

Designation: C 1067 - 00

Standard Practice for Conducting A Ruggedness or Screening Program for Test Methods for Construction Materials¹

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1. Scope

1.1 This practice covers a procedure for detecting sources of variation in a test method. The procedure should be used during the development of a test method, before the interlaboratory study is executed, such as those in Practices C 670, C 802, and E 691. Interlaboratory studies can be expensive to execute. Resources will probably be more efficiently used if sources of variation in a test method are eliminated prior to performing the interlaboratory study. The procedure also is useful for determining sources of variation in an existing test method that has been found to have poor precision.

1.2 This practice covers, in very general terms, techniques for planning, collecting data, and analyzing results from a few laboratories. Annex A1 provides the details of the procedure with an example and Annex A2 gives the theoretical background.

1.3 The practice does not give information pertinent to estimating within- or between-laboratory precision.

1.4 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

2. Referenced Documents

2.1 ASTM Standards:

- C 670 Practice for Preparing Precision and Bias Statements for Test Methods for Construction Materials²
- C 802 Practice for Conducting an Interlaboratory Test Program to Determine the Precision of Test Methods for Construction Materials²

E 456 Terminology Relating to Quality and Statistics³

- **E 691** Practice for Conducting an Interlaboratory Study to Determine the Precision of a Test Method³
- E 1169 Guide for Conducting Ruggedness Tests³

3. Terminology

3.1 Definitions:

3.1.1 *determination value*, *n*—numerical quantity calculated as directed in the test method using direct measurements obtained in accordance with the procedures given in the test method.

3.1.2 *replication*, *n*—the act of obtaining two or more determination values under specified conditions. The number of replications must be finite and the scope of the replication operation may be narrow or broad, but must be specified.

3.1.3 For definitions of other statistical terms used in this standard, refer to Terminology E 456.

3.2 Definitions of Terms Specific to This Standard:

3.2.1 *factor*, n—an element in the test procedure or laboratory environment that is a potential source of variation in test results.

3.2.2 *ruggedness*, *adj*—the characteristic of a test method that produces test results that are not influenced by small differences in the testing procedure or environment.

3.2.3 *screening*, *n*—the detection of significant sources of variation as compared to chance variation.

3.2.4 *variable*, *n*—a number or quantity that varies.

4. Summary of Practice

4.1 The practice requires that the user develop, from theoretical or practical knowledge, or both, a list of factors that plausibly would cause significant variation in test results if the factors were not controlled. The technique is limited to the analysis of the effects seven factors and requires considerably less effort than would be required to collected data for seven factors in a full factorial study. Procedures exist for analysis of

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² Annual Book of ASTM Standards, Vol 04.02.

³ Annual Book of ASTM Standards, Vol 14.02.

smaller and larger numbers of factors (see Guide E 1169), but seven is a convenient number for many test methods for construction materials. The seven-factor analysis requires 16 determinations by each laboratory. The procedure can be usefully executed by a single laboratory, but sometimes additional information can be obtained if it is repeated in one or two additional laboratories.

4.2 The procedure requires that two levels of each factor be identified, then 16 determinations be done on a prescribed combinations of factor levels. The levels assigned to a factor may be quantitative or qualitative (for example, brass versus steel).

4.3 The disadvantage of this type of analysis is that the method only estimates simple effects of each factor and does not detect interactive effects among factors.

5. Significance and Use

5.1 The purpose of a ruggedness evaluation is to determining how sensitive the test method is to changes in levels of pertinent operating factors. Normally, operating conditions for a test method are defined along with an allowable tolerance. A ruggedness analysis determines that effect of worst-case variation in operating conditions within this tolerance range. The method then can be revised with smaller tolerances on operating conditions to improve the precision.

5.2 A major reason for poor precision in test methods is the lack of adequate control over the sources of variation in testing procedures or testing environments. These sources of variation often are not controlled adequately because they were not identified during the development of the test procedures.

5.3 All new test methods must be subjected to an interlaboratory program for purposes of developing a precision and bias statement. These programs can be expensive and lengthy, and the result may be that the determination is made that the method is too variable to be published without further revision. Interlaboratory studies typically give the subcommittee an indication that the method is too variable, but they do not usually give a clear picture of what is causing the variation. Application of this ruggedness practice using one or a few laboratories may be a much more economical way to determine these causes.

5.4 Many existing test methods were published before there was a requirement that precision and bias statements be developed. Since this became a requirement, most of these test methods have developed precision and bias statements, and the result is that many have been found to suffer from relatively large amount of variation. Use of this practice represents a relatively simple way to investigate the causes of variation in test methods, so that a subcommittee will have some guidance as to which parts of the test method need to be studied further for revision.

