequent probe or sensor calibration. The validation method characterizes the performance of the chamber and absorbing material.

Each probe has a specific volume and physical size, for example the battery case and/or the circuit board. In other calibration procedures, a spherical quiet zone is guaranteed in the calibration volume. The

specific requirements of this annex concentrate on a VSWR test for test points located at the antenna beam axes.

Test fixtures and their influences (such as the fixtures to hold the probe, which may be exposed to electromagnetic fields and interfere with the calibration) cannot be entirely evaluated. A separate test is required to validate the influences of the fixtures.

#### L.4.2.1 Measuring Net Power to a Transmitting Device using Directional Couplers

Net power delivered to a transmitting device can be measured with a 4-port bi-directional coupler, or two 3-port single directional couplers connected back-to-back (forming the so-called "dual directional coupler"). A common setup using a bi-directional coupler to measure the net power to a transmitting device is shown in Figure L2.



Figure L2 – Setup for measuring net power to a transmitting device

The forward coupling and reverse coupling are defined as (when all other ports are terminated with matched loads):

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$$C_{fwd} = \frac{P_1}{P_3} \times \frac{P_2}{P_1}$$
$$C_{rev} = \frac{P_2}{P_4},$$

The net power delivered to the transmitting device is then:  $P_{net} = C_{fivd} P M_1 - C_{rev} P M_2$ ,

where  $PM_1$  and  $PM_2$  are the power meter readings in linear units.

Where the VSWR of the antenna is known, then a single three-port coupler can be used. For example, when the antenna has a VSWR of 1,5 this is equivalent to a Voltage Reflection Coefficient (VRC) of 0,2.

The accuracy is affected by the directivity of the coupler. The directivity is a measure of the coupler's ability to isolate the forward and the reverse signals. For a well-matched transmitting device, the reverse power is much smaller than the forward power. The effect of the directivity is therefore less important than in a reflectivity application. For example, when the transmitting antenna has a VSWR of 1,5, and the coupler has a directivity of 20 dB, the absolute maximum uncertainty in the net power due to the finite directivity is 0,22 dB - 0,18 dB = 0,04 dB with a U-shaped distribution. (where 0,22 dB is the apparent power loss of incident from VSWR 1,5)

The net power delivered to the transmitting device is then:

$$P_{net} = C_{fwd} P M_1 (1 - V R C^2)$$

#### L.4.2.2 Establishing a Standard Field using Horn Antennas

The gain of the horn antenna is determined by the methods described in L3.4. The on-axis electric field (in V/m) is determined by

$$E = \sqrt{\frac{\eta_0 P_{net} g}{4\pi}} \frac{1}{d},$$

where  $\eta_0 = 377 \ \Omega$  for free space,  $P_{net}$  (in W) is the net power determined by the method described in L.4.2.1, *g* is the numeric gain of the antenna determined by L3.4 and *d* (in m) is the distance from the antenna aperture.

#### L.4.2.3 Chamber validation test frequency range and frequency steps

The chamber VSWR test shall cover the frequency range for which the calibration of the probe is intended, and use the same frequency steps as given in L.2.3.

VSWR tests shall be carried out in the chamber at the lowest and highest frequencies of operation of each antenna. Where narrow band absorbers are used, e.g. ferrites, more frequency points may need to be measured. The Chamber should be used for probe calibration only in the frequency range where it meets the VSWR criteria.

#### L.4.2.4 Chamber validation procedure N 61000-4-3:2006/A1:2008

The chamber used for the probe calibration shall be verified by the following procedure except in cases where the physical conditions of the chamber do not allow it to be used. In such cases the alternative method of 4.2.7 can be applied.

The probe shall be located at the measurement position using a support material with a low permittivity (e.g. styrene foam) in accordance with Figure L3 and Figure L4.

A field probe is placed at the location where it will be used for calibration. Its polarization and position along the boresight of the transmitting horn antenna will be varied to determine the chamber VSWR. The transmit antenna shall be the same for both the chamber VSWR test and the probe calibration.

The arrangements of the standard gain horn antenna and the probe inside the chamber are shown in Figure L3. The probe and the horn antenna shall be set on the same horizontal axis with a separation distance L measured from the front face of the antenna to the centre of the probe.

In every case the field probe shall be laterally positioned in the center of the horn antenna face.