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TECHNICAL SPECIFICATION



Electroacoustics - Hedring aids Method for measuring electroacoustic performance up to 16 kHz (standards.iteh.ai)

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INTERNATIONAL ELECTROTECHNICAL COMMISSION

ELECTROACOUSTICS – HEARING AIDS – METHOD FOR MEASURING ELECTROACOUSTIC PERFORMANCE UP TO 16 kHz

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IEC TS 62886, which is a Technical Specification, has been prepared by IEC technical committee 29: Electroacoustics.

The text of this Technical Specification is based on the following documents:

Enquiry draft	Report on voting
29/897/DTS	29/902A/RVC

Full information on the voting for the approval of this Technical Specification can be found in the report on voting indicated in the above table.

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INTRODUCTION

Advancement in hearing aid design makes it possible to increase the bandwidth of hearing aids up to 16 kHz. Accordingly, there is a need for an accurate and yet robust measurement method for the transducer (receiver, earphone) designer, the hearing aid designer, and the fitter of hearing aids.

The 2 cm^3 coupler as described in IEC 60318-5 is only suitable for measurements up to 8 kHz. The limitation is caused by unfavourable acoustic modes of the coupler.

The occluded-ear simulator as described in IEC 60318-4 simulates the average human external ear up to 8 kHz, and can be used as a test coupler up to 16 kHz. The occluded earsimulator is designed for a specific insertion depth of the earmould, which is associated with a half-wavelength $\lambda/2$ resonance at about 13,5 kHz. This half-wavelength resonance degrades the reproducibility of measurement results in that frequency range and harmonic distortion measurements made at corresponding multiples of the resonance frequency. Also, this resonance represents a complex load to the hearing aid transducer, which makes it more difficult to differentiate between transducer and load related effects.

The effective internal volume of the coupler described in this Technical Specification is 0.4 cm^3 , which is small enough not to produce any resonance in the frequency range below 16 kHz. The frequency response of the magnitude of acoustic impedance follows a pattern of a capacitive load up to about 30 kHz. With a sufficiently high source impedance and a sufficiently small coupling volume, the 0.4 cm^3 coupler produces an approximately 14 dB higher output at 1 kHz in comparison to data obtained with the 2 cm³ coupler.

The coupler described in this document will allow the characterisation of hearing aids and transducers, including the verification of simulation models, up to 16 kHz.

0,4 cm³ is also approximately the residual volume of the ear canal when fitted with a CIC hearing aid (completely-in-the-canal) hearing aid, making this coupler particularly useful for this application.

In combination with an appropriate real-ear probe microphone measurement, the 0,4 cm³ coupler will enable the derivation of real-ear to coupler difference (RECD) up to 16 kHz.

ELECTROACOUSTICS – HEARING AIDS – METHOD FOR MEASURING ELECTROACOUSTIC PERFORMANCE UP TO 16 kHz

1 Scope

IEC TS 62886, which is a Technical Specification, describes a coupler and measurement methods to characterise the electroacoustic performance of hearing aids and insert earphones primarily in the range of 8 kHz to 16 kHz.

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

IEC 60118-0, *Electroacoustics – Hearing aids – Part 0: Measurement of the performance characteristics of hearing aids*

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IEC 60318-4, Electroacoustics – Simulators of human head and ear – Part 4: Occluded-ear simulator for the measurement of earphones coupled to the ear by means of ear inserts

IEC 60318-5, Electroacoustics – Simulators of human head and ear – Part 5: 2 cm³ coupler for the measurement of the aring haids and tage phones coupled to the means of ear inserts f705f32b27e4/iec-ts-62886-2016

IEC 61094-4, Measurement microphones – Part 4: Specifications for working standard microphones

IEC 60263, Scales and sizes for plotting frequency characteristics and polar diagrams

3 Terms, definitions and abbreviated terms

3.1 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- IEC Electropedia: available at http://www.electropedia.org/
- ISO Online browsing platform: available at http://www.iso.org/obp

3.1.1

reference cavity

simple cylindrical cavity with the same nominal diameter and height as the coupler under test, establishing a volume that can be measured using precision dimensional metrology

Note 1 to entry: In the context of this document, the reference cavity is 400 mm³ \pm 3 mm³, with a diameter of 9,45 mm \pm 0,02 mm and a height of 5,70 mm \pm 0,02 mm.

3.1.2

effective coupler volume

adjusted volume of the coupler under test that causes the measured sound pressure level in the coupler under test to equal the measured sound pressure level in the reference cavity

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3.1.3

coupler volume ratio

20 times the logarithmic ratio to the base of 10 of the effective coupler volumes of a 2 cm^3

and 0,4 cm³ coupler (
$$20 \lg \frac{V_{2 \text{ cm}^3}}{V_{0.4 \text{ cm}^3}} \text{ dB}$$
)

Note 1 to entry: The coupler volume ratio is expressed in dB.

Note 2 to entry: The coupler volume ratio can vary between 13,46 dB and 14,50 dB since the effective coupler volume of the 2 cm³ coupler (according to IEC 60318-5) is defined as 2 000 mm³ \pm 70 mm³ and the effective coupler volume of the 0,4 cm³ coupler is defined as 400 mm³ \pm 10 mm³ (see 4.2.2).

