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**Petroleum and natural gas industries —  
Design and installation of piping systems  
on offshore production platforms**

*Industries du pétrole et du gaz naturel — Conception et installation de  
systèmes de tuyauterie sur les plates-formes de production en mer*

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## Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

International Standards are drafted in accordance with the rules given in the ISO/IEC Directives, Part 3.

Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

Attention is drawn to the possibility that some of the elements of this International Standard may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights.

International Standard ISO 13703 was prepared by Technical Committee ISO/TC 67, *Materials, equipment and offshore structures for petroleum and natural gas industries*, Subcommittee SC 6, *Processing equipment and systems*.

Annexes A, B and C of this International Standard are for information only.

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## Introduction

This International Standard is based on API RP 14E, 5<sup>th</sup> edition, October 1991.

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# Petroleum and natural gas industries — Design and installation of piping systems on offshore production platforms

## 1 Scope

This International Standard specifies minimum requirements and gives guidance for the design and installation of new piping systems on production platforms located offshore for the petroleum and natural gas industries. It covers piping systems up to 69 000 kPa (ga) maximum, within temperature range limits for the materials meeting the requirements of ASME B31.3.

**NOTE** For applications outside these pressure and temperature ranges, this International Standard may be used but special consideration should be given to material properties.

Annex A gives some worked examples for solving piping design problems.

## 2 Normative references

The following normative documents contain provisions which, through reference in this text, constitute provisions of this International Standard. For dated references, subsequent amendments to, or revisions of, any of these publications do not apply. However, parties to agreements based on this International Standard are encouraged to investigate the possibility of applying the most recent editions of the normative documents indicated below. For undated references, the latest edition of the normative document referred to applies. Members of ISO and IEC maintain registers of currently valid International Standards.

ISO 13623, *Petroleum and natural gas industries — Pipeline transportation systems*.

API RP 520-2<sup>1)</sup>, *Recommended practice for design and installation of pressure-relieving systems in refineries — Part 2*.

ASME<sup>2)</sup>, *Boiler and pressure vessel code: Section VIII: Pressure vessels, Division 1*.

ASME B 31.3, *Process piping*.

NACE MR0175<sup>3)</sup>, *Sulfide stress cracking resistant metallic materials for oil field equipment*.

NACE TM0177, *Laboratory testing of metals for resistance to specific forms of environmental cracking in H<sub>2</sub>S environments*.

NACE TM0284, *Evaluation of pipeline and pressure vessel steels for resistance to hydrogen-induced cracking*.

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1) American Petroleum Institute, 1220 L Street, N.W., Washington, DC 20005-4070, U.S.A.

2) American Society of Mechanical Engineers, 345 East 47<sup>th</sup> Street, New York, N.Y. 10017, U.S.A.

3) National Association of Corrosion Engineers, P.O. Box 218340, Houston, Texas 77218-8340, U.S.A.

### 3 Terms, definitions, symbols and abbreviated terms

For the purposes of this International Standard, the following terms, definitions, symbols and abbreviated terms apply.

#### 3.1 Terms and definitions

##### 3.1.1

##### **chloride stress-corrosion cracking service**

service in which the process stream contains water and chlorides in a sufficient concentration, and at a high enough temperature, to induce stress-corrosion cracking of susceptible materials

NOTE Other constituents present, such as oxygen (O<sub>2</sub>), may contribute to such chloride stress-corrosion cracking.

##### 3.1.2

##### **choke**

device specifically intended to restrict the flow rate of fluids

##### 3.1.3

##### **corrosion-erosion**

eroding away of a protective film of corrosion product by the action of the process stream, exposing fresh metal which then corrodes

NOTE Extremely high metal mass loss can occur under these conditions.

##### 3.1.4

##### **corrosive gas**

gas which, when dissolved in water or other liquid, causes corrosion of metal

NOTE Corrosive gases usually contain hydrogen sulfide (H<sub>2</sub>S), carbon dioxide (CO<sub>2</sub>) and/or oxygen (O<sub>2</sub>).

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##### 3.1.5

##### **corrosive hydrocarbon service**

service in which the process stream contains water or brine and carbon dioxide (CO<sub>2</sub>), hydrogen sulfide (H<sub>2</sub>S), oxygen (O<sub>2</sub>) or other corrosive agents under conditions which cause corrosion of metal

##### 3.1.6

##### **expansion bellows**

corrugated piping device designed to absorb expansion and contraction

##### 3.1.7

##### **expansion bend**

piping configuration designed to absorb expansion and contraction

##### 3.1.8

##### **flowline**

piping that carries well fluid from wellhead to manifold or first process vessel

##### 3.1.9

##### **flow regime**

flow condition of a multi-phase process stream

EXAMPLES Slug flow, mist flow or stratified flow.

