

Edition 4.0 2016-01

# INTERNATIONAL STANDARD





Superconductivity -

Part 4: Residual resistance ratio measurement – Residual resistance ratio of Nb-Ti and Nb<sub>3</sub>Sn composite superconductors

Supraconductivité -

Partie 4: Mesurage du rapport de résistance résiduelle – Rapport de résistance résiduelle des composites supraconducteurs de Nb-Ti et de Nb<sub>3</sub>Sn



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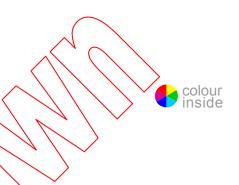
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## INTERNATIONAL STANDARD

## NORME INTERNATIONALE



Superconductivity -

Part 4: Residual resistance ratio measurement – Residual resistance ratio of Nb-Ti and Nb<sub>3</sub>Sn composite superconductors

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Partie 4: Mesurage du rapport de résistance résiduelle – Rapport de résistance résiduelle des composites supraconducteurs de Nb-Ti et de Nb<sub>3</sub>Sn



INTERNATIONAL ELECTROTECHNICAL COMMISSION

COMMISSION ELECTROTECHNIQUE INTERNATIONALE

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### INTERNATIONAL ELECTROTECHNICAL COMMISSION

### SUPERCONDUCTIVITY -

# Part 4: Residual resistance ratio measurement – Residual resistance ratio of Nb-Ti and Nb<sub>3</sub>Sn composite superconductors

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International Standard IEC 61788-4 has been prepared by IEC technical committee 90: Superconductivity.

This fourth edition cancels and replaces the third edition published in 2011. This edition constitutes a technical revision.

This edition includes the following significant technical changes with respect to the previous edition:

a) the unification of similar test methods for residual resistance ratio (RRR) of Nb-Ti and Nb<sub>3</sub>Sn composite superconductors, the latter of which is described in IEC 61788-11.

The text of this standard is based on the following documents:

FDIS	Report on voting
90/359/FDIS	90/360/RVD

Full information on the voting for the approval of this standard can be found in the report on voting indicated in the above table.

This publication has been drafted in accordance with the ISO/IEC Directives, Part 2.

A list of all parts of the IEC 61788 series, published under the general title Superconductivity, can be found on the IEC website.

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### INTRODUCTION

Copper, Cu/Cu-Ni or aluminium is used as matrix material in Nb-Ti and  $\text{Nb}_3\text{Sn}$  composite superconductors and works as an electrical shunt when the superconductivity is interrupted. It also contributes to recovery of the superconductivity by conducting heat generated in the superconductor to the surrounding coolant. The cryogenic-temperature resistivity of copper is an important quantity, which influences the stability and AC losses of the superconductor. The residual resistance ratio is defined as a ratio of the resistance of the superconductor at room temperature to that just above the superconducting transition.

This part of IEC 61788 specifies the test method for residual resistance ratio of Nb-Ti and Nb<sub>3</sub>Sn composite superconductors. The curve method is employed for the measurement of the resistance just above the superconducting transition. Other methods are described in A.3.



### SUPERCONDUCTIVITY -

# Part 4: Residual resistance ratio measurement – Residual resistance ratio of Nb-Ti and Nb<sub>3</sub>Sn composite superconductors

### 1 Scope

This part of IEC 61788 specifies a test method for the determination of the residual resistance ratio (RRR) of Nb-Ti and Nb $_3$ Sn composite superconductors with Cu, Cu-Ni Cu-Ni and Al matrix. This method is intended for use with superconductor specimens that have a monolithic structure with rectangular or round cross-section, RRR value less than 350, and cross-sectional area less than 3 mm $^2$ . In the case of Nb $_3$ Sn, the specimens have received a reaction heat-treatment.

### 2 Normative references

The following documents, in whole or in part, are normalizely referenced in this document and are indispensable for its application. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

IEC 60050-815, International Electrotechnical Vocabulary – Part 815: Superconductivity (available at: www.electropedia.org)

### 3 Terms and defin<mark>itions</mark>

For the purposes of this document, the terms and definitions given in IEC 60050-815 and the following apply.

### 3.1

### residual resistance ratio

### RRR

ratio of resistance at room temperature to the resistance just above the superconducting transition

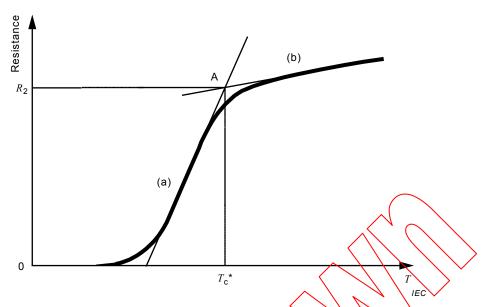
Note 1 to entry: This note applies to the French language only.

