# INTERNATIONAL 

# Thermoplastics pipes - Universal wall thickness table <br> <br> iTeh STANDARD PREVIEW <br> <br> iTeh STANDARD PREVIEW <br> (Jubesen matières thermoplastiques - Tableau universel des épaisseurs 

## ISO 4065:1996

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f3ad3b80b60c/iso-4065-1996

## Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an internationai Standard requires approval by at least $75 \%$ of the member bodies casting a vote.

International Standard ISO 4065 was preparedaby deghnidak Comhnitteei) ISO/TC 138, Plastics pipes, fittings and valves for the transport of fluids.

This second edition cancels and replaces the first edition (150 4065:1978), which has been technically revised.standards.iteh.ailcatalog/standards/sistc8c5c743-c453-478f-a3dd-
f3ad3b80b60c/iso-4065-1996
The aim of the first edition was to identify a series of standard wall thicknesses for thermoplastics pipes as a means of controlling the wide variety of wall thicknesses which might otherwise be produced. The revision of this document has resulted in a number of basic changes. The standard now provides a basis for establishing a series of wall thicknesses for use in the preparation of product standards. However, it is not regarded as providing an exclusive list of wall thicknesses, as there may be occasions when specific applications require other wall thicknesses to take into account additional factors such as stiffness or temperature conditions.

Annex A of this International Standard is for information only.

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# Thermoplastics pipes - Universal wall thickness table 

## 1 Scope

This International Standard specifies the relationship between the nominal wall thickness $e_{n}$ and the nominal outside diameter $d_{n}$ of thermoplastics pipes.

It is applicable to smooth thermoplastics pipes of constant circular cross-section along the whole length of the pipe, whatever their method of manufacture, their composition or their intended application.

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## 2 Normative reference

3.3 wall thickness at any point, $e_{y}$ : The measured
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flanges and components designated by thread size. It is a convenient round number for reference purposes.

NOTE 1 For metric pipe series conforming to ISO 161-1[1] (see annex A), the nominal outside diameters, expressed in millimetres, are the minimum mean outside diameters $d_{\text {em,min }}$ in the applicable standard for pipe.
3.2 mean outside diameter, $d_{\mathrm{em}}$ : The measured length of the outer circumference of the pipe divided by $\pi^{1}$, rounded to the next higher 0.1 mm . ISO 4065:1996 wall thickness at any point around the circumf
The following standard contains provisions which through reference in this text, constitute provisions of this International Standard. At the time of publication, the edition indicated was valid. All standards are subject to revision, and parties to agreements based on this International Standard are encouraged to investigate the possibility of applying the most recent edition of the standard indicated below. Members of IEC and ISO maintain registers of currently valid International Standards.

ISO 3:1973, Preferred numbers - Series of preferred numbers.

## 3 Definitions

For the purposes of this International Standard, the following definitions apply.
3.1 nominal outside diameter, $d_{n}$ : A numerical designation of size which is common to all components in a thermoplastics piping system other than
3.4 nominal wall thickness, $e_{n}$ : A wall thickness tabulated in this International Standard, and identical to the minimum permissible wall thickness at any point, $e_{y, \text { min }}$.
3.5 standard dimension ratio, SDR: The ratio of the nominal outside diameter $d_{\mathrm{n}}$ of a pipe to its nominal wall thickness $e_{n}$.

NOTE 2 This value may also be derived from the equation given in 3.6.
3.6 pipe series, $\mathbf{S}$ : A dimensionless number related to the nominal outside diameter $d_{\mathrm{n}}$ and nominal wall thickness $e_{n}$, the value of which is as specified in the tables in this International Standard.

The pipe series number $S$ is given by the following equation:

$$
S=\frac{S D R-1}{2}
$$

[^1]and for pressure pipes this can be expressed as:
$$
\mathrm{S}=\frac{\sigma}{p}
$$
where
$p$ is the internal pressure;
$\sigma$ is the induced stress;
$p$ and $\sigma$ being expressed in the same units.
For the selection of $p$ and $\sigma$, the reader is referred to ISO 161-1 [1].

S-values equal to or less than 10 are selected from the R 10 series of preferred numbers given in ISO 3, whilst those greater than 10 are selected from the R 20 series.

