
**Natural gas — Calculation of compression
factor —**

Part 2:
Calculation using molar-composition analysis

*Gaz naturel — Calcul du facteur de compression —
Partie 2: Calcul par analyse de la composition molaire*
(standards.iteh.ai)

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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

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International Standard ISO 12213-2 was prepared by Technical Committee ISO/TC 193, *Natural gas*, Subcommittee SC 1, *Analysis of natural gas*.

ISO 12213 consists of the following parts, under the general title *Natural gas — Calculation of compression factor*:
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- *Part 1: Introduction and guidelines*
- *Part 2: Calculation using molar-composition analysis*
- *Part 3: Calculation using physical properties*

Annexes A to D form an integral part of this part of ISO 12213. Annexes E to G are for information only.

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Natural gas — Calculation of compression factor —

Part 2:

Calculation using molar-composition analysis

1 Scope

This International Standard specifies methods for the calculation of compression factors of natural gases, natural gases containing a synthetic admixture and similar mixtures at conditions under which the mixture can exist only as a gas.

This part of ISO 12213 specifies a method for the calculation of compression factors when the detailed composition of the gas by mole fractions is known, together with the relevant pressures and temperatures.

The method is applicable to pipeline quality gases within the ranges of pressure p and temperature T at which transmission and distribution operations normally take place, with an uncertainty of about $\pm 0,1$ %. It can be applied, with greater uncertainty, to wider ranges of gas composition, pressure and temperature (see annex E).

More detail concerning the scope and field of application of the method is given in part 1 of this International Standard.

2 Normative references

The following standards contain provisions which, through reference in this text, constitute provisions of this part of ISO 12213. At the time of publication, the editions indicated were valid. All standards are subject to revision, and parties to agreements based on this part of ISO 12213 are encouraged to investigate the possibility of applying the most recent editions of the standards indicated below. Members of IEC and ISO maintain registers of currently valid International Standards.

ISO 31-3:1992, *Quantities and units — Part 3: Mechanics*.

ISO 31-4:1992, *Quantities and units — Part 4: Heat*.

ISO 6976:1995, *Natural gas — Calculation of calorific values, density, relative density and Wobbe index from composition*.

ISO 12213-1:1997, *Natural gas — Calculation of compression factor — Part 1: Introduction and guidelines*.

3 Definitions

All definitions relevant to the use of this part of ISO 12213 are given in part 1.

4 Method of calculation

4.1 Principle

The method recommended uses an equation based on the concept that pipeline quality natural gas may be uniquely characterized for calculation of its volumetric properties by component analysis. This analysis, together with the pressure and temperature, are used as input data for the method.

The method uses a detailed molar-composition analysis in which all constituents present in amounts exceeding a mole fraction of 0,000 05 should be represented. Typically, this includes all alkane hydrocarbons up to about C₇ or C₈ together with nitrogen, carbon dioxide and helium.

For other gases, additional components such as water vapour, hydrogen sulfide and ethylene need to be taken into consideration (see reference [1] in annex G).

For manufactured gases, hydrogen and carbon monoxide are also likely to be significant components.

4.2 The AGA8-92DC equation

The compression factor is determined using the AGA8 detailed characterization equation (denoted hereafter as the AGA8-92DC equation). This is an extended virial-type equation. The equation is described in AGA Report No. 8^[1]. It may be written as

$$Z = 1 + B\rho_m - \rho_r \sum_{n=13}^{18} C_n^* + \sum_{n=13}^{58} C_n^* (b_n - c_n k_n \rho_r^{k_n}) \rho_r^{b_n} \exp(-c_n \rho_r^{k_n}) \quad \dots (1)$$

where

- Z is the compression factor;
- B is the second virial coefficient;
- ρ_m is the molar density (moles per unit volume);
- ρ_r is the reduced density;
- b_n, c_n, k_n are constants (see table B.1);
- C_n^* are coefficients which are functions of temperature and composition.

The reduced density ρ_r is related to the molar density ρ_m by the equation

$$\rho_r = K^3 \rho_m \quad \dots (2)$$

where K is a mixture size parameter.

