

### **SLOVENSKI STANDARD** SIST EN 60825-1:2014

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Varnost laserskih izdelkov - 1. del: Klasifikacija opreme in zahteve (IEC 60825-1:2014)

Safety of laser products - Part 1: Equipment classification and requirements

Sicherheit von Lasereinrichtungen - Teil 1: Klassifizierung von Anlagen und Anforderungen **iTeh STANDARD PREVIEW** 

(standards.iteh.ai) Sécurité des appareils à laser - Partie 1: Classification des matériels et exigences

SIST EN 60825-1:2014 https://standards.iteh.ai/catalog/standards/sist/d7ae388f-fb35-4e30-8974-Ta slovenski standard je istoveten zi 620/sis EN-60825-1;2014

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13.280	Varstvo pred sevanjem
31.260	Optoelektronika, laserska oprema

Radiation protection **Optoelectronics**. Laser equipment

SIST EN 60825-1:2014

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### SIST EN 60825-1:2014

### EUROPEAN STANDARD NORME EUROPÉENNE EUROPÄISCHE NORM

### EN 60825-1

August 2014

ICS 13.110; 31.260

Supersedes EN 60825-1:2007

**English Version** 

### Safety of laser products - Part 1: Equipment classification and requirements (IEC 60825-1:2014)

Sécurité des appareils à laser - Partie 1: Classification des matériels et exigences (CEI 60825-1:2014) Sicherheit von Lasereinrichtungen - Teil 1: Klassifizierung von Anlagen und Anforderungen (IEC 60825-1:2014)

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### Foreword

The text of document 76/502/FDIS, future edition 3 of IEC 60825-1, prepared by IEC/TC 76 "Optical radiation safety and laser equipment" was submitted to the IEC-CENELEC parallel vote and approved by CENELEC as EN 60825-1:2014.

The following dates are fixed:

-	<ul> <li>latest date by which the document has to be implemented at national level by publication of an identical national standard or by endorsement</li> </ul>	(dop)	2015-03-19
-	latest date by which the national standards conflicting with the document have to be withdrawn	(dow)	2017-06-19

This document supersedes EN 60825-1:2007.

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The text of the International Standard IEC 60825-1:2014 was approved by CENELEC as a European Standard without any modification. SIST EN 60825-1:2014

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IEC 60027-1	https://standards.iteh	1.a <mark>i/6472</mark> 0g/st 7c16cf2620/	apdards/sist/d7ac3281fb3274230-8974- /sist-en-60825-1-2014
IEC 60065	144	NOTE	Harmonised as EN 60065.
IEC 60079 (Se	ries)	NOTE	Harmonised as EN 60079 (Series).
IEC 60204-1		NOTE	Harmonised as EN 60204-1.
IEC 60601-2-2	2	NOTE	Harmonised as EN 60601-2-22.
IEC 60825-2		NOTE	Harmonised as EN 60825-2.
IEC 60825-4		NOTE	Harmonised as EN 60825-4.
IEC 60825-12		NOTE	Harmonised as EN 60825-12.
IEC 60950 (Se	ries)	NOTE	Harmonised as EN 60950 (Series).
IEC 61010-1		NOTE	Harmonised as EN 61010-1.
IEC 61508 (Se	ries)	NOTE	Harmonised as EN 61508 (Series).
IEC 62115		NOTE	Harmonised as EN 62115.
IEC 62368-1		NOTE	Harmonised as EN 62368-1.
IEC/ISO 11553	3 (Series)	NOTE	Harmonised as EN ISO 11553 (Series).
ISO 11146-1		NOTE	Harmonised as EN ISO 11146-1.
ISO 12100		NOTE	Harmonised as EN ISO 12100.
ISO 13694		NOTE	Harmonised as EN ISO 13694.
ISO 13849 (Se	eries)	NOTE	Harmonised as EN ISO 13849 (Series).
ISO 15004-2:2	007	NOTE	Harmonised as EN ISO 15004-2:2007.
ISO 80000-1		NOTE	Harmonised as EN ISO 80000-1.