5.5 The procedure can be used for a program within a single laboratory, but involvement of at least three laboratories is recommended, particularly if the single laboratory were to be the one in which the test method was developed. This is particularly important for new test methods. The originating laboratory is so much a part of the development of the test method that it is difficult for it to be objective in spotting any problems in the clarity of the test method directions. Two additional laboratories will probably contribute fresh critical review of the validity of the test method and provide assistance in clarifying the instructions of the test method when needed.

6. Materials

6.1 The number and types of material shall cover the range of material properties to which the test method is applicable. The test method does not apply to material types or property values outside the range evaluated. Three to five materials will usually be sufficient.

6.1.1 Some preliminary testing may help the laboratories involved determine the materials that shall be used in the screening program.

7. Procedure

7.1 Determine the number of laboratories that will participate in the program and which materials each will use in the program. The maximum amount of information is obtained if all laboratories include all materials in their part of the program, however cost can be reduced by each laboratory using a different material. Caution must be exercised in interpreting the results since laboratory-dependent cannot be separated from material-dependent effects.

7.2 Factors that are likely to have the greatest effect on the variability in the test results are selected for study. Levels of these factors are determined, selecting the minimum and maximum levels that would plausibly occur in the execution of the test method if there were no particular efforts to control them. Only two levels are allowed. Levels often represent quantitative properties, such as temperature, pressure, etc, but they may also represent nonquantitative values, such as old vs new, wet vs dry, etc. In this standard, factors are assigned letter designations, A - G, and the two levels of each factor are designated with upper and lower cases of these letters, as in Table 1.

7.3 Assign combinations of factor levels to experimental determinations according to Table 1. The 8 determinations will be done in duplicate, therefore, the full study on each material will require 16 determinations.

7.4 Construct a 16 row by 16 column results matrix from the 16 determinations values $(d_1 - d_{16})$ as shown in Table 2. The absolute values of the determinations in each row are identical, only the signs vary. Calculate Z and W statistics as shown in the equations below.

$$Z_r = \sum_{i=1}^{16} d_i$$
, where d_i 's are the 16 results in each row (r). (1)

$$W_r = \frac{Z_r^2}{16} \tag{2}$$

TABLE 1 Pattern of Assigning Levels to Seven Factors

| | | | De | eterminati | on Numl | ber | | |
|--------|---|---|----|------------|---------|-----|---|---|
| Factor | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| А | а | а | а | а | А | А | А | А |
| В | b | b | В | В | b | b | В | В |
| С | С | С | С | С | С | С | С | C |
| D | D | D | d | d | d | d | D | D |
| E | е | E | е | E | E | е | E | е |
| F | F | f | f | F | F | f | f | F |
| G | G | g | g | G | g | G | G | g |