##### 3.1.10

##### **fluid**

gas, vapour, liquid or combinations thereof



**3.1.11****header**

part of a manifold that directs fluid to a specific process system

See Figures 5 and 6.

**3.1.12****hydrocarbon wettability**

ability of the process stream to form a protective hydrocarbon film on metal surfaces

**3.1.13****manifold**

assembly of pipe, valves and fittings by which fluid from one or more sources is selectively directed to various process systems

**3.1.14****nipple**

section of threaded or socket-welded pipe, shorter than 300 mm, used as an appurtenance

**3.1.15****nominal pipe size****nominal size****NPS****DN**

designation of size in inches which is common to all components in a piping system other than those components designated by outside diameter

NOTE Nominal pipe size is designated by the letters NPS (when relating to inches) or DN (when relating to millimetres) followed by a number; it is a convenient number for reference purposes and it is normally only loosely related to manufacturing dimensions.

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**3.1.16****non-corrosive hydrocarbon service**

service in which the process stream conditions do not cause significant metal mass loss, selective attack, chloride stress-corrosion cracking or sulfide stress-cracking

**3.1.17****normal conditions**

absolute pressure of 101,325 kPa and temperature of 0 °C

**3.1.18****platform piping**

any piping intended to contain or transport fluid on a platform

**3.1.19****pressure rating**

number relating to the pressure for which a system is suitable

NOTE The number may relate directly to the rated working pressure (e.g. ISO 10423 [1] pressure rating 13,8 MPa and API pressure rating 2 000 psi) or may have a more indirect correlation (e.g. ASME class 300).

**3.1.20****pressure sensor**

device designed to detect a predetermined pressure

**3.1.21****process component**

single functional piece of production equipment and associated piping

EXAMPLES Pressure vessel, heater, pump, etc.

**3.1.22**

**riser**

vertical portion of a pipeline (including the bottom bend) arriving on or departing from a platform

**3.1.23**

**shutdown valve**

automatically-operated valve used for isolating a process component or process system

**3.1.24**

**sulfide stress-cracking service**

service in which the process stream contains water or brine and contains a sufficient concentration of hydrogen sulfide ( $H_2S$ ) to induce sulfide stress-cracking of susceptible materials

**3.1.25**

**wellhead pressure**

maximum shut-in surface pressure that may exist in a well

**3.2 Symbols and abbreviated terms**

**3.2.1 Symbols**

- A* minimum pipe cross-sectional flow area required per unit volume flowrate, expressed in square millimetres per cubic metre per hour ( $mm^2/m^3/h$ )
- B* mean coefficient of thermal expansion at operating temperatures normally encountered, expressed in millimetres per kelvin ( $mm/K$ )
- C* empirical constant, dimensionless
- C<sub>e</sub>* sum of corrosion, mechanical strength and thread allowance, expressed in millimetres (mm)
- C<sub>v</sub>* valve coefficient, dimensionless

NOTE 1 This value is equal to the water flowrate in US gpm at 60 °F required to generate a pressure drop of 1 psi (US Customary units only are used in this instance to maintain alignment with other published data).

- D<sub>i</sub>* pipe inside diameter, expressed in metres (m)
- D<sub>o</sub>* pipe outside diameter, expressed in millimetres (mm)
- d<sub>i</sub>* pipe inside diameter, expressed in millimetres (mm)
- d<sub>g</sub>* gas relative density (air = 1), dimensionless
- d<sub>L</sub>* liquid relative density (water = 1), dimensionless
- E* longitudinal weld joint factor, dimensionless
- E<sub>m</sub>* modulus of elasticity of piping material in the cold condition, expressed in newtons per square millimetre ( $N/mm^2$ )
- f* Moody friction factor, dimensionless
- g* gravitational constant, expressed in metres per second per second ( $m/s^2$ )
- h<sub>a</sub>* acceleration head, expressed in metres (m) of liquid
- h<sub>f</sub>* friction head, expressed in metres (m) of liquid