## 4 Calculation of wall-thickness values

According to ISO 161-1, wall thicknesses for pressure pipes are calculated from either of the following equations:

$$
e_{\mathrm{n}}=\frac{1}{2 \frac{\sigma}{p}+1} \times d_{\mathrm{n}}
$$

and

$$
e_{\mathrm{n}}=\frac{1}{2 \mathrm{~S}+1} \times d_{\mathrm{n}}
$$

where
$e_{\mathrm{n}}$ is the nominal wall thickness;
$d_{\mathrm{n}}$ is the nominal outside diameter; $e_{\mathrm{n}}$ and $d_{\mathrm{n}}$ being expressed in the same units;
$\sigma$ is the induced stress;
$p$ is the internal pressure; $\sigma$ and $p$ being expressed in the same units;
$S$ is the series number.
The general equations are also applicable to the relationship between the maximum allowable operating pressure $p_{\text {PMS }}$ and the design stress $\sigma_{\mathrm{S}}$, as follows:

$$
e_{\mathrm{n}}=\frac{1}{2 \frac{\sigma_{\mathrm{S}}}{p_{\mathrm{PMS}}}+1} \times d_{\mathrm{n}}
$$

Values for $p_{\text {PMS }}$ are selected from the R 10 series of preferred numbers given in ISO 3.
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Values for $\sigma_{s}$ equal to or less than 10 MPa are selected from the R 10 series of preferred numbers given in ISO 3, whilst those greater than 10 MPa are selected from the R 20 series.

S may therefore be defined as the quotient of the design stress and the maximum allowable operating pressure as follows:

$$
\mathrm{S}=\frac{\sigma_{\mathrm{S}}}{p_{\mathrm{PMS}}}
$$

For maximum allowable operating pressures between 2,5 bar and 25 bar and design stresses between $2,5 \mathrm{MPa}$ and 16 MPa , the corresponding S values are given in table 1. This table also incorporates an additional pipe series based on a nominal pressure of 6 bar which is not a preferred number of the R 10 series. This maximum allowable operating pressure has been included in table 1 because it is used in many countries in preference to the value of $6,3 \mathrm{bar}$.

Table 2 gives the calculated values of $S$ taken from ISO 497 ${ }^{[2]}$, and table 3 gives calculated values of $S$ for a $p_{\text {PMS }}$ of 6 bar.

## NOTESPREVIIEW

3 With the exception of the 6 bar series, $S$ is the quotient (standarcof two R 10 numbers for design stresses of 10 MPa and below, and therefore it is itself a number of the R 10 series also, For values greater than $10 \mathrm{MPa}, \mathrm{S}$ is the quotient of an $\mathrm{R}_{1} 10$ and an $\mathrm{R}_{2} 0_{4}$ number and therefore in this case the number is an $R 20$ value.
This is the key to the reduction in the many theoretical combinations of design stress and operating pressure to a practical selection of values of $S$. Since preferred numbers are themselves rounded off from the theoretical values, quotients of preferred numbers cannot basically be identical either with preferred numbers or with the theoretical values.

These theoretical values may, however, be considered as mean values for all corresponding quotients. Therefore, a universal wall thickness table which is mathematically based on the theoretical values of the R 10 and $R 20$ series of preferred numbers for $S$ guarantees a minimum number of deviations from the numerous theoretical wall thicknesses.

4 All calculated values of wall thickness given in tables 4 and 5 have been rounded off to one significant figure using the following procedure:
Step 1: Express the calculated value to three significant figures, e.g. 0,XXX.
Step 2:
a) If the second significant figure is 1 or higher, then the first significant figure is rounded up.
b) If the second significant figure is 0 and the third significant figure is 5 or over, then the first significant figure is rounded up, but if the third significant figure is 4 or less, then the value is rounded down by expressing the value as the first significant figure.

## 5 Wall-thickness tables

Table 4 gives the relationship between the nominal wall thickness $e_{\mathrm{n}}$ and the nominal outside diameter $d_{n}$ based on the $S$-values given in table 2 .

The wall thicknesses of an additional pipe series based on a maximum permissible operating pressure of 6 bar are given in table 5, and are calculated from the S -values given in table 3.