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| | | | | | | | | | | | | ` | 10/ | | | | | |
|-----|----------------|----------------|----------------|------------|----------------|----------------|----------------|----------------|----------------|-----------------|-----------------|------------------|------------------|-----------------|-----------------|-----------------|----------|----------------|
| | | Eight D | Determina | ations for | Replicat | e Set 1 | | | | Eig | ght Dete | mination | s for Rep | licate Se | et 2 | | | |
| row | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | Ζ | W |
| 1 | d ₁ | d ₂ | d ₃ | d_4 | d ₅ | d ₆ | d ₇ | d ₈ | d ₉ | d ₁₀ | d ₁₁ | d ₁₂ | d ₁₃ | d ₁₄ | d ₁₅ | d ₁₆ | Z_1 | W_1 |
| 2 | d_1 | d_2 | d_3 | d_4 | $-d_5$ | $-d_6$ | $-d_7$ | $-d_8$ | d ₉ | d ₁₀ | d ₁₁ | d ₁₂ | -d ₁₃ | $-d_{14}$ | $-d_{15}$ | $-d_{16}$ | Z_2 | W_2 |
| 3 | d_1 | d_2 | $-d_3$ | $-d_4$ | d_5 | d_6 | $-d_7$ | $-d_8$ | d_9 | d ₁₀ | $-d_{11}$ | -d ₁₂ | d ₁₃ | d ₁₄ | $-d_{15}$ | $-d_{16}$ | | W ₃ |
| 4 | d_1 | $-d_2$ | d_3 | $-d_4$ | d_5 | $-d_6$ | d_7 | $-d_8$ | d_9 | $-d_{10}$ | d ₁₁ | -d ₁₂ | d ₁₃ | $-d_{14}$ | | $-d_{16}$ | | W_4 |
| 5 | d_1 | d_2 | $-d_3$ | $-d_4$ | $-d_5$ | $-d_6$ | d ₇ | d ₈ | d ₉ | d ₁₀ | $-d_{11}$ | -d ₁₂ | -d ₁₃ | | d ₁₅ | d ₁₆ | Z_5 | W_5 |
| 6 | d_1 | $-d_2$ | d_3 | $-d_4$ | $-d_5$ | d_6 | $-d_7$ | d ₈ | d ₉ | $-d_{10}$ | d ₁₁ | $-d_{12}$ | -d ₁₃ | d ₁₄ | $-d_{15}$ | d ₁₆ | Z_6 | W_6 |
| 7 | d_1 | $-d_2$ | $-d_3$ | d_4 | d_5 | $-d_6$ | $-d_7$ | d ₈ | d ₉ | $-d_{10}$ | $-d_{11}$ | d ₁₂ | d ₁₃ | $-d_{14}$ | $-d_{15}$ | d ₁₆ | Z_7 | W_7 |
| 8 | d_1 | $-d_2$ | $-d_3$ | d_4 | $-d_5$ | d ₆ | d ₇ | $-d_8$ | d ₉ | $-d_{10}$ | $-d_{11}$ | d ₁₂ | -d ₁₃ | d ₁₄ | d ₁₅ | $-d_{16}$ | Z_8 | W_8 |
| 9 | d_1 | d_2 | d ₃ | d_4 | d_5 | d ₆ | d ₇ | d ₈ | $-d_9$ | $-d_{10}$ | $-d_{11}$ | -d ₁₂ | $-d_{13}$ | $-d_{14}$ | $-d_{15}$ | $-d_{16}$ | Z_9 | W_9 |
| 10 | d_1 | d_2 | d ₃ | d_4 | $-d_5$ | $-d_6$ | $-d_7$ | $-d_8$ | $-d_9$ | $-d_{10}$ | $-d_{11}$ | -d ₁₂ | d ₁₃ | d ₁₄ | d ₁₅ | d ₁₆ | Z_{10} | W_{10} |
| 11 | d_1 | d_2 | $-d_3$ | $-d_4$ | d_5 | d_6 | $-d_7$ | $-d_8$ | $-d_9$ | $-d_{10}$ | d ₁₁ | d ₁₂ | -d ₁₃ | $-d_{14}$ | d ₁₅ | d ₁₆ | Z_{11} | W_{11} |
| 12 | d_1 | $-d_2$ | d ₃ | $-d_4$ | d_5 | $-d_6$ | d ₇ | $-d_8$ | $-d_9$ | d ₁₀ | $-d_{11}$ | d ₁₂ | -d ₁₃ | d ₁₄ | $-d_{15}$ | d ₁₆ | Z_{12} | W_{12} |
| 13 | d_1 | d_2 | $-d_3$ | $-d_4$ | $-d_5$ | $-d_6$ | d ₇ | d ₈ | $-d_9$ | $-d_{10}$ | d ₁₁ | d ₁₂ | d ₁₃ | d ₁₄ | $-d_{15}$ | $-d_{16}$ | Z_{13} | W_{13} |
| 14 | d_1 | $-d_2$ | d ₃ | $-d_4$ | $-d_5$ | d_6 | $-d_7$ | d ₈ | $-d_9$ | d ₁₀ | $-d_{11}$ | d ₁₂ | d ₁₃ | $-d_{14}$ | d ₁₅ | $-d_{16}$ | Z_{14} | W_{14} |
| 15 | d_1 | $-d_2$ | $-d_3$ | d_4 | d_5 | $-d_6$ | $-d_7$ | d ₈ | $-d_9$ | d ₁₀ | d ₁₁ | -d ₁₂ | -d ₁₃ | d ₁₄ | d ₁₅ | $-d_{16}$ | | W_{15} |
| 16 | d_1 | $-d_2$ | $-d_3$ | d_4 | $-d_5$ | d_6 | d ₇ | $-d_8$ | $-d_9$ | d ₁₀ | d ₁₁ | -d ₁₂ | d ₁₃ | $-d_{14}$ | $-d_{15}$ | d ₁₆ | Z_{16} | W_{16} |

7.5 The W statistic for row 1 represents the simple sum of the determinations and are not used in this analysis. Statistics for rows 2–8 ($W_2 - W_8$) represent the effects of the seven factors. The statistic for row 9 (W_9) represent the total variation between the two replicate sets and is not used in this analysis. Statistics for rows 10 through 16 ($W_{10} - W_{16}$) are used to calculate the error variance (X), which then is used to calculate the test criterion (F) for each factor, as shown by the equations below. Calculations are summarized in Table 3.

$$X = \left(\sum_{r=10}^{16} W_r^2\right) / 7 \text{ ttps:} / \text{sta(3) dar}$$

 $F_f = \frac{W_r^2}{X}$, where F_f is the *F* statistic for the effect of factor $f(1-7, \text{ represented by } W_2 - W_8, \text{ respectively})$

7.6 A F value of ≥ 5.59 represents a significant effect for factor f at a probability of 5 % for drawing an erroneous (1067-00) conclusion. 8. Keywords