$h_p$	absolute pressure head, expressed in metres (m) of liquid
$h_{st}$	static head, expressed in metres (m) of liquid
$h_{vh}$	velocity head, expressed in metres (m) of liquid
$h_{vpa}$	absolute vapour pressure, expressed in metres (m) of liquid
$h_W$	pressure loss, expressed in kilopascals (kPa)
$K$	acceleration factor, dimensionless
$L$	developed pipe length, expressed in metres (m)
$L_m$	pipe length, expressed in kilometres (km)
$m$	manufacturing wall thickness tolerance, expressed as a percentage (%)
$NPSH_a$	available net positive suction head, expressed in metres (m) of liquid
$p$	operating pressure, expressed in kilopascals [kPa (abs)]
NOTE 2	Also denoted in text as "flowing pressure".
$p_i$	internal design pressure, expressed in kilopascals [kPa (ga)]
$q_g$	gas flow rate, expressed in cubic metres per hour (m <sup>3</sup> /h) at normal conditions
$q_L$	liquid flow rate, expressed in cubic metres per hour (m <sup>3</sup> /h)
$q_m$	total liquid plus vapour mass flowrate, expressed in kilograms per hour (kg/h)
$R$	gas/liquid volume ratio, dimensionless
$Re$	Reynolds number, dimensionless
$R_p$	pump speed, expressed in revolutions per minute (r/min)
$S$	allowable stress, expressed in newtons per square millimetre (N/mm <sup>2</sup> )
$T$	operating temperature, expressed in kelvin (K)
NOTE 3	Also denoted in text as "flowing temperature".
$t$	pressure design thickness, expressed in millimetres (mm)
$t_{nom}$	minimum nominal pipe wall thickness, expressed in millimetres (mm)
$U$	anchor distance (straight line distance between anchors), expressed in metres (m)
$v_e$	fluid erosional velocity, expressed in metres per second (m/s)
$v_g$	average gas velocity, expressed in metres per second (m/s)
NOTE 4	Also denoted in text as "gas velocity"
$v_L$	average liquid velocity, expressed in metres per second (m/s)
$y$	resultant of total displacement strains, expressed in millimetres (mm)

$Y$	temperature factor, dimensionless
$Z$	gas compressibility factor, dimensionless
$\Delta L$	expansion to be absorbed by pipe, expressed in millimetres (mm)
$\Delta p$	pressure drop, expressed in kilopascals (kPa)
$\rho_g$	gas density at operating pressure and temperature, expressed in kilograms per cubic metre (kg/m <sup>3</sup> )
$\rho_L$	liquid density at operating temperature, expressed in kilogram per cubic metre (kg/m <sup>3</sup> )
$\rho_m$	gas/liquid mixture density at operating pressure and temperature, expressed in kilograms per cubic metre (kg/m <sup>3</sup> )
$\Delta T$	temperature change, expressed in kelvin (K)
$\mu_g$	gas viscosity at flowing pressure and temperature, expressed in pascal seconds (Pa·s)
$\mu_L$	liquid viscosity, expressed in pascal seconds (Pa·s)

### 3.2.2 Abbreviated terms

ERW	Electric Resistance Weld
PWHT	Post-Weld Heat Treatment
RF	Raised Face
RTJ	Ring Type Joint
SAW	Submerged Arc Weld
SMYS	Specified Minimum Yield Strength

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## 4 General considerations

### 4.1 Materials

Carbon steel materials are suitable for many of the piping systems on production platforms, although stainless steels and other materials are also widely used. The following should be considered when selecting piping materials:

- a) type of service;
- b) compatibility with other materials;
- c) mechanical strength, ductility, elasticity and toughness;
- d) need for special welding procedures, or other jointing techniques;
- e) need for special inspections, tests, or quality control;
- f) possible misapplication in the field;
- g) corrosion and erosion caused by internal fluids and/or marine environments;
- h) need for performance in a fire situation.

## 4.2 Code of pressure piping

**4.2.1** The design and installation of platform piping shall be in accordance with ASME B31.3, as modified by this International Standard. Risers for which ASME B31.3 is not applicable should be designed and installed in accordance with 4.2.2 to 4.2.6.

**4.2.2** Design, construction, inspection and testing of risers shall be in accordance with ISO 13623 and governmental rules and regulations as appropriate to the application, using a design stress no greater than 0,6 times SMYS. Pipeline design codes may be used from pig trap to pig trap, except where precluded by national regulations.