### Annex ZA

(normative)

## Normative references to international publications with their corresponding European publications

The following documents, in whole or in part, are normatively referenced in this document and are indispensable for its application. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies. NOTE 1 When an International Publication has been modified by common modifications, indicated by (mod), the relevant EN/HD applies.

NOTE 2 Up-to-date information on the latest versions of the European Standards listed in this annex is available here: www.cenelec.eu.

Publication	Year	Title EN/HD	Year
IEC 60050	series	International Electrotechnical Vocabulary -	series
IEC 62471 (mod)	-	Photobiological safety of lamps and lampEN 62471 systems	-

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Edition 3.0 2014-05

# INTERNATIONAL STANDARD

# NORME INTERNATIONALE



GROUP SAFETY PUBLICATION PUBLICATION GROUPÉE DE SÉCURITÉ

Safety of laser products -STANDARD PREVIEW Part 1: Equipment classification and requirements:

Sécurité des appareils à laser –<u>SIST EN 60825-1:2014</u> Partie 1: Classification des matériels et exigences f-fb35-4e30-8974fd7c16cf2620/sist-en-60825-1-2014

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### INTERNATIONAL ELECTROTECHNICAL COMMISSION

IEC 60825-1 Edition 3.0 2014-05

### SAFETY OF LASER PRODUCTS -

### Part 1: Equipment classification and requirements

### INTERPRETATION SHEET 1

This interpretation sheet has been prepared by IEC technical committee 76: Optical radiation safety and laser equipment.

The text of this interpretation sheet is based on the following documents:

(standard	S Report on voting
76/587/FDIS	76/593/RVD

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Full information on the voting for the approval of this interpretation sheet can be found in the report on voting indicated in the above table.

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### Subclause 4.3 Classification rules

This subclause is clarified by the following:

### Introduction

For some complex extended sources or irregular temporal emissions, the application of the rules of subclause 4.3 may require clarification because of changes from IEC 60825-1:2007.

NOTE 1 For the purpose of this interpretation sheet, the abbreviation "AE" is used for "accessible emission".

NOTE 2 The clarifications also apply in an equivalent way to MPE analysis, i.e. for Annex A.

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### 1 Subclause 4.3 b) Radiation of multiple wavelengths

See IEC 60825-1:2014/ISH2.

### 2 Subclause 4.3 c) Radiation from extended sources

When using the default (simplified) evaluation method (subclause 5.4.2) for wavelengths  $\geq$  400 nm and < 1 400 nm, the angle of acceptance may be limited to 100 mrad for determining the accessible emission to be compared against the accessible emission limit, except in the wavelength range 400 nm to 600 nm for durations longer than 100 s where the circular-cone angle of acceptance is not limited. When evaluating the emissions for comparison to the Class 3B AELs, the angle of acceptance is not limited.

### 3 Subclause 4.3 d) Non-uniform, non-circular or multiple apparent sources

In subclause 4.3 d), for comparison with the thermal retinal limits, the requirement to vary the angle of acceptance in each dimension might appear to contradict the labelling in Figure 1 and Figure 2 of subclause 5.4.3 where the field stop is labelled as circular.

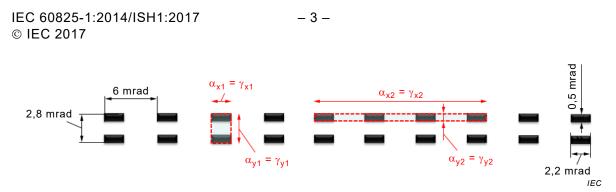
### Interpretation

A circular field stop is applicable for circularly symmetric images of the apparent source and for this case is consistent with the procedure given in subclause 4.3 d). For images of the apparent source that are not circularly symmetric, the simple example below clarifies the application of subclause 4.3 d). (standards.iteh.ai)

A circular field stop with an angular subtense equal to  $_4\alpha_{max}$  is, however, applicable for noncircularly symmetric profiles if the analysis performed according to subclause 4.3 d), following variation of the angle of acceptance in each dimension, results in a solution which is equal to  $\alpha_{max}$  in both dimensions.