The molar density can be written as

$$\rho_m = p/(ZRT) \quad \dots (3)$$

where

- p is the absolute pressure;
- R is the universal gas constant;
- T is the absolute temperature.

Z is calculated as follows: first the values of B and C_n^* ($n = 13$ to 58) are calculated, using relationships given in annex B. Equations (1) and (3) are then solved simultaneously for ρ_m and Z by a suitable numerical method (see figure B.1).

4.3 Input variables

The input variables required for use with the AGA8-92DC equation are the absolute pressure, absolute temperature and molar composition.

The composition is required, by mole fraction, of the following components: nitrogen, carbon dioxide, argon, methane, ethane, propane, *n*-butane, methyl-2-propane (iso-butane), *n*-pentane, methyl-2-butane (iso-pentane), hexanes, heptanes, octanes, nonanes, decanes, hydrogen, carbon monoxide, hydrogen sulfide, helium, oxygen and water.

NOTE — If the mole fractions of the heptanes, octanes, nonanes and decanes are unknown, then use of a composite C₆₊ fraction may be acceptable. The user should carry out a sensitivity analysis in order to test whether a particular approximation of this type degrades the result.

All components with mole fractions greater than 0,000 05 shall be accounted for. Trace components (such as ethylene) shall be treated as given in table 1.

If the composition is known by volume fractions, these shall be converted to mole fractions using the method given in ISO 6976. The sum of all mole fractions shall be unity to within 0,000 1.

4.4 Ranges of application

4.4.1 Pipeline quality gas

The ranges of application for pipeline quality gas are as defined below:

| | |
|--------------------------|---|
| absolute pressure | $0 \text{ MPa} \leq p \leq 12 \text{ MPa}$ |
| temperature | $263 \text{ K} \leq T \leq 338 \text{ K}$ |
| superior calorific value | $30 \text{ MJ}\cdot\text{m}^3 \leq H_S \leq 45 \text{ MJ}\cdot\text{m}^3$ |
| relative density | $0,55 \leq \rho \leq 0,80$ |

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The mole fractions of the natural-gas components shall be within the following ranges:

| | |
|---------------------|---|
| methane | $0,7 \leq x_{\text{CH}_4} \leq 1,00$ |
| nitrogen | $0 \leq x_{\text{N}_2} \leq 0,20$ |
| carbon dioxide | $0 \leq x_{\text{CO}_2} \leq 0,20$ |
| ethane | $0 \leq x_{\text{C}_2\text{H}_6} \leq 0,10$ |
| propane | $0 \leq x_{\text{C}_3\text{H}_8} \leq 0,035$ |
| butanes | $0 \leq x_{\text{C}_4\text{H}_{10}} \leq 0,015$ |
| pentanes | $0 \leq x_{\text{C}_5\text{H}_{12}} \leq 0,005$ |
| hexanes | $0 \leq x_{\text{C}_6} \leq 0,001$ |
| heptanes | $0 \leq x_{\text{C}_7} \leq 0,000 5$ |
| octanes plus | $0 \leq x_{\text{C}_{8+}} \leq 0,000 5$ |
| higher hydrocarbons | |
| hydrogen | $0 \leq x_{\text{H}_2} \leq 0,10$ |
| carbon monoxide | $0 \leq x_{\text{CO}} \leq 0,03$ |
| helium | $0 \leq x_{\text{He}} \leq 0,005$ |
| water | $0 \leq x_{\text{H}_2\text{O}} \leq 0,000 15$ |

Any component for which x_i is less than 0,000 05 can be neglected.

Minor and trace components are listed in table 1.

Table 1 — Minor and trace components

| Minor or trace component | Assigned component |
|---|--------------------|
| Oxygen | oxygen |
| Argon | argon |
| Hydrogen sulfide | hydrogen sulfide |
| Ethylene, acetylene | carbon dioxide |
| Propylene, propadiene | propane |
| Butenes, butadienes | <i>n</i> -butane |
| Neo-pentane, pentenes, benzene, cyclopentane | <i>n</i> -pentane |
| All C ₆ -isomers, cyclohexane, ethylbenzene, xylenes | <i>n</i> -hexane |
| All C ₇ -isomers, cycloheptane, toluene | <i>n</i> -heptane |
| All C ₈ -isomers | <i>n</i> -octane |
| All C ₉ -isomers | <i>n</i> -nonane |
| All C ₁₀ -isomers and all higher hydrocarbons | <i>n</i> -decane |

The method applies only to mixtures in the single-phase gaseous state (above the dew point) at the conditions of temperature and pressure of interest.