**4.2.3** One hundred percent radiography of welding should be performed on riser piping. The non-destructive testing of platform piping complying with ASME B31.3 should as a minimum satisfy Table 10 of this International Standard.

**4.2.4** Impact tests shall be performed as specified by ASME B31.3. The design of high-pressure piping systems (i.e. above ASME class 2500) needs special consideration and shall be in accordance with the high-pressure piping requirements of ASME B31.3.

**4.2.5** Valves, fittings and flanges should be manufactured in conformance with International and/or National Standards. Pressure/temperature ratings and material compatibility should be verified.

**4.2.6** In determining the transition between risers and platform piping to which these practices apply, the first incoming and last outgoing valve that block pipeline flow are the limits of this International Standard's application, except for riser wall thickness calculations and material selection which may be to a pipeline code to permit a constant bore for pigging. Recommended practices included in this International Standard may be utilized for riser design when factors such as water depth, batter of platforms legs, potential bubbling area etc. are considered. National regulations may require the pipeline code to be continued to/from the pig launcher/receiver.

**4.2.7** It is also common practice for a pipeline code to apply through the riser up to the pig trap and to include the piping and the first valve on each branch on the riser/pipeline.

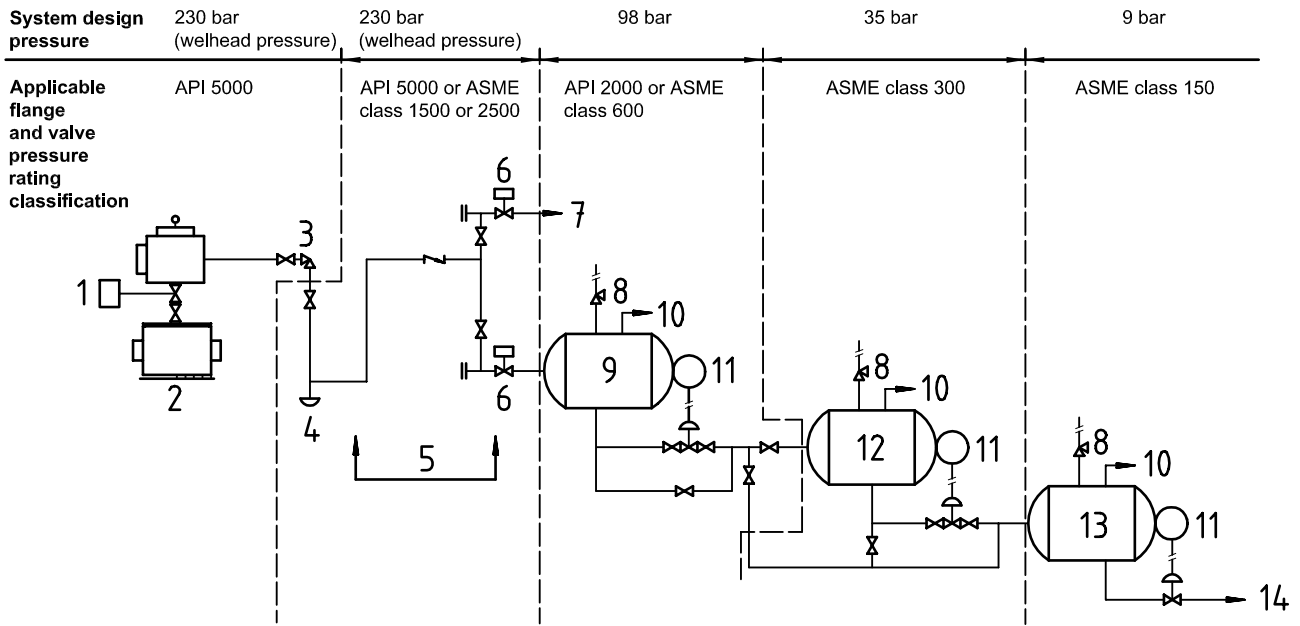
## 4.3 Demarcation between systems with different pressure ratings

**4.3.1** Normally, after the well-stream leaves the wellhead the pressure is reduced in stages.

After the pressure is reduced, process components of lower pressure ratings may be used. A typical example is shown in Figure 1.

**4.3.2** A pressure-containing process component shall either be designed to withstand the maximum internal pressure which can be exerted on it under any conditions, or shall be protected by a pressure-relieving device. In this case, a pressure-relieving device means a safety relief valve or a rupture disc. In general, when determining if pressure-relieving devices are needed, high-pressure shutdown valves, check valves, control valves or other such devices should not be considered as preventing overpressure of process components.