7.7 An example of an analysis of data representing results on 4 materials from 3 laboratories is shown in Annex A1.

TABLE 3 Summary of Statistics for Seven Factors and Random

| | | Error | |
|--------|-----------------------------|---------------------------------------|--|
| Factor | W | F | |
| А | W_{2} | W_2^2/X | |
| В | W_3 | W_3^2/X | |
| С | W_4 | W_4^2/X | |
| Е | W_5 | W_5^2/X | |
| F | W_6 | W_{6}^{2}/X | |
| G | W_7 | W_{7}^{2}/X | |
| ndhrd | ₩ ['] ₈ | W_{8}^{2}/X | |
| | W ₁₀ | | |
| | W_{11} | | |
| | W ₁₂ | | |
| | -W ₁₃ | $X = \Sigma(W^2)/7$, for W_{10-16} | |
| | W_{14} | | |
| | W_{15} | | |
| | Wie | | |

8.1 precision; ruggedness; test method; variation

(Mandatory Information)

ANNEXES

A1. EXAMPLE OF A RUGGEDNESS PROGRAM

A1.1 This annex describes the procedure for conducting a ruggedness evaluation using as an example a description of the ruggedness evaluation on a test method for the measurement of the viscosity of asphalt.

A1.2 As the first step in the ruggedness evaluation, each of the laboratories critically examined the procedure in the proposed test method. The objectives of the examination were as follows:

A1.2.1 To determine if the instructions are clear, concise, and complete,

A1.2.2 To decide which factors are likely to influence test results and therefore should be included in the study,

A1.2.3 To pick materials that cover the range of the property of interest for the range of physical forms of the materials to be tested, and

A1.2.4 To determine the proper levels to be evaluated for each of the chosen variables.

A1.3 In this example, representatives of the three laboratories, after familiarizing themselves with the test method as specified in A1.2, met and tried to improve the instructions for the viscosity method. They selected variables, materials, and levels that showed the effect of the variation. One of the laboratories measured viscosity at 24°C, 25°C, and 26°C and found that there was about a 10 % variation with a change of 1°C. This was considered too large so 24.6 and 25.4°C were selected as the lower and upper temperature levels for the ruggedness test. In the same manner, the effect of the other variables were evaluated and the two levels to be evaluated were determined.

NOTE A1.1-Seven variables were selected and placed in a systematic procedure called an incomplete Latin Square or a Youden Square (1). The variables are listed below and shown in a Youden Square in Table A1.1. This plan can evaluate the seven variables with eight determinations. Table A1.2 shows the variables and the levels selected for this example.

A1.4 Four materials were selected to cover the range of the test method and the viscosities were determined by each of the three laboratories with one replication. The results are displayed in Table A1.3. This plan required 16 determinations by each laboratory on each material or 64 determinations by each laboratory.

A1.5 Table A1.4 specifies the experimental plan for a Youden Square for seven factors. The theory of its use is covered in Annex A2. Table A1.4 consists of 16 rows and 16 columns of coefficients each equal to ± 1 and arranged in a definite pattern.

A1.6 To obtain Table A1.5, first copy one row from Table A1.3 16 times in the general format of Table A1.5 and then multiply each entry in the new table by the corresponding entry in Table A1.4. Table A1.5 is just such a table derived from the data for Material 1 and Laboratory 1 in Table A1.3.

A1.7 To obtain Table A1.6, add, with due regard to sign, each row of Table A1.5 to obtain the first column of Table A1.6 containing $Z_1 - Z_{16}$. Next, square each entry in column one of Table A1.6 to obtain the corresponding entry in column two and then divide each entry in column two of Table A1.6 by 16 to obtain the corresponding entry in column three. The first row, Z_1 , represents the sum of all viscosities for the first row in Table A1.5 and will not be used in this analysis. The second

TABLE A1.1 Pattern for Assigning Levels to Seven Factors

| | | D | etermina | tion Num | nber | | | |
|----------|---|---|----------|----------|------|---|---|---|
| Variable | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| A or a | а | а | а | а | А | А | А | А |
| B or b | b | b | В | В | b | b | В | В |
| C or c | С | С | С | С | С | С | С | С |
| D or d | D | D | d | d | d | d | D | D |
| E or e | е | E | е | E | E | е | E | е |
| F or f | F | f | f | F | F | f | f | F |
| G or g | G | g | g | G | g | G | G | g |

= 24.6°, the lower level of temperature. а

25.4°, the higher level of temperature. A

- = New viscometer tube. b
- В Worn viscometer tube =
- С 290-mm Hg, lower vacuum. =
- 310-mm Hg, higher vacuum. С
- Charge viscometer without stirring sample. d
- D Charge viscometer after stirring for 1 min. =
- Mount the viscometer vertically. е Е Mount the viscometer 3° from vertical. =
- Charge with meniscus 1 mm above line. f
- F Charge with meniscus 1 mm below line. =
- Hold viscometer in bath 10 min less than normal before testing.
- Hold viscometer in bath 10 min longer than normal before testing.