4.4.2 Wider ranges of application

The ranges of application tested beyond the limits given in 4.4.1 are:

| | |
|--------------------------|---|
| absolute pressure | $0 \text{ MPa} \leq p \leq 65 \text{ MPa}$ |
| temperature | $225 \text{ K} \leq T \leq 350 \text{ K}$ |
| relative density | $0,55 \leq d \leq 10,90$ |
| superior calorific value | $20 \text{ MJ}\cdot\text{m}^{-3} \leq H_s \leq 48 \text{ MJ}\cdot\text{m}^{-3}$ |

The allowable mole fractions of the major natural gas components are:

| | |
|----------------|---|
| methane | $0,50 \leq x_{\text{CH}_4} \leq 1,00$ |
| nitrogen | $0 \leq x_{\text{N}_2} \leq 0,50$ |
| carbon dioxide | $0 \leq x_{\text{CO}_2} \leq 0,30$ |
| ethane | $0 \leq x_{\text{C}_2\text{H}_6} \leq 0,20$ |
| propane | $0 \leq x_{\text{C}_3\text{H}_8} \leq 0,05$ |
| hydrogen | $0 \leq x_{\text{H}_2} \leq 0,10$ |

The limits for minor and trace gas components are as given in 4.4.1 for pipeline quality gas. For use of the method outside these ranges, see annex E.

4.5 Uncertainty

4.5.1 Uncertainty for pipeline quality gas

The uncertainty of results for use on all pipeline quality gas within the limits described in 4.4.1 is $\pm 0,1 \%$ (for the temperature range 263 K to 350 K and pressures up to 12 MPa) (see figure 1). For temperatures above 290 K and at pressures up to 30 MPa the uncertainty of the result is also $\pm 0,1 \%$.

For lower temperatures, the uncertainty of $\pm 0,1 \%$ is at least maintained for pressures up to about 10 MPa.