**4.3.3** Pressure-rating boundaries shall be indicated on piping and instrument diagrams. Each system component (vessels, flanges, pipe or accessories) shall be designed to withstand the highest pressure to which it could be subjected under any foreseeable conditions, or it shall be protected by a pressure-relieving device. Abnormal pressure conditions shall be considered, e.g. start-up, shutdown, surge, etc.



NOTE 1 Design temperature is 65 °C throughout.

NOTE 2 Required shutdown sensors are not shown.

NOTE 3 Flowline and manifold are designed for wellhead pressure.

NOTE 4 System design pressures may be limited by factors other than the flange and valve pressure classifications (i.e. pipe wall thickness, separator design pressure, etc.).

NOTE 5 Only where spare relief valves are installed may upstream isolation valves be installed, and then it is essential that all isolation valves are interlocked to ensure that the pressurized system is protected at all times.

**Key**

- |                           |                           |                               |
|---------------------------|---------------------------|-------------------------------|
| 1 Upper master gate valve | 6 Shutdown valve          | 11 Level controller           |
| 2 Wellhead                | 7 To other systems        | 12 Medium pressure separator  |
| 3 Wing choke              | 8 Pressure safety valve   | 13 Low pressure separator     |
| 4 Flow tee                | 9 High pressure separator | 14 Treating, storage or sales |
| 5 Manifold                | 10 Gas outlet             |                               |

**Figure 1 — Example of a process system, denoting flange and valve pressure-rating changes**

## 4.4 Corrosion considerations

### 4.4.1 General

Detailed corrosion-control practices for platform piping systems are outside the scope of this International Standard. Such practices should, in general, be developed by corrosion control specialists. Platform piping systems should, however, be designed to accommodate and be compatible with the corrosion control practices described below. Recommendations for corrosion-resistant materials and mitigation practices are given in the appropriate clauses of this International Standard.

The corrosivity of process streams may change over time. The possibility of changing conditions should be considered at the design stage.

### 4.4.2 Mass loss corrosion

Carbon steel platform piping systems may corrode under some process conditions. Production process streams containing water, brine, carbon dioxide (CO<sub>2</sub>), hydrogen sulfide (H<sub>2</sub>S) or oxygen (O<sub>2</sub>), or combinations of these, may be corrosive to metals used in system components. The type of attack (uniform metal loss, pitting, corrosion-erosion, etc.) as well as the specific corrosion rate can vary in the same system, and can vary over time. The corrosivity of a process stream is a complex function of many variables, including:

- a) hydrocarbon, water, salt and corrosive gas content;
- b) hydrocarbon wettability;
- c) flow velocity, flow regime and piping configuration;
- d) temperature, pressure and pH;
- e) solids content (sand, mud, bacterial slime and microorganisms, corrosion products, and scale).

Corrosivity predictions are very qualitative and may be unique for each system. Some corrosivity information for corrosive gases found in production streams is shown in Table 1.

Table 1 is intended only as a general guide for corrosion mitigation considerations and not for specific corrosivity predictions. Corrosion inhibition is an effective mitigation procedure when corrosive conditions are predicted or anticipated (see 5.1.2).

**Table 1 — Qualitative guideline for mass loss corrosion of steel**

Corrosive gas	Solubility <sup>a</sup> ratio × 10 <sup>-6</sup>	Limiting values in brine	
		Non-corrosive ratio × 10 <sup>-6</sup>	Corrosive ratio × 10 <sup>-6</sup>
Oxygen (O <sub>2</sub> )	8	< 0,005	> 0,025
Carbon dioxide (CO <sub>2</sub> )	1 700	< 600	> 1 200
Hydrogen sulfide (H <sub>2</sub> S)	3 900	See Note	See Note

NOTE No limiting values for mass loss corrosion by hydrogen sulfide are shown in this table because the amount of carbon dioxide and/or oxygen greatly influences the metal loss corrosion rate. Hydrogen sulfide alone is usually less corrosive than carbon dioxide due to the formation of an insoluble iron sulfide film which tends to reduce metal mass loss corrosion.

<sup>a</sup> Solubility ratio by volume. Solubility at 20 °C in distilled water at 1 atm partial pressure. Oxygen (O<sub>2</sub>) is for 1 atm air pressure. Source: [3].