## 6 Non-pressure pipes

Although the calculation of the wall thickness with the value of $S$ derived from the quotient of the design
stress $\sigma_{\mathrm{s}}$ and a maximum allowable operating pressure $p_{\mathrm{PMS}}$ which applies to pipes predominantly subject to internal hydrostatic pressure, the values given in tables 4 and 5 also apply to pipes not subject to internal pressure.

## 7 Deviations

Notwithstanding the generalities expressed in clause 6, it is appreciated that there may be some occasions when specific applications require other wall thicknesses in order to take into account additional factors such as stiffness or temperature conditions. It is strongly recommended that such exceptions are kept to a minimum, however.

Table 1 - Individual S-values calculated from selected values of design stress, $\sigma_{\mathrm{s}}$, and maximum allowable operating pressure, $p_{\text {PMS }}$

| Design <br> stress <br> $\sigma_{s}$ |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MPa | S -values |  |  |  |  |  |  |  |  |  |  |  |
| 16 | 6.4000 | 8,000 0 | 10,000 | 12.800 id | 16,000 ${ }^{\text {I }}$ | 20,000 | 25,3973 | 26,667 | 32,000 | 40,000 | 50,794 | 64,000 |
| 14 | 5,600 0 | 7,000 0 | 8,750 0 | 11,200 32 | 134,00960 | 15000865 | 22.222 | 23,333 | 28,000 | 35,000 | 44,444 | 56,000 |
| 12,5 | 5,000 0 | 6,250 0 | 7,812 5 | 10,000 | 12,500 | 15,625 | 19,841 | 20,833 | 25,000 | 31,250 | 39,683 | 50,000 |
| 11,2 | 4,480 0 | 5,600 0 | 7,000 0 | 8,960 0 | 11,200 | 14,000 | 17,778 | 18,667 | 22,400 | 28,000 | 35,556 | 44,800 |
| 10 | 4,000 0 | 5,000 0 | 6,250 0 | 8,000 0 | 10,000 | 12,500 | 15,873 | 16,667 | 20,000 | 25,000 | 31,746 | 40,000 |
| 8 | 3,200 0 | 4,000 0 | 5,000 0 | 6,400 0 | 8,000 0 | 10,000 | 12,698 | 13,333 | 16,000 | 20,000 | 25,397 | 32,000 |
| 6,3 | 2,520 0 | 3,1500 | 3,937 5 | 5,040 0 | 6,300 0 | 7,875 0 | 10,000 | 10,500 | 12,600 | 15,750 | 20,000 | 25,200 |
| 5 | 2,000 0 | 2,500 0 | 3,1250 | 4,0000 | 5,000 0 | 6,250 0 | 7,936 5 | 8,333 3 | 10,000 | 12,500 | 15,873 | 20,000 |
| 4 |  | 2,000 0 | 2,500 0 | 3,200 0 | 4,0000 | 5,000 0 | 6,439 2 | 6,6667 | 8,000 0 | 10,000 | 12,698 | 16,000 |
| 3,15 |  |  | 1,968 8 | 2,150 0 | 3,150 0 | 3,937 5 | 5,000 0 | 5,250 0 | 6,300 0 | 7,875 0 | 10,000 | 12,600 |
| 2,5 |  |  |  | 2,000 0 | 2,000 0 | 3,125 0 | 3,968 3 | 4,1667 | 5,000 0 | 6,250 0 | 7,936 5 | 10,000 |
| NOTE - Individual S-values below 2,0000 have been excluded from this table as the resulting pipe geometry is considered to be unacceptable for practical applications. |  |  |  |  |  |  |  |  |  |  |  |  |

Table 2 - Nominal S-values and their calculated values, taken from ISO 497 for $p_{\text {PMS }}$ values of 2; 2,5; 3,15; 4; 5; 6,3; 8; 10; 12,5; 16; 20 and 25 bar ${ }^{1)}$