row, Z_2 , is the algebraic addition of the second row in Table A1.5 and measures the effect of temperature. In the same manner, the third row, Z_3 , measures the effect of the age of the viscometer. The fourth row, Z_4 , measures the effect of vacuum level. The fifth row, Z_5 , measures the effect of stirring. The sixth row, Z_6 , measures the effect of the viscometer being slanted. The seventh row, Z_7 , measures the effect of variation in meniscus level. The eighth row, Z_8 measures the effect of variation in time in the bath of the viscometer prior to testing. The ninth row, Z_0 , measures the variation between the first and second replication. Rows 10 through 16 $(Z_{10}-Z_{16})$ measure the factor differences that yield the estimate of error variance. By adding W_{10} through W_{16} we can estimate the error variance with seven degrees of freedom using Eq A1.1:

$$\chi = \sum_{i=10}^{16} W_{i}^{2} / 7\sigma^{2}$$
 (A1.1)

where:

= pooled sum of squares for error,

 χ = pooled sum of squares for error in th row, and σ^2 = true, but unknown error variance.

A1.7.1 By dividing χ into W_i^2/σ^2 , representing the sums of squares for the main factors, we can test for the significance of the *j*th factor difference as shown in Eq A1.2:

$$F_{j} = W_{j}^{2} / \sigma^{2} / \sum_{i=10}^{16} W_{i}^{2} / 7 \sigma^{2} = W_{j}^{2} / \sum_{i=10}^{16} W_{i}^{2} / 7$$
(A1.2)

A1.7.2 Eq A1.2 will have an F-distribution with 1 and 7 degrees of freedom.

A1.8 The pooled sum of squares for error was determined and compared with the sums of squares for each of the main factors or treatments. The ratio that is significant at the 0.05 level is 5.59.

A1.9 F values for each of the main factors were calculated for Tables A1.6-A1.17. The results of these calcula-tions are shown for all factors in Table A1.18. All ratios that were less than 5.59 are shown in the table as NS to show that they are not significant. Z_2 or the effect of temperature was found highly significant for every material and every laboratory indicating the importance of improved control of temperature. Z_4 or the effect of variation in vacuum showed five significant values indicating a need for tightened controls on vacuum. Z_6 or the effect of the viscometer deviating from the vertical position was significant in six of the laboratory-material combinations indicating the need for tightened controls on the position of the viscometer. Z_3 , Z_5 , Z_7 , and Z_8 showed some scattering of barely significant values but these were not judged to be of sufficient importance to require tighter controls.

A1.10 Representatives of the three laboratories met after completion of the laboratory work and the subsequent analysis. After discussion of the results, the decision was made that it was practical and desirable to control temperature, vacuum, and the angle of the viscosity tube to the following limits:

> Temperature 25 ± 0.1, °C Vacuum 300 ± 2, mm (Hg) and Angle with Horizontal 90 ± 1°

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| | | | Determinaton N | umber | | | | |
|------------------------------|------|------|----------------|-------|------|------|------|------|
| Variable | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Temperature °C | 24.6 | 24.6 | 24.6 | 24.6 | 25.4 | 25.4 | 25.4 | 25.4 |
| Age of Tube | New | New | Old | Old | New | New | Old | Old |
| Vacuum, mm Hg | 310 | 290 | 310 | 290 | 310 | 290 | 310 | 290 |
| Stirring | Yes | Yes | No | No | No | No | Yes | Yes |
| Angle with Horizontal Degree | 90 | 87 | 90 | 87 | 87 | 90 | 87 | 90 |
| Fill line, mm | 4 | 6 | 6 | 4 | 4 | 6 | 6 | 4 |
| Time in Bath, min | 40 | 20 | 20 | 40 | 20 | 40 | 40 | 20 |