3.1.4

3.1.5

coupler level difference

difference between the sound pressure levels in the 0,4 cm³ coupler and the 2 cm³ coupler produced by the same sound source

Note 1 to entry: The coupler level difference includes the influence of the impedance of the sound source. For finite source impedance, the coupler level difference will be less than the coupler volume ratio.

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effective length of coupling tubing length of the acoustic coupling tubing that extends from the output of the receiver or BTE hearing aid ear hook to the coupler reference plane

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Note 1 to entry: The actual length of tubing used may deviate 100m 5 the effective length of coupling tubing, for example, a) the overlap resulting from the connection to the ear hook or hearing aid receiver may increase the actual length of tubing used, whereas (b) connection to the nipple of the coupling plate or earmould simulator, which is considered part of the effective length of coupling tubing, may reduce the actual length of tubing used accordingly. See Figure 2, Figure 5 and Figure 6.

3.2 Abbreviated terms

- CIC completely-in-the-canal
- ITC in-the-canal
- IIC invisible-in-the-canal
- ITE in-the-ear
- BTE behind-the-ear
- RIC receiver-in-the canal
- RECD real-ear to coupler difference
- SPL sound pressure level

Mechanical design of the 0,4 cm³ coupler 4

4.1 General

The coupler consists essentially of a cylindrical cavity whose effective volume is nominally 400 mm³. The base of the cylindrical cavity contains the diaphragm of a microphone, or a microphone with an adaptor. A protection grid may or may not be fitted. The microphone measures the sound pressure level (SPL) in the coupler. The coupler shall be constructed of hard, dimensionally stable, non-porous and non-magnetic material. The general construction of the coupler and mounting of the microphone shall aim to minimise the response of the microphone to vibration (for example from an earphone) or to extraneous sound outside the cavity.

The external diameter of the coupler should be kept as small as possible in order to minimise diffraction errors which might affect the measurements when the coupler has to be placed in a sound field.

Where tolerances are specified in this document, these shall be reduced by an amount equal to the actual expanded measurement uncertainty of the test laboratory before deciding if a device conforms to the stated requirement.

Figure 1 shows the mechanical design of the coupler.



h Coupler reference plane

Key d₁

h₁

а

b

c d

е

g

i Microphone insertion stop feature

Figure 1 – Mechanical design of the 0,4 cm³ coupler, shown with removable coupling plate with a nipple for the attachment of coupling tubing

4.2 Cavity dimensions

4.2.1 Critical dimensions

The critical dimensions of the coupler are those which determine the shape and the volume of the cavity terminated by a measurement microphone, and the static pressure equalisation vent.

4.2.2 Effective coupler volume

The effective coupler volume shall be 400 mm³ \pm 10 mm³.

The contribution of any front cavity and of the finite diaphragm impedance associated with the measurement microphone shall be included in the effective volume of the coupler. Therefore, the height of the cylindrical cavity should be designed such that the effective volume of the coupler conforms to the requirement for all microphone models intended for use with the coupler.

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4.2.3 Diameter of the coupler cavity

The diameter d_1 of the cylindrical coupler cavity shall be 9,45 mm \pm 0,05 mm.

4.3 Verification procedure of the effective coupler volume

4.3.1 General

The verification of the effective coupler volume (see 3.1.2) by acoustical means is performed by comparing the sound pressure in the coupler – which includes the coupler microphone with protection grid, the static pressure equalisation vent, microphone insertion stop if fitted and any other feature affecting the effective volume – with the sound pressure produced in a reference cavity (see 3.1.1).

4.3.2 Test set-up

The coupling plate for this test includes a source and a control microphone. This assembly can be attached to the reference cavity and the coupler under test. The control microphone measures the sound pressure in the reference cavity and in the coupler under test. The sound source input signal shall be the same for both measurements.

NOTE If both measurements are performed immediately one after another in a stable environment, effects related to heat conduction into the cavity walls will be essentially the same for both tests.

4.3.3 Effective volume of the coupler under test

During the sound pressure measurements made in the coupler under test and in the reference cavity, the effective volume of the coupler under test and the effective volume of the reference cavity will be increased by the effective volume V_s of the sound source.

Assuming constant air temperature and using Boyle's law:

 $p_{ref}/(V_{ref} + V_s) = p_{coupler}/(V_{coupler} + V_s)$

$$V_{\text{coupler}} = \left(\frac{P_{\text{ref}}}{P_{\text{coupler}}}\right) V_{\text{ref}} + \left(\frac{P_{\text{ref}}}{P_{\text{coupler}}}\right) V_{\text{s}} - V_{\text{s}}$$

where

*V*_{ref} is the volume of reference cavity

 V_{coupler} is the volume of the coupler under test

- $V_{\rm s}$ is the effective volume of the sound source which is the combined volumes of the sound source and control microphone
- p_{ref} is the sound pressure in the reference cavity

 p_{coupler} is the sound pressure in the coupler under test

 $V_{\rm s}$ cancels out, if $p_{\rm coupler}$ equals $p_{\rm ref^{-}}$

Subsequently, V_{coupler} equals V_{ref} .