Table 3 - S-values and design stresses, taken from table 1 for the calculation of wall thicknesses for the $p_{\mathrm{PMS}}$ value of $\mathbf{6}$ bar

| Design stress MPa | Calculated S-values | Nominal S-values |
| :---: | :---: | :---: |
| 2,5 | 4,166 7 | 4,2 |
| 3,15 | 5,250 0 | 5,3 |
| 4 PTV | 4-6,6667 | 6,7 |
| 5-1 | -8,333 3 | 8,3 |
| S.ite6,3.ai) | 10,500 | 10,5 |
| 8 | 13,333 | 13,3 |
| 5:1996 ${ }^{10}$ | 16,667 | 16,7 |
| ds/sist/c81,2c743-c45 | 3-47818,667 | 18,7 |
| o-406512,56 | 20,833 | 20,8 |
| 14 | 23,333 | 23,3 |
| 16 | 26,667 | 26.7 |



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Table 4 - Nominal wall thickness, $e_{n}$, for $p_{\text {PMS }}$ values of 2,$5 ; 3,15 ; 4 ; 5 ; 6,3 ; 8 ; 10 ; 12,5 ; 16 ; 20$ and 25 bar

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| outside diameter, | $\begin{gathered} 2 \\ (5) \end{gathered}$ | $2,5$ (6) | $\begin{gathered} 3,2 \\ (7,4) \end{gathered}$ | $\begin{gathered} 4 \\ \hline \end{gathered}$ | $\begin{gathered} 5 \\ (11) \end{gathered}$ | $\begin{gathered} 6,3 \\ (13,6) \end{gathered}$ | $\begin{gathered} 8 \\ (17) \end{gathered}$ | $\begin{gathered} 10 \\ (21) \end{gathered}$ | $\begin{gathered} 11,2 \\ (23,4) \end{gathered}$ | $\begin{aligned} & 12,5 \\ & (26) \end{aligned}$ | 14 <br> (29) | $\begin{gathered} 16 \\ \text { (33) } \end{gathered}$ | $\begin{gathered} 20 \\ (41) \end{gathered}$ | $\begin{gathered} 25 \\ \text { (51) } \end{gathered}$ | $\begin{gathered} 32 \\ \text { (65) } \end{gathered}$ | $\begin{gathered} 40 \\ \text { (81) } \end{gathered}$ | $\begin{gathered} 50 \\ \text { (101) } \end{gathered}$ | $\begin{gathered} 63 \\ \text { (127) } \end{gathered}$ |
| $d_{n}$ | ITeh STANDARD PREV Nominal wall thickness, |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2,5 | 0,5 |  |  |  |  |  | . |  |  |  |  |  |  |  |  |  |  |  |
| 3 | 0,6 | 0.5 | 0.5 |  | ISO | 4065:19 |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | 0,8 | 0,7ht | s// 9 cifid | tds. ife 5 a | catalogst | ndards/sis | tc8c5c74 | 3-c453-4 | 78-a3dd- |  |  |  |  |  |  |  |  |  |
| 5 | 1,0 | 0,9 | 0.7 | 0.6 | ad30:5b | 0c/iso-40 | 65-1996 |  |  |  |  |  |  |  |  |  |  |  |
| 6 | 1,2 | 1,0 | 0,9 | 0,7 | 0,6 | 0,5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 | 1,6 | 1,4 | 1,1 | 0,9 | 0,8 | 0,6 | 0,5 |  |  |  |  |  |  |  |  |  |  |  |