Note 2 to entry: In this part of IEC 61788 for Nb-Ti and Nb<sub>3</sub>Sn composite superconductors, the room temperature is defined as 293 K (20 °C), and the residual resistance ratio is obtained in Formula (1), where the resistance ( $R_1$ ) at 293 K is divided by the resistance ( $R_2$ ) just above the superconducting transition.

$$r_{\rm RRR} = \frac{R_1}{R_2} \tag{1}$$

Here  $r_{\rm RRR}$  is a value of the residual resistance ratio,  $R_2$  is a value of the resistance measured in a strain-free condition and zero external magnetic field.

Figure 1 shows schematically a resistance versus temperature curve acquired on a specimen while measuring the cryogenic resistance.



The cryogenic resistance,  $R_2$ , is determined by the intersection,  $A_1$  of two straight lines (a) and (b) at temperature  $T_c^*$ .

Figure 1 - Relationship between temperature and resistance

### 4 Principle

The resistance measurement both at room and cryogenic temperatures shall be performed with the four-terminal technique. All measurements are done without an applied magnetic field.

The target relative combined standard unsertainty of this method is defined as an expanded uncertainty (k = 2) not to exceed 5 %

The maximum bending strain induced during mounting and cooling the Nb-Ti specimen shall not exceed 2 %. The measurement shall be conducted in a strain-free condition or in a condition with allowable thermal strain for the  $Nb_3Sn$  specimen.

### 5 Apparatus

### 5.1 Material of measurement mandrel or of measurement base plate

Material of the measurement mandrel for a coiled Nb-Ti specimen or of the measurement base plate for a straight Nb-Ti or Nb $_3$ Sn specimen shall be copper, aluminium, silver, or the like whose thermal conductivity is equal to or better than 100 W/(m·K) at liquid helium temperature (4,2 K). The surface of the material shall be covered with an insulating layer (tape or a layer made of polyethylene terephthalate, polyester, polytetrafluoroethylene, etc.) whose thickness is 0,1 mm or less.

### 5.2 Diameter of the measurement mandrel and length of the measurement base plate

The diameter of the measurement mandrel shall be large enough to keep the bending strain of the specimen less than or equal to 2 % for the Nb-Ti specimen. The  $Nb_3Sn$  specimen on a base plate shall be measured in a strain-free condition or a condition with allowable thermal strain.

The measurement base plate shall be at least 30 mm long in one dimension.

### 5.3 Cryostat for the resistance $(R_2)$ measurement

The cryostat shall include a specimen support structure and a liquid helium reservoir for measurement of the resistance  $R_2$ . The specimen support structure shall allow the specimen, which is mounted on a measurement mandrel or a measurement base plate, to be lowered into and raised out of a liquid helium bath. In addition, the specimen support structure shall be made so that a current can flow through the specimen and the resulting voltage generated along the specimen can be measured.

### 6 Specimen preparation

The test specimen shall have no joints or splices with a length of 30 mm or longer. The specimen shall be instrumented with current contacts near each of its ends and a pair of voltage contacts over its central portion. The distance between two voltage taps (L) shall be 25 mm or longer. A thermometer for measuring cryogenic temperature shall be attached near the specimen.

Some mechanical method shall be used to hold the specimen against the insulated layer of the measurement mandrel or base plate. Special care should be taken during instrumentation and installation of the specimen on the measurement mandrel or base plate so that no excessive force, which may cause undesired bending strain or tensile strain, would be applied to the specimen. Ideally, it is intended that the Nb<sub>3</sub>Sn specimen be as straight as possible; however, this is not always the case, thus care should be taken to measure the specimen in its as received condition.

The specimen shall be mounted on a measurement mandrel or on a measurement base plate for these measurements. Both resistance measurements,  $R_1$  and  $R_2$ , shall be made on the same specimen and the same mounting.

### 7 Data acquisition and analysis

### 7.1 Resistance $(R_1)$ at room temperature

The mounted specimen shall be measured at room temperature  $(T_{\rm m}$  (K)), where  $T_{\rm m}$  satisfies the following condition. 273 K  $\geq T_{\rm m} \leq$  308 K. A specimen current  $(I_1$  (A)) shall be applied so that the current density is in the range of 0,1 A/mm² to 1 A/mm² based on the total wire cross-sectional area, and the resulting voltage  $(U_1$  (V)),  $I_1$  and  $I_{\rm m}$  shall be recorded. Formula (2) below shall be used to calculate the resistance  $(R_{\rm m})$  at room temperature. The resistance  $(R_1)$  at 293 K (20 °C) shall be calculated using Formula (3) for a wire with Cu matrix. The value of  $R_1$  shall be set equal to  $R_{\rm m}$ , without any temperature correction, for wires that do not contain a pure Cu component.