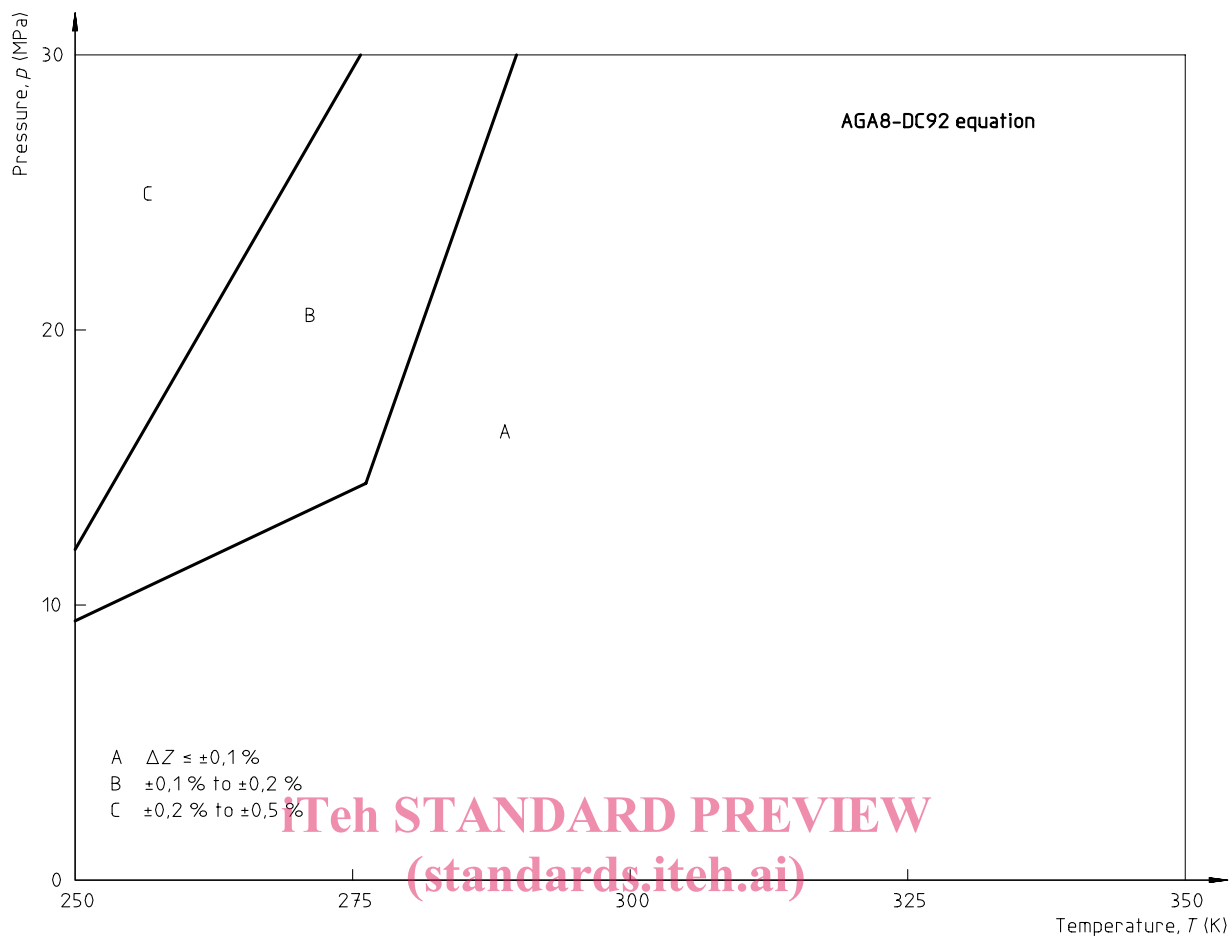


Figure 1 — Uncertainty limits for the calculation of compression factors (The uncertainty limits given are expected to be valid for natural gases and similar gases with $x_{\text{N}} \leq 0,20$, $x_{\text{CO}_2} \leq 0,20$, $x_{\text{C}_2\text{H}_6} \leq 0,10$ and $x_{\text{H}_2} \leq 0,10$, and for $30 \text{ MJ}\cdot\text{m}^{-3} \leq H_{\text{S}} \leq 45 \text{ MJ}\cdot\text{m}^{-3}$ and $0,55 \leq d \leq 0,80$)

This uncertainty level has been determined by comparison with the GERG databank of measurements of the compression factor for natural gases [2], [3]. A detailed comparison was also made with the GRI PVT data on gravimetrically prepared simulated natural-gas mixtures [4], [5].

The uncertainty of the measurements in both databanks used to test the method is of the order of $\pm 0,1\%$.

4.5.2 Uncertainty for wider ranges of application

The estimated uncertainties for calculations of compression factors beyond the limits of quality given in 4.4.1 are discussed in annex E.

4.5.3 Impact of uncertainties of input variables

Listed in table 2 are typical values for the uncertainties of the relevant input variables. These values may be achieved under optimum operating conditions.

As a general guideline only, an error propagation analysis using the uncertainties in the input variables produces an additional uncertainty of about $\pm 0,1\%$ in the result at 6 MPa and within the temperature range 263 K to 338 K. Above 6 MPa, the additional uncertainties are greater and increase roughly in direct proportion to the pressure.

Table 2 — Uncertainties of input variables

| Input variable | Absolute uncertainty |
|-----------------------------------|----------------------|
| Absolute pressure | $\pm 0,02$ MPa |
| Temperature | $\pm 0,15$ K |
| Mole fraction of | |
| inerts | $\pm 0,001$ |
| nitrogen | $\pm 0,001$ |
| carbon dioxide | $\pm 0,001$ |
| methane | $\pm 0,001$ |
| ethane | $\pm 0,001$ |
| propane | $\pm 0,000 5$ |
| butanes | $\pm 0,000 3$ |
| pentanes plus higher hydrocarbons | $\pm 0,000 1$ |
| hydrogen and carbon monoxide | $\pm 0,001$ |

4.5.4 Reporting of results

Results for compression factor and molar density shall be reported to four and to five places of decimals, respectively, together with the pressure and temperature values and the calculation method used (ISO 12213-2, AGA8-92DC equation). For verification of calculation procedures, it is useful to carry extra digits.

