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# INTERNATIONAL STANDARD

## NORME INTERNATIONALE



## iTeh STANDARD PREVIEW

Optical fibres – Part 1-48: Measurement methods and test procedures – Polarization mode dispersion

IEC 60793-1-48:2017

Fibres optiques – 75146ccceb54/iec-60793-1-48-2017 Partie 1-48: Méthodes de mesure et procédures d'essai – Dispersion de mode de polarisation





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Edition 3.0 2017-08

# INTERNATIONAL STANDARD

## NORME INTERNATIONALE



## Optical fibres – **iTeh STANDARD PREVIEW** Part 1-48: Measurement methods and test procedures – Polarization r

Part 1-48: Measurement methods and test procedures – Polarization mode dispersion

IEC 60793-1-48:2017

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## Part 1-48: Measurement methods and test procedures – Polarization mode dispersion

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International Standard IEC 60793-1-48 has been prepared by subcommittee 86A: Fibres and cables, of IEC technical committee 86: Fibre optics.

This third edition cancels and replaces the second edition published in 2007. It constitutes a technical revision. This edition includes the following significant technical change with respect to the previous edition:

a) removal of the SOP approach.

The text of this standard is based on the following documents:

CDV	Report on voting
86A/1678/CDV	86A/1766/RVC

Full information on the voting for the approval of this standard can be found in the report on voting indicated in the above table.

This publication has been drafted in accordance with the ISO/IEC Directives, Part 2.

This International Standard is to be read in conjunction with IEC 60793-1-1:2008. A list of all parts in the IEC 60793 series, published under the general title Optical fibres, can be found on the IEC website.

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## INTRODUCTION

Polarization mode dispersion (PMD) causes an optical pulse to spread in the time domain. This dispersion could impair the performance of a telecommunications system. The effect can be related to differential phase and group velocities and corresponding arrival times  $\delta \tau$  of different polarization components of the signal. For a sufficiently narrow band source, the effect can be related to a differential group delay (DGD),  $\Delta \tau$ , between pairs of orthogonally polarized principal states of polarization (PSP) at a given wavelength. For broadband transmission, the delays bifurcate and result in an output pulse that is spread out in the time domain. In this case, the spreading can be related to the average of DGD values.

In long fibre spans, DGD is random in both time and wavelength since it depends on the details of the birefringence along the entire fibre length. It is also sensitive to time-dependent temperature and mechanical perturbations on the fibre. For this reason, a useful way to characterize PMD in long fibres is in terms of an average DGD value over an appropriately large optical frequency range, either RMS  $< \Delta \tau$ , the rms DGD over this frequency range, or MEAN  $<\Delta \tau$ , the (linear) mean of the DGD over this same frequency range. In principle, the average DGD value (RMS  $<\Delta \tau >$  or MEAN  $<\Delta \tau >$ ) does not undergo large changes for a given fibre from day to day or from source to source, unlike the parameters  $\delta \tau$  or  $\Delta \tau$ . In addition, the average DGD value is a useful predictor of lightwave system performance.

The term "PMD" is used both in the general sense of two polarization modes having different group velocities, and in the specific sense of the average DGD value (RMS  $<\Delta\tau$ > or MEAN < $\Delta\tau$ >). Although the DGD  $\Delta\tau$  or pulse broadening  $\Delta\delta$  is preferably averaged over frequency, for certain situations it may be averaged over time, or temperature.

The coupling length  $l_c$  is the length of fibre or cable at which appreciable coupling between the two polarization states begins to occur. If the fibre length L satisfies the condition  $L \ll l_c$ , mode coupling is negligible, and <u>ATZ</u> Scales with fibre length. The corresponding PMD https://standards.iteh.ai/catalog/standards/sit/c0fida86-3748-4b98-8376coefficient is 75146ccceb54/jec-60793-1-48-2017

short-length PMD coefficient =  $\langle \Delta \tau \rangle /L$ .

Fibres in practical systems nearly always have fibre lengths much greater than the coupling length and random mode coupling. When mode coupling is random,  $<\Delta \tau >$  scales with the square root of fibre length, and

long-length PMD coefficient =  $\langle \Delta \tau \rangle / \sqrt{L}$ .

## OPTICAL FIBRES -

## Part 1-48: Measurement methods and test procedures – Polarization mode dispersion

## 1 Scope

This part of IEC 60793 applies to three methods of measuring polarization mode dispersion (PMD), which are described in Clause 4. It establishes uniform requirements for measuring the PMD of single-mode optical fibre, thereby assisting in the inspection of fibres and cables for commercial purposes.