| 10 | 2,0 | 1,7 | 1,4 | 1,2 | 1,0 | 0.8 | 0,6 | 0.5 | 0,5 |  |  |  |  |  |  |  |  |  |
| 12 | 2,4 | 2,0 | 1,7 | 1,4 | 1,1 | 0,9 | 0,8 | 0,6 | 0,6 | 0,5 | 0,5 |  |  |  |  |  |  |  |
| 16 | 3.3 | 2,7 | 2,2 | 1,8 | 1,5 | 1,2 | 1,0 | 0,8 | 0,7 | 0,7 | 0,6 | 0,5 |  |  |  |  |  |  |
| 20 | 4.1 | 3,4 | 2,8 | 2,3 | 1,9 | 1,5 | 1,2 | 1,0 | 0,9 | 0,8 | 0,7 | 0,7 | 0,5 |  |  |  |  |  |
| 25 | 5,1 | 4,2 | 3,5 | 2,8 | 2,3 | 1,9 | 1,5 | 1,2 | 1,1 | 1,0 | 0.9 | 0,8 | 0.7 | 0,5 |  |  |  |  |
| 32 | 6,5 | 5.4 | 4,4 | 3,6 | 2,9 | 2,4 | 1,9 | 1,6 | 1,4 | 1,3 | 1,1 | 1,0 | 0,8 | 0,7 | 0,5 |  |  |  |
| 40 | 8,1 | 6,7 | 5,5 | 4,5 | 3.7 | 3,0 | 2,4 | 1,9 | 1,8 | 1,6 | 1,4 | 1,3 | 1.0 | 0,8 | 0,7 | 0,5 |  |  |
| 50 | 10,1 | 8,3 | 6,9 | 5,6 | 4.6 | 3.7 | 3.0 | 2.4 | 2,2 | 2,0 | 1.8 | 1,6 | 1,3 | 1,0 | 0.8 | 0.7 | 0.5 |  |
| 63 | 12,7 | 10,5 | 8,6 | 7.1 | 5,8 | 4.7 | 3,8 | 3.0 | 2.7 | 2.5 | 2.2 | 2,0 | 1,6 | 1,3 | 1,0 | 0,8 | 0,7 | 0,5 |
| 75 | 15.1 | 12,5 | 10,3 | 8,4 | 6,8 | 5,6 | 4,5 | 3,6 | 3,2 | 2,9 | 2,6 | 2,3 | 1,9 | 1,5 | 1,2 | 1,0 | 0,8 | 0,6 |
| 90 | 18,1 | 15,0 | 12,3 | 10,1 | 8,2 | 6,7 | 5,4 | 4,3 | 3,9 | 3,5 | 3.1 | 2,8 | 2,2 | 1.8 | 1,4 | 1,2 | 0,9 | 0.8 |
| 110 | 22,1 | 18,3 | 15,1 | 12,3 | 10,0 | 8.1 | 6,6 | 5,3 | 4.7 | 4.2 | 3.8 | 3,4 | 2.7 | 2,2 | 1,8 | 1,4 | 1,1 | 0,9 |
| 125 | 25,1 | 20,8 | 17,1 | 14.0 | 11,4 | 9,2 | 7,4 | 6,0 | 5,4 | 4.8 | 4,3 | 3,9 | 3,1 | 2,5 | 2,0 | 1,6 | 1,3 | 1.0 |
| 140 | 28,1 | 23,3 | 19,2 | 15,7 | 12,7 | 10,3 | 8,3 | 6,7 | 6,0 | 5,4 | 4.8 | 4.3 | 3,5 | 2,8 | 2,2 | 1,8 | 1,4 | 1,1 |
| 160 | 32,1 | 26,6 | 21,9 | 17,9 | 14,6 | 11,8 | 9,5 | 7.7 | 6,9 | 6.2 | 5,5 | 4,9 | 4.0 | 3.2 | 2.5 | 2,0 | 1,6 | 1,3 |
| 180 | 36,1 | 29,9 | 24,6 | 20,1 | 16,4 | 13,3 | 10,7 | 8,6 | 7.7 | 6,9 | 6,2 | 5,5 | 4.4 | 3,6 | 2,8 | 2,3 | 1,8 | 1.5 |
| 200 | 40,1 | 33,2 | 27,4 | 22,4 | 18,2 | 14.7 | 11,9 | 9,6 | 8,6 | 7.7 | 6,9 | 6.2 | 4.9 | 3,9 | 3,2 | 2,5 | 2,0 | 1,6 |
| 225 | 45,1 | 37,4 | 30,8 | 25,2 | 20,5 | 16,6 | 13,4 | 10,8 | 9,6 | 8,6 | 7.7 | 6,9 | 5,5 | 4.4 | 3,5 | 2.8 | 2,3 | 1.8 |
| 250 | 50,1 | 41,5 | 34,2 | 27.9 | 22.7 | 18,4 | 14.8 | 11.9 | 10,7 | 9.6 | 8.6 | 7.7 | 6,2 | 4,9 | 3,9 | 3.1 | 2,5 | 2.0 |




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[^1]:    1) The value of $\pi$ is taken to be 3,142 .