As a general principle, for whatever emission duration t the AEL is determined (such as the pulse duration, the pulse group duration or the time base for averaging of the power), the same emission duration t is also used to calculate  $\alpha_{max}(t)$ .

The following example demonstrates the method described in subclause 4.3 d) to analyse irregular or complex images of a source. It is noted that the example is equivalent to the second part of the example ("Additional Remarks"; 6 mrad spacing instead of 3 mrad) B.9.1 of IEC TR 60825-14:2004 (however, for 6 mrad element spacing, the result in terms of which grouping is critical was not correct). The source is a diode array (Figure 1). The task is to determine the applicable AEL that limits the AE for Class 2. Each diode contributes a partial accessible emission AE of 1 mW that passes through a 7 mm aperture stop at the distance where the analysis is performed (i.e. a total power of 20 mW passes through the aperture stop), and the emission is continuous wave. The analysis requires determination of the most restrictive (maximum) ratio of AE over AEL by variation of the angle of acceptance in position and size to achieve different fields of view.



## Figure 1 – Image of a source pattern for the example of 20 emitters. Two possible groupings are defined by the respective angle of acceptance $\gamma_x$ and $\gamma_y$

The analysis of a sub-group of sources is associated with a certain value of  $\alpha$  for that group, and a certain accessible emission associated with that sub-group. For instance  $\alpha$  of a single element equals (1,5 mrad + 2,2 mrad)/2 = 1,85 mrad so that the AEL = 1,23 mW. The applicable AE = 1 mW and AE/AEL = 1 mW/1,23 mW = 0,8. For a vertical two-element group, as shown in the figure with  $\gamma_{x1}$  and  $\gamma_{y1}$ ,  $\alpha$  = (2,8 + 2,2)/2 = 2,5 mrad so that AEL = 1,66 mW; AE =  $2 \times 1$  mW = 2 mW and AE/AEL = 1,2, which is more restrictive than AE/AEL for only one element. For one row of 10 diodes  $\alpha$  = (1,5 + 56,2)/2 = 28,9 mrad, AEL = 19,2 mW, the AE =  $10 \times 1$  mW = 10 mW and AE/AEL = 0.5. Analysis of all possible groupings shows that the vertical two-element group has the maximum AE/AEL and therefore is the solution of the analysis. This means that the AEL of Class 2 is exceeded by a factor 1,2. Note that only a portion of the power of 20 mW that passes through the 7 mm aperture stop is considered as the AE (2 mW; as partial power within the angle of acceptance that is associated to the part of the image with the maximum ratio of AE/AEL) that is compared against the AEL. The entire array represents the highest ratio of AE/AEL in cases where the element spacing is sufficiently close, e.g. when the contributions of extra elements to the AE are not dominated by the increased AEL due to the larger subtended angle.

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For pulsed emission, for the determination of  $\alpha$  according to the above method (4.3 d)) where the ratio of AE to AEL is maximized, requirement 3) of 4.3 f) is not applied, i.e. the AEL<sub>single</sub> is not reduced by  $C_5$ . Due to the dependence of  $\alpha_{max}$  on emission duration *t*, the analysis of the image of the apparent source may result in different values of  $\alpha$  and of the partial accessible emission, depending which emission duration is analysed for the requirements of 4.3 f). For example, for emission durations shorter than 625 µs ( $\alpha_{max} = 5$  mrad), the maximum partial array to consider in the image analysis is a vertical two element group.