## 2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

IEC 60793-1-1, Optical fibres - Part 1-1. Measurement methods and test procedures - General and guidance

## (standards.iteh.ai)

IEC TR 61292-5, Optical amplifiers - Part 5: Polarization mode dispersion parameter -General information IEC 60793-1-48:2017

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ITU-T Recommendation G.650.2/5 Definitions and test4methods for statistical and non-linear related attributes of single-mode fibre and cable

## 3 Terms, definitions, symbols and abbreviated terms

#### 3.1 Terms and definitions

For the purposes of this document, the terms and definitions given in ITU-T Recommendation G.650.2 apply.

NOTE Further explanation of their use in this document is provided in IEC TR 61282-9.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- IEC Electropedia: available at http://www.electropedia.org/
- ISO Online browsing platform: available at http://www.iso.org/obp

#### 3.2 Symbols and abbreviated terms

Arg	Argument function
ASE	Amplified spontaneous emission
BBS	Broadband source
CFT	Cosine Fourier transform
c/c <sub>0</sub>	Velocity of light in vacuum/in free space
DGD	Differential group delay
DGD <sub>max</sub>	Maximum DGD value

DOP	Degree of polarization
Ε	Number of extrema in $R(\lambda)$ (method A)
EC	Extrema counting
$f(\Delta \tau)$	Maxwell probability distribution
FA	Fixed analyser (method A)
FCFT	Fast cosine Fourier transform
FT	Fourier transform
FUT	Fibre under test
GINTY	General analysis for method C
INTY	Interferometry method (method C)
I/O	Input/output
JME	Jones matrix eigenanalysis (method B)
k	Mode coupling factor
l <sub>c</sub>	Coupling length
L	Length of fibre/fibre cable test sample
LED	Light emitting diode
N	Total number of measurements/population of mode-coupled fibres/wavelength intervals
$P_{A}(\lambda)$	Optical power recorded with analyser in place (method A)
P <sub>F</sub>	Probability of exceeding DGD max ch.al)
$P_{B}(\lambda)$	Optical power recorded with analyser rotated 90 ° (method A)
$P_{TOT}(\lambda)$	Optical power recorded With analyser removed (method A) https://standards.iteh.ai/catalog/standards/sist/coffda86-3748-4698-8376-
$P_{X}(\tau)/P_{X}(\tau)$	Received power4in the4,two orthogonal SOP axes corresponding to the fringes in method C
PBS	Polarization beam splitter
PDL	Polarization dependent loss
PDV	Polarization dispersion vector
PMD	Polarization mode dispersion
PMD <sub>Q</sub>	Link design PMD value
PSA	Poincaré sphere analysis (method B)
PSP	Principle states of polarization
$R(\lambda)$	Output ratio from PMD measurement system (method A)
RBW	Resolution bandwidth
RTM	Reference test method
S	Normalized output Stokes vectors
SOP	State of polarization
SPE	Stokes parameter evaluation (method B)
Т	Jones matrix
<i>T</i> -1	Inverse of the Jones matrix
t <sub>c</sub>	Optical source coherence time (method C)
TINTY	Traditional analysis for method C
α	Single parameter which specifies a Maxwell distribution
v?	Chi any and variable

$\Delta \hat{h} / \Delta \hat{v} / \Delta \hat{q} / \Delta \hat{c}$	Finite differences computed from the Stokes vectors
δλ	Wavelength step size
$\Delta\lambda$	Optical source spectral width (full width half maximum (FWHM) unless otherwise noted)
δν	Optical frequency step size
$\Delta  heta$	Rotation angle on Poincaré sphere
δτ	Arrival time of different polarization components of a signal or pulse broadening
$\Delta\delta au_{max}$	Maximum $\delta  au$ value that can be measured
$\Delta\delta au_{min}$	Minimum $\delta  au$ value that can be measured
$\Delta \tau$	DGD value
$\Delta \tau_{\max}$	Maximum DGD
$<\Delta \tau >$	Average DGD over wavelength scan range or PMD value
$\sqrt{<\Delta \tau^2 >}$	r.m.s. DGD over wavelength scan range or PMD value (method C)
$<\Delta \tau >_0$	Maximum PMD specification that each fibre shall meet in a population of mode-coupled fibres
$<\Delta \tau >_t$	Average DGD over time
$<\Delta \tau >_{T}$	Average DGD over temperature PREVIEW
$<\Delta \tau >_{\lambda}$	Average DGD over wavelength itch.ai)
$\Delta \omega$	Angular frequency variation in method B
$\lambda$ $\lambda_0$	Test wavelength used to measure PMD https://standards.iteh.ai/catalog/standards/sist/c0ffda86-3748-4b98-8376- Central wavelength.of.the.light-source 2017
$\lambda_1/\lambda_2$	First/last wavelength in set of test wavelengths (or position of first/last maximum or minimum in $R(\lambda)$ in method A)
ν	Optical light frequency
$\rho_1   \rho_2$	Complex eigenvalues of $T(\omega + \Delta \omega)T^{-1}(\omega)$
σ	One-standard-deviation uncertainty
$\sigma_0$	r.m.s. width of the squared envelope of the autocorrelation interferogram (method C, GINTY)
$\sigma_{A}$	r.m.s. width of the autocorrelation envelope (method C)
$\sigma_{R}$	Second moment of FT data (method A)
$\sigma_x$	r.m.s. width of the squared envelope of the cross-correlation interferogram (method C, GINTY)
$\sigma_{ m e}$	r.m.s. width of the cross-correlation envelope (method C, TINTY)
ω	Angular optical frequency
Ω	PDV