$$R_{\rm m} = \frac{U_1}{I_1} \tag{2}$$

$$R_{1} = \frac{R_{\rm m}}{\left[1 + 0.00393 \times \left(T_{\rm m} - 293\right)\right]}$$
 (3)

### 7.2 Resistance $(R_2 \text{ or } R_2^*)$ just above the superconducting transition

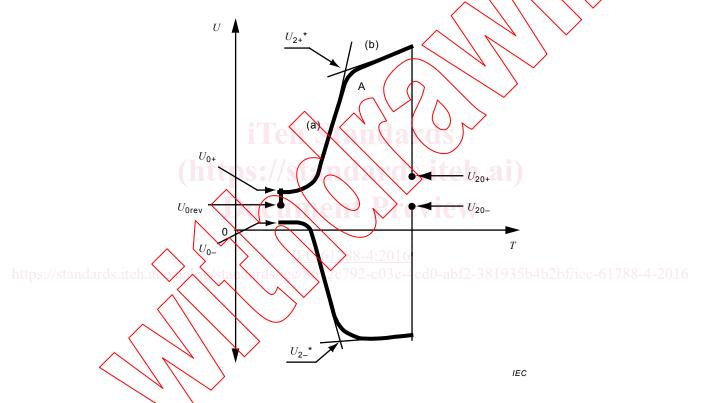
### 7.2.1 Correction of strain effect

Under a strained condition of the Nb-Ti specimen, the measured cryogenic resistance,  $R_2^*$ , is not a correct value for  $R_2$ . The corresponding correction of the strain effect is described in 7.3.

### 7.2.2 Data acquisition of cryogenic resistance

The specimen, which is still mounted as it was for the room temperature measurement, shall be placed in the cryostat for electrical measurement specified in 5.3. Horizontal mounting of the specimen is recommended in A.1. Alternate cryostats that employ a heating element to sweep the specimen temperature are described in A.2. The specimen shall be slowly lowered into the liquid helium bath and cooled to liquid helium temperature over a time period of at least 5 min.

During the acquisition phases of the low-temperature  $R_2^*$  measurements, a specimen current  $(I_2)$  shall be applied so that the current density is in the range 0,1 A/mm² to 10 A/mm² based on the total wire cross-sectional area, and the resulting voltage (U(V)),  $I_2(A)$ , and specimen temperature (T(K)) shall be recorded. In order to keep the ratio of signal to noise high enough, the measurement shall be carried out under the condition that the absolute value of the resulting voltage above the superconducting transition exceeds 10  $\mu$ V. An illustration of the data to be acquired and its analysis is shown in Figure 2.



NOTE Voltages with subscripts + and - are those obtained in the first and second measurements under positive and negative currents, respectively, and  $U_{20+}$  and  $U_{20-}$  are those obtained at zero current. For clarity,  $U_{0\text{rev}}$  measured at zero current is not shown coincident with  $U_{0-}$ . Straight line (a) is drawn in the transition region with a sharp increase in the voltage with temperature and straight line (b) is drawn in the region with a nearly constant voltage.

Figure 2 – Voltage versus temperature curves and definitions of each voltage

When the specimen is in the superconducting state and the test current  $(I_2)$  is applied, two voltages shall be measured nearly simultaneously:  $U_{0+}$  (the initial voltage recorded with a positive current polarity) and  $U_{0\text{rev}}$  (the voltage recorded during a brief change in applied current polarity). A valid  $R_2^{\star}$  measurement requires that excessive interfering voltages are not present and that the specimen is initially in the superconducting state. Thus, the following condition shall be met for a valid measurement:

$$\frac{\left|U_{0+} - U_{0\text{rev}}\right|}{\overline{U}_{2}} < 1 \% \tag{4}$$

where  $\overline{U}_2$  is the average voltage for the specimen in the normal state at cryogenic temperature, which is defined by Formula (5).

The specimen shall be gradually warmed so that it changes to the normal state completely. When the cryostat for the resistance measurement specified in 5.3 is used, this can be achieved simply by raising the specimen to an appropriate position above the liquid helium level. The specimen voltage versus temperature curve shall be acquired with the rate of temperature increase maintained between 0,1 K/min and 10 K/min. The voltage versus temperature curve shall continue to be recorded during the transition into the normal state, up to a temperature somewhat less than 15 K for the Nb-Ti specimen and less than 25 K for the Nb $_3$ Sn specimen. Then, the specimen current shall be decreased to zero and the corresponding voltage,  $U_{20+}$ , shall be recorded at a temperature below 15 K for the Nb-Ti specimen and below 25 K for the Nb $_3$ Sn specimen.