TABLE A1.3 Raw Data for Viscosity Example Seven Factors With Replication

| | | | | | | | | Visc | osity | | | | | | | |
|----------|------|------|-----------|------------|-------------|----------|------|------------|-------|------|----------|-------------|------------|----------|------|------|
| Material | | | First Rep | olicate De | eterminatio | on Numbe | r | | | | Second F | Replicate D | eterminati | on Numbe | er | |
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| | | | | | | | | Laboratory | 1 | | | | | | | |
| 1 | 2370 | 2258 | 2355 | 2185 | 1825 | 1845 | 1820 | 1830 | 2320 | 2275 | 2350 | 2380 | 1840 | 1850 | 1825 | 1820 |
| 2 | 520 | 495 | 519 | 480 | 401 | 404 | 398 | 402 | 492 | 516 | 490 | 522 | 390 | 408 | 402 | 395 |
| 3 | 4205 | 4006 | 4191 | 3846 | 3212 | 3284 | 3185 | 3221 | 4200 | 4160 | 4130 | 4020 | 3218 | 3180 | 3280 | 3280 |
| 4 | 1075 | 1061 | 1060 | 961 | 803 | 793 | 801 | 805 | 1050 | 1070 | 1015 | 1000 | 808 | 790 | 795 | 805 |
| | | | | | | | | Laboratory | 2 | | | | | | | |
| 1 | 2350 | 2240 | 2335 | 2165 | 1805 | 1825 | 1800 | 1810 | 2280 | 2310 | 2400 | 2120 | 1825 | 1806 | 1809 | 1812 |
| 2 | 540 | 515 | 539 | 500 | 421 | 424 | 418 | 422 | 518 | 545 | 524 | 492 | 410 | 425 | 430 | 420 |
| 3 | 4235 | 4036 | 4121 | 3876 | 3242 | 3314 | 3117 | 3250 | 4250 | 4142 | 3960 | 4205 | 3310 | 3112 | 3240 | 3117 |
| 4 | 1102 | 1040 | 1085 | 980 | 820 | 811 | 824 | 828 | 1110 | 1125 | 1040 | 1050 | 825 | 804 | 816 | 835 |
| | | | | | | | | Laboratory | 3 | | | | | | | |
| | | | | | | | | | | | | | | | | |
| 1 | 2390 | 2278 | 2375 | 2205 | 1845 | 1865 | 1840 | 1850 | 2400 | 2268 | 2350 | 2250 | 1860 | 1850 | 1870 | 1845 |
| 2 | 510 | 485 | 509 | 470 | 391 | 394 | 388 | 392 | 505 | 482 | 510 | 480 | 395 | 390 | 385 | 392 |
| 3 | 4200 | 3975 | 4160 | 3816 | 3190 | 3246 | 3150 | 3200 | 4180 | 3990 | 4140 | 3890 | 3200 | 3180 | 3220 | 3195 |
| 4 | 1050 | 990 | 1035 | 930 | 786 | 766 | 775 | 780 | 1040 | 980 | 1050 | 970 | 780 | 760 | 785 | 782 |

TABLE A1.4 Pattern for Assigning Levels to Seven Factors with Replication

| | | | | Replic | ate 1 | | | | | | | Replic | ate 2 | | | |
|---------------|-------------|----------------|----------------|-----------------------|-----------------------|-----------------------|-----|----------------|--------|---------------------|-----|-----------------|-----------------|------------------------|-----------------|-----------------|
| | 1 | 2 | 3 | 4 | 5 | 6 | AST | <u>/ C18</u> | 67-00 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| | X_1 | X ₂ | X ₃ | <i>X</i> ₄ | <i>X</i> ₅ | <i>X</i> ₆ | X7 | X ₈ | 775 X9 | 165 X ₁₀ | X11 | X ₁₂ | X ₁₃ | <i>X</i> ₁₄ | X ₁₅ | X ₁₆ |
| Z_1 | Independent | 1 | 5. iteri.a | 1 | 8 stand | 1 | 1 I | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Z_2 | 1 | 1 | 1 | 1 | -1 | -1 | -1 | -1 | 1 | 1 | 1 | 1 | -1 | -1 | -1 | -1 |
| Z_3 | 1 | 1 | -1 | -1 | 1 | 1 | -1 | -1 | 1 | 1 | -1 | -1 | 1 | 1 | -1 | -1 |
| Z_4 | 1 | -1 | 1 | -1 | 1 | -1 | 1 | -1 | 1 | -1 | 1 | -1 | 1 | -1 | 1 | -1 |
| Z_5 | 1 | 1 | -1 | -1 | -1 | -1 | 1 | 1 | 1 | 1 | -1 | -1 | -1 | -1 | 1 | 1 |
| Z_6 | 1 | -1 | 1 | -1 | -1 | 1 | -1 | 1 | 1 | -1 | 1 | -1 | -1 | 1 | -1 | 1 |
| Z_7 | 1 | -1 | -1 | 1 | 1 | -1 | -1 | 1 | 1 | -1 | -1 | 1 | 1 | -1 | -1 | 1 |
| Z_8 | 1 | -1 | -1 | 1 | -1 | 1 | 1 | -1 | 1 | -1 | -1 | 1 | -1 | 1 | 1 | -1 |
| Z_9 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -1 | -1 | -1 | -1 | -1 | -1 | -1 | -1 |
| Z_{10} | 1 | 1 | 1 | 1 | -1 | -1 | -1 | -1 | -1 | -1 | -1 | -1 | 1 | 1 | 1 | 1 |
| Z_{11} | 1 | 1 | -1 | -1 | 1 | 1 | -1 | -1 | -1 | -1 | 1 | 1 | -1 | -1 | 1 | 1 |
| Z_{12} | 1 | -1 | 1 | -1 | 1 | -1 | 1 | -1 | -1 | 1 | -1 | 1 | -1 | 1 | -1 | 1 |
| Z_{13}^{12} | 1 | 1 | -1 | -1 | -1 | -1 | 1 | 1 | -1 | -1 | 1 | 1 | 1 | 1 | -1 | -1 |
| Z_{14}^{13} | 1 | -1 | 1 | -1 | -1 | 1 | -1 | 1 | -1 | 1 | -1 | 1 | 1 | -1 | 1 | -1 |
| Z_{15} | 1 | -1 | -1 | 1 | 1 | -1 | -1 | 1 | -1 | 1 | 1 | -1 | -1 | 1 | 1 | -1 |
| Z_{16}^{13} | 1 | -1 | -1 | 1 | -1 | 1 | 1 | -1 | -1 | 1 | 1 | -1 | 1 | -1 | -1 | 1 |