## 4 General

## 4.1 Methods for measuring PMD

Three methods are described for measuring PMD (see Annexes A, B and C for more details). The methods are listed below in the order of their introduction. For some methods, multiple approaches of analysing the measured results are also provided.

- a) Method A
  - 1) Fixed analyser (FA)
  - 2) Extrema counting (EC)
  - 3) Fourier transform (FT)
  - 4) Cosine Fourier transform (CFT)
- b) Method B
  - 1) Stokes parameter evaluation (SPE)
  - 2) Jones matrix eigenanalysis (JME)
  - 3) Poincaré sphere analysis (PSA)
- c) Method C
  - 1) Interferometry (INTY)
  - 2) Traditional analysis (TINTY)
  - 3) General analysis (GINTY)

The PMD value is defined in terms of the differential group delay (DGD),  $\Delta \tau$ , which usually varies randomly with wavelength, and is reported as one or another statistical metric. Equation (1) is a linear average value of the DGD values and is used for the specification of optical fibre cable. Equation (2) is the root mean square value which is reported by some methods. Equation (3) can be used to convert one value to the other if the DGDs are assumed to follow a Maxwell random distribution.

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$$\left\langle \Delta \tau \right\rangle = \left(\frac{8}{3\pi}\right)^{1/2} \sqrt{\left\langle \Delta \tau \right\rangle} \tag{3}$$

Equation (3) applies only when the distribution of DGDs is Maxwellian, for instance when the fibre is randomly mode coupled. The generalized use of Equation (3) can be verified by statistical analysis. A Maxwell distribution may not be the case if there are point sources of elevated birefringence (relative to the rest of the fibre), such as a tight bend, or other phenomena that reduce the mode coupling, such as a continual reduced bend radius with fibre in tension. In these cases, the distribution of the DGDs will begin to resemble the square root of a non-central Chi-square distribution with three degrees of freedom. For these cases, the  $PMD_{\rm RMS}$  value will generally be larger relative to the  $PMD_{\rm MEAN}$  that is indicated in Equation (3). Time domain methods such as method C and method A, cosine Fourier transform, which are based on  $PMD_{\rm RMS}$ , can use Equation (3) to convert to  $PMD_{\rm MEAN}$ . If mode coupling is reduced, the resulting reported PMD value from these methods can exceed those that can be reported by the frequency domain measurements that report  $PMD_{\rm MEAN}$ , such as method B.

The PMD coefficient is the PMD value normalized to the fibre length. For normal transmission fibre, for which random mode coupling occurs and for which the DGDs are distributed as Maxwell random variables, the PMD value is divided by the square root of the length, and the PMD coefficient is reported in units of  $ps/\sqrt{km}$ . For some fibres with negligible mode coupling, such as polarization maintaining fibre, the PMD value is divided by the length, and the PMD coefficient is reported in units of  $ps/\sqrt{km}$ .

All methods are suitable for laboratory measurements of factory lengths of optical fibre and optical fibre cable. For all methods, changes in the deployment of the specimen can alter the results. For installed lengths of optical fibre cable that may be moving or vibrating, either method C or method B is appropriate (in an implementation capable of millisecond measurement time scales).

All methods require light sources that are controlled at one or more states of polarization (SOPs). All methods require injecting light across a broad spectral region (i.e. 50 nm to 200 nm wide) to obtain a PMD value that is characteristic of the region (i.e. 1 300 nm or 1 550 nm). The methods differ in:

- a) the wavelength characteristics of the source;
- b) the physical characteristics that are actually measured;
- c) the analysis methods.