The specimen shall then be slowly lowered into the liquid helium bath and cooled to within  $\pm 1$  K from the temperature at which the initial voltage signal  $U_{0+}$  was resorded. A specimen current,  $I_2$ , with the same magnitude but negative polarity (polarity opposite that used for the initial curve) shall be applied and the voltage  $U_0$  shall be recorded at this temperature. The procedural steps shall be repeated to record the voltage versus temperature curve with this negative current. In addition, when the measurement current  $I_2$ , decreases to 0, the recording of  $U_{20-}$  shall be made at within  $\pm 1$  K from the temperature at which  $U_{20+}$  was recorded.

Each of the two voltage versus temperature curves shall be analysed by drawing a line (a) through the data where the absolute value of voltage sharply increases with temperature (see Figure 2) and drawing a second line (b) through the data above the transition where the voltage is nearly constant for Nb-Ti or raised gradually and almost linearly for Nb<sub>3</sub>Sn with temperature increase.  $V_{2+}^*$  and  $V_{2-}^*$  in Figure 2 shall be determined at the intersection of these two lines for the positive and negative polarity curves, respectively.

The corrected voltages,  $U_{2+}$  and  $U_{2-}$ , shall be calculated using the following equations:  $U_{2+} = U_{2+}^* - V_{0+}$  and  $U_{2-} = U_{2-}^* - U_{0-}$ . The average voltage,  $\overline{U}_2$ , shall be defined as

$$\overline{U}_2 = \frac{|U_{2+} - U_{2-}|}{2} \tag{5}$$

A valid  $R_2^{\star}$  measurement requires that the shift of thermoelectric voltage be within acceptable limits during the measurements of  $U_{2+}$  and  $U_{2-}$ . Thus, the following condition shall be met for a valid measurement:

$$\frac{\left|\Delta_{+} - \Delta_{-}\right|}{\overline{U}_{2}} < 3\% \tag{6}$$

where  $\Delta_+$  and  $\Delta_-$  are defined as  $\Delta_+ = U_{20+} - U_{0+}$  and  $\Delta_- = U_{20-} - U_{0-}$ . If the  $R_2^\star$  measurement does not meet the validity requirements in 7.2.2, specifically either in Formula (4) or (6), then improvement steps either in hardware or experimental operation shall be taken to meet these requirements before results are reported.

Formula (7) shall be used to calculate the measured resistance ( $R_2^*$ ) just above the superconducting transition.

$$R_2^* = \frac{\overline{U}_2}{I_2} \tag{7}$$

### 7.2.3 Optional acquisition methods

The method described in the body of this part of IEC 61788 is the "reference" method and optional acquisition methods are outlined in A.3.

### 7.3 Correction on measured $R_2^*$ of Nb-Ti composite superconductor for bending strain

If there is no pure Cu component in the superconductor, then  $R_2$  shall be set equal to  $R_2^*$ .

For a specimen with a pure Cu component, the bending strain shall be defined by  $\varepsilon_{\rm b}=100\times(h/r)$  (%), where h is a half of the specimen thickness and r is the bending radius. If the bending strain is less than 0,3 %, then no correction is necessary, and  $R_2$  shall be set equal to  $R_2^*$ .

If neither of the above two situations applies, then the resistance  $R_2$  just above the superconducting transition under the strain-free condition shall be estimated by

$$R_2 = R_2^* - \Delta \rho \times \frac{\dot{L}}{S_{\text{Cu}}}$$
 (8)

where  $\Delta \rho$  is defined below and  $S_{\text{Cu}}$  and L are defined in 8.4. The increase in the resistivity of pure copper at 4,2 K due to tensile strain,  $\varepsilon$  (%), is expressed by

$$\Delta \rho (\Omega m) = 6.24 \times 10^{-12} \varepsilon - 5.11 \times 10^{-14} \varepsilon^2; \ \varepsilon \le 2 \%$$
 (9)

The calculation of Formula (9) shall be carried out assuming that the equivalent tensile strain  $\varepsilon$  is  $(1/2)\varepsilon_D$  and  $(4/3\pi)\varepsilon_D$  for rectangular and round wires, respectively. The bending strain dependency of residual resistance ratio for pure copper is described in A.4.

### 7.4 Residual resistance ratio (RRR)

The RRR value shall be calculated using Formula (1).

### 8 Uncertainty and stability of the test method

### 8.1 Temperature

The room temperature shall be determined with a standard uncertainty not exceeding 0,6 K, while holding the specimen, which is mounted on the measurement mandrel or on the measurement base plate, at room temperature.

### 8.2 Voltage measurement

For the resistance measurement, the voltage signal shall be measured with a relative standard uncertainty not exceeding 0,3 %.