With these changes an interlaboratory study was made on the method.

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TABLE A1.5 Matrix Based on Table A1.4 for Laboratory I, Material 1

NOTE 1—The data contained in Tables A1.7-A1.17 is derived from matrices constructed as illustrated by this table for each of the remaining eleven laboratory-material combinations from Table A1.3.

| | | | Repl | icate 1 | | | | | | | Repl | icate 2 | | | |
|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|----------------|------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|-----------------|
| <i>X</i> ₁ | <i>X</i> ₂ | <i>X</i> ₃ | <i>X</i> ₄ | <i>X</i> ₅ | <i>X</i> ₆ | <i>X</i> ₇ | X ₈ | <i>X</i> 9 | <i>X</i> ₁₀ | <i>X</i> ₁₁ | <i>X</i> ₁₂ | <i>X</i> ₁₃ | <i>X</i> ₁₄ | <i>X</i> ₁₅ | X ₁₆ |
| 2370 | 2258 | 2355 | 2185 | 1825 | 1845 | 1820 | 1830 | 2320 | 2275 | 2350 | 2380 | 1840 | 1850 | 1825 | 1820 |
| 2370 | 2258 | 2355 | 2185 | -1825 | -1845 | -1820 | -1830 | 2320 | 2275 | 2350 | 2380 | -1840 | -1850 | -1825 | -1820 |
| 2370 | 2258 | -2355 | -2185 | 1825 | 1845 | -1820 | -1830 | 2320 | 2275 | -2350 | -2380 | 1840 | 1850 | -1825 | -1820 |
| 2370 | -2258 | 2355 | -2185 | 1825 | -1845 | 1820 | -1830 | 2320 | -2275 | 2350 | -2380 | 1840 | -1850 | 1825 | -1820 |
| 2370 | 2258 | -2355 | -2185 | -1825 | -1845 | 1820 | 1830 | 2320 | 2275 | -2350 | -2380 | -1840 | -1850 | 1825 | 1820 |
| 2370 | -2258 | 2355 | -2185 | -1825 | 1845 | -1820 | 1830 | 2320 | -2275 | 2350 | -2380 | -1840 | 1850 | -1825 | 1820 |
| 2370 | -2258 | -2355 | 2185 | 1825 | -1845 | -1820 | 1830 | 2320 | -2275 | -2350 | 2380 | 1840 | -1850 | -1825 | 1820 |
| 2370 | -2258 | -2355 | 2185 | -1825 | 1845 | 1820 | -1830 | 2320 | -2275 | -2350 | 2380 | -1840 | 1850 | 1825 | -1820 |
| 2370 | 2258 | 2355 | 2185 | 1825 | 1845 | 1820 | 1830 | -2320 | -2275 | -2350 | -2380 | -1840 | -1850 | -1825 | -1820 |
| 2370 | 2258 | 2355 | 2185 | -1825 | -1845 | -1820 | -1830 | -2320 | -2275 | -2350 | -2380 | 1840 | 1850 | 1825 | 1820 |
| 2370 | 2258 | -2355 | -2185 | 1825 | 1845 | -1820 | -1830 | -2320 | -2275 | 2350 | 2380 | -1840 | -1850 | 1825 | 1820 |
| 2370 | -2258 | 2355 | -2185 | 1825 | -1845 | 1820 | -1830 | -2320 | 2275 | -2350 | 2380 | -1840 | 1850 | -1825 | 1820 |
| 2370 | 2258 | -2355 | -2185 | -1825 | -1845 | 1820 | 1830 | -2320 | -2275 | 2350 | 2380 | 1840 | 1850 | -1825 | -1820 |
| 2370 | -2258 | 2355 | -2185 | -1825 | 1845 | -1820 | 1830 | -2320 | 2275 | -2350 | 2380 | 1840 | -1850 | 1825 | -1820 |
| 2370 | -2258 | -2355 | 2185 | 1825 | -1845 | -1820 | 1830 | -2320 | 2275 | -2350 | -2380 | -1840 | 1850 | 1825 | -1820 |
| 2370 | -2258 | -2355 | 2185 | -1825 | 1845 | 1820 | -1830 | -2320 | 2275 | -2350 | -2380 | 1840 | -1850 | -1825 | 1820 |