5 Suppliers of computer programmes

It is planned to make software available which implements this International Standard. Users are invited to contact their ISO member body or ISO Central Secretariat to enquire about the availability of such software.

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Annex A (normative)

Symbols and units

| Symbol | Meaning | Units |
|-------------|---|---|
| a_n | Constant in table B.1 | — |
| B | Second virial coefficient | $\text{m}^3 \cdot \text{kmol}^{-1}$ |
| B_{nij}^* | Mixture interaction coefficient [equations (B.1) and (B.2)] | — |
| B_n | Constant in table B.1 | — |
| c_n | Constant in table B.1 | — |
| C_n^* | Coefficients which are functions of temperature and composition | — |
| E_i | Characteristic energy parameter for i th component (table B.2) | K |
| E_j | Characteristic energy parameter for j th component (table B.2) | K |
| E_{ij} | Binary energy parameter for second virial coefficient | K |
| E_{ij}^* | Binary energy interaction parameter for second virial coefficient (table B.3) | — |
| F | Mixture high-temperature parameter | — |
| F_i | High-temperature parameter for i th component (table B.2) | — |
| F_j | High-temperature parameter for j th component (table B.2) | — |
| f_n | Constant in table B.1 | — |
| G | Mixture orientation parameter | — |
| G_i | Orientation parameter for i th component (table B.2) | — |
| G_j | Orientation parameter for j th component (table B.2) | — |
| G_{ij} | Binary orientation parameter | — |
| G_{ij}^* | Binary interaction parameter for orientation (table B.2) | — |
| g_n | Constant in table B.1 | — |
| H_S | Superior calorific value | $\text{MJ} \cdot \text{m}^3$ |
| K | Size parameter | $(\text{m}^3/\text{kmol})^{1/3}$ |
| K_i | Size parameter for i th component (table B.2) | $(\text{m}^3/\text{kmol})^{1/3}$ |
| K_j | Size parameter for j th component (table B.2) | $(\text{m}^3/\text{kmol})^{1/3}$ |
| K_{ij} | Binary interaction parameter for size (table B.3) | — |
| k_n | Constant in table B.1 | — |
| M | Molar mass | $\text{kg} \cdot \text{kmol}^{-1}$ |
| M_i | Molar mass of i th component | $\text{kg} \cdot \text{kmol}^{-1}$ |
| N | Number of components in gas mixture | — |
| n | An integer (from 1 to 58) | — |
| p | Absolute pressure | MPa |
| Q | Quadrupole parameter | — |
| Q_i | Quadrupole parameter for i th component | — |
| Q_j | Quadrupole parameter for j th component | — |
| q_n | Constant (table B.1) | — |
| R | Gas constant (= 0,008 314 510) | $\text{MJ} \cdot (\text{kmol} \cdot \text{K})^{-1}$ |
| S_i | Dipole parameter for i th component (table B.2) | — |
| S_j | Dipole parameter for j th component (table B.2) | — |
| s_n | Constant (table B.1) | — |

| Symbol | Meaning | Units |
|----------|---|----------------------|
| T | Absolute temperature | K |
| U | Mixture energy parameter | K |
| U_{ij} | Binary interaction parameter for mixture energy (table B.3) | — |
| u_n | Constant in table B.1 | — |
| W_i | Association parameter for i th component (table B.2) | — |
| W_j | Association parameter for j th component (table B.2) | — |
| w_n | Constant (table B.1) | — |
| x_i | Mole fraction of i th component in gas mixture | — |
| x_j | Mole fraction of j th component in gas mixture | — |
| Z | Compression factor | — |
| ρ | Mass density | kg·m ⁻³ |
| ρ_r | Reduced density of gas | — |
| ρ_m | Molar density | kmol·m ⁻³ |

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