Method A measures PMD by measuring a response to a change of narrowband light across a wavelength range. At the source, the light is linearly polarized at one or more SOPs. For each SOP, the change in output power that is filtered through a fixed polarization analyser, relative to the power detected without the analyser, is measured as a function of wavelength. The resulting measured function can be analysed in one of three ways:

- a) by counting the number of peaks and valleys (EC) of the curve and application of a formula that has been shown [1]<sup>1</sup> to agree with the average of DGD values, when the DGDs are distributed as Maxwellian. This analysis is considered as a frequency domain approach;
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- b) by taking the FT of the measured function. This FT is equivalent to the pulse spreading obtained by the broadband transmission of method C. Appropriate characterisation of the width of the FT function agrees with the average of DGD values, when the DGDs are distributed as Maxwellian;
- c) by taking the **CFT**/sofidthe idifference tof athe sinor malized spectra from two orthogonal analyser settings and calculating the romes of the squared envelope. The PMDRMS value is reported. This is equivalent to simulating the fringe pattern of the cross-correlation function that would result from interferometric measurements.

Method B measures  $\Delta \tau(\omega)$  by measuring a response to a change of narrowband light across a wavelength range. At the source, the light is linearly polarized at one or more SOPs. The Stokes vector of the output light is measured for each wavelength. The change of these Stokes vectors with angular optical frequency,  $\omega$ , and with the (optional) change in input SOP yields the DGD as a function of wavelength through relationships that are based on the following definitions:

$$\frac{ds(\omega)}{d\omega} = \Omega(\omega) \times s(\omega) \tag{4}$$

$$\Delta \tau(\omega) = |\Omega(\omega)| \tag{5}$$

where

- *s* is the normalized output Stokes vector;
- $\Omega$  is the polarization dispersion vector (PDV) in the direction of the PSPs;

 $\Delta \tau$  is the DGD.

For both the JME and PSA analysis approaches, three linear SOPs at nominally 0  $^{\circ}$ , 45  $^{\circ}$ , and 90  $^{\circ}$  (orthogonal on the Poincaré sphere) shall be launched for each wavelength.

<sup>&</sup>lt;sup>1</sup> Numbers in square brackets refer to the Bibliography

The JME approach is completed by transforming the output Stokes vectors to Jones matrices [2], appropriately combining the matrices at adjacent wavelengths and by a calculation using the eigenvalues of the result to obtain the DGD, by application of an argument formula, at the base frequency.

The PSA approach is completed by doing matrix algebra on the normalized output Stokes vectors to infer the rotation of the output Stokes vector on the Poincaré sphere at two adjacent wavelengths, using the application of an arcsine formula to obtain the DGD. The JME and PSA approaches are mathematically equivalent for common assumptions (see IEC TR 61282-9).

Method C is based on a broadband light source that is linearly polarized. The crosscorrelation of the emerging electromagnetic field is determined by the interference pattern of output light, i.e. the interferogram. The determination of the PMD delay for the wavelength range associated with the source spectrum is based on the envelope of the fringe pattern of the interferogram. Two analyses are available to obtain the PMD delay (see IEC TR 61282-9), both of which measure the  $PMD_{\text{RMS}}$  value:

- a) TINTY uses a set of specific operating conditions for its successful applications and a basic setup;
- b) GINTY uses no limiting operating conditions but, in addition to the same basic set-up as TINTY, it uses a modified setup.

The analysis approaches represent an evolution of the understanding of PMD. The GINTY is, for example, more complete than TINTY. The reproducibility of PMD depends on the PMD level and the wavelength range of the measurement [3]. Better relative reproducibility is achieved for broader wavelength ranges and higher PMD values for a given range. For measurements of higher PMD values, for example 0,5 ps, the differences in the analysis methods are less important than for the measurements of low PMD values.

Information common to all three methods is contained in Clauses 4 to 10, and requirements pertaining to each individual method appear in Annexes A, B, and C, respectively. IEC TR 61282-9 provides the mathematical formulations for all methods.

## 4.2 Reference test method

Method B is the reference test method (RTM), which shall be the one used to settle disputes.

#### 4.3 Applicability

PMD in fibre is a statistical parameter. IEC 60794-3 includes a statistical requirement on PMD, called  $PMD_Q$  or link design value that is based on sampled measurements of optical fibre cable and calculations for concatenated links. The PMD of a cabled fibre can vary from the PMD of the uncabled fibre due to effects of cable construction and processing. A limit on the  $PMD_Q$  of the uncabled fibre is, however, required to limit the  $PMD_Q$  on cabled fibre. Uncabled fibre  $PMD_Q$  less than half the cabled fibre  $PMD_Q$  limit is generally considered as a conservative rule. Alternative limits may be determined for particular constructions and stable cable processes.

The fibre or cable deployment should be selected so that externally induced mode coupling is minimized. Sources of such external mode coupling can be:

- a) excessive tension;
- b) excessive bending induced from
  - 1) fibre cross-overs on a shipping reel;
  - 2) crimping of fibre within a cable on a spool that is too small;
  - 3) too small a bend radius.
- c) excessive twist.