TABLE A1.6 Results of Calculations for Matrix Due to Laboratory 1 and Material 1

| $Z_1 = 33\ 148$ | $Z_1^2 = 1\ 098\ 789\ 904$ | $W_1^2 = 68\ 674\ 369$ |
|---------------------|----------------------------|------------------------|
| $Z_2 = 3838$ | $Z_2^2 = 14730244$ | $W_2^2 = 920\ 640.25$ |
| Z ₃ = 18 | $Z_3^2 = 324$ | $W_3^2 = 20.25$ |
| $Z_4 = 262$ | $Z_4^2 = 68\ 644$ | $W_4^2 = 4\ 290.25$ |
| $Z_5 = -112$ | $Z_5^2 = 12544$ | $W_5^2 = 784$ |
| $Z_6 = 332$ | $Z_6^2 = 110224$ | $W_6^2 = 6889$ |
| $Z_7 = -8$ | $Z_7^2 = 64$ | $W_7^2 = 4$ |
| Z ₈ = 42 | $Z_8^2 = 1.764$ | $W_8^2 = 110.25$ |
| $Z_9 = -172$ | $Z_9^2 = 29584$ | $W_9^2 = 1849$ |
| $Z_{10} = -142$ | $Z_{10}^2 = 20.164$ | $W_{10}^2 = 1\ 260.25$ |
| $Z_{11} = 198$ | $Z_{11}^2 = 39\ 204$ | $W_{11}^2 = 2450.25$ |
| $Z_{12} = 242$ | $Z_{12}^2 = 58\ 564$ | $W_{12}^2 = 3\ 660.25$ |
| $Z_{13} = 248$ | $Z_{13}^2 = 61504$ | $W_{13}^2 = 3844$ |
| $Z_{14} = 292$ | $Z_{14}^{2} = 85\ 264$ | $W_{14}^{2} = 5329$ |
| $Z_{15} = -128$ | $Z_{15}^{2} = 16384$ | $W_{15}^2 = 1.024$ |
| $Z_{16} = -138$ | $Z_{16}^2 = 19044$ | $W_{16}^2 = 1\ 190.25$ |
| | | |

https://standards.iteh.ai/catalog/standards/sist/a3fb14d1-7752-4653-b9c7-748f4c1adc4e/astm-c1067-00

| TABLE A1.7 | Results of Calculations for Matrix due to |
|------------|---|
| | Laboratory 1 and Material 2 |

| $Z_1 = 7234$ | $Z_1^2 = 52\ 330\ 756$ | $W_1^2 = 3270672.25$ |
|-----------------------|------------------------|----------------------|
| $Z_2 = 834$ | $Z_2^2 = 695\ 556$ | $W_2^2 = 43\ 472.25$ |
| Z ₃ = 18 | $Z_3^2 = 324$ | $W_3^2 = 20.25$ |
| $Z_4 = -10$ | $Z_4^2 = 100$ | $W_4^2 = 6.25$ |
| $Z_5 = 6$ | $Z_5^2 = 36$ | $W_5^2 = 2.25$ |
| $Z_6 = 26$ | $Z_6^2 = 676$ | $W_6^2 = 42.25$ |
| $Z_7 = -30$ | $Z_7^2 = 900$ | $W_7^2 = 56.25$ |
| Z ₈ = 18 | $Z_8^2 = 324$ | $W_8^2 = 20.25$ |
| $Z_9 = 4$ | $Z_9^2 = 16$ | $W_9^2 = 1.00$ |
| $Z_{10} = -16$ | $Z_{10}^2 = 256$ | $W_{10}^2 = 16$ |
| $Z_{11} = 24$ | $Z_{11}^2 = 576$ | $W_{11}^2 = 36$ |
| $Z_{12} = 124$ | $Z_{12}^2 = 15\ 376$ | $W_{12}^2 = 961$ |
| Z ₁₃ = 16 | $Z_{13}^2 = 256$ | $W_{13}^2 = 16$ |
| Z ₁₄ = 116 | $Z_{14}^2 = 13\ 456$ | $W_{14}^2 = 841$ |
| $Z_{15} = 4$ | $Z_{15}^2 = 16$ | $W_{15}^2 = 1$ |
| $Z_{16} = -48$ | $Z_{16}^2 = 2\ 304$ | $W_{16}^2 = 144$ |