Ref.: Classification of extended source products according to IEC 60825-1, K. Schulmeister, ILSC 2015 Proceedings Paper, p 271 – 280; *Download: https://www.filesanywhere.com/fs/v.aspx?v=8b70698a595e75bcaa69* 

### 4 Subclause 4.3 f) 3) determination of $\alpha$

For an analysis of pulsed emission,  $\alpha_{max}$ , which is a function of time  $\alpha_{max}$  (t), limits both the value of  $\alpha$  for the determination of  $C_6(\alpha)$  as well as the angle of acceptance  $\gamma$  for the determination of the accessible emission (see 4.3 c) and d)) and Clause 3 of this interpretation sheet; in this process,  $\alpha_{max}$  (t) is determined for the same emission duration t that is used to determine AEL(t) (i.e. the pulse duration or the pulse group duration for 4.3 f) 3) and the averaging duration for 4.3 f) 2), respectively). However, the parameter  $\alpha$  is also used in subclause 4.3 f) 3) in the criteria which  $C_5$  is applied. For these criteria, the parameter  $\alpha$  is not limited in the same way as for the determination of  $C_6$  according to 4.3 d).

For the criterion "Unless  $\alpha > 100 \text{ mrad}$ ", the angular subtense of the apparent source  $\alpha$  is not restricted by  $\alpha_{\text{max}}$ . For non-uniform (oblong, rectangular, or linear) sources, the inequality needs to be satisfied by both angular dimensions of the source in order for  $C_5 = 1$  to apply.

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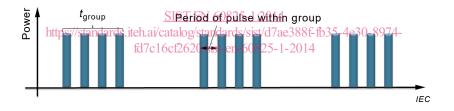
To calculate  $T_2(\alpha)$  and in the criteria " $\alpha \le 5$  mrad", "5 mrad  $< \alpha \le \alpha_{max}$ ", and " $\alpha > \alpha_{max}$ ", the quantity  $\alpha$  is limited to a maximum value of 100 mrad, equivalent to  $\alpha_{max}$  that applies for 0,25 s emission duration and longer. For  $T_2$  and these inequalities,  $\alpha$  is not limited to a value of  $\alpha_{max}$  (*t*) smaller than 100 mrad, and is therefore the same as the value that applies for the determination of  $C_6$  for an emission duration of 0,25 s and longer. As is generally defined (see subclause 4.3 d)) the arithmetic mean is applied to determine  $\alpha$ , i.e. it is not necessary that both dimensions satisfy the criterion "For  $\alpha \le 5$  mrad" independently.

For the determination of the applicable value of  $C_5$  in 4.3. f) 3) in an analysis of moving apparent sources (originating from scanned emission when not accommodating to the pivot point or vertex) the value of  $\alpha$  in the respective inequalities relating to the choice of  $C_5$  in 4.3 f) 3) is determined for the *stationary* apparent source and the respective accommodation condition that is analysed (such as accommodation to infinity).

### 5 Subclause 4.3 f) 3) groups of pulses with group duration longer than $T_i$

For non-uniform repetitive pulse patterns, i.e. groups of pulses (see Figure 2 for an example), when  $\alpha > 5$  mrad and the duration of the group of pulses is longer than  $T_i$ , it is not clearly stated how the thermal additivity expressed by requirement 3) of 4.3 f) is applied. For *uniform* (i.e. constant peak power, duration and period) repetitive pulse trains, it is not necessary to analyse the emission patterns in terms of groupings of pulses.

When individual pulses are close together, they are thermally grouped and thermally represent one "effective" pulse so that  $C_5$  also (additionally to analysing the pulse train based on the actual pulses and the average power) applies to these "effective" pulses, where N is the number of pulse groups within  $T_2$  or within the time base, whichever is shorter.



### Figure 2 – Example of three groups of pulses (each group duration is longer than $T_i$ ) where each group is considered as one "effective" pulse and $C_5$ is applied to the AEL that applies to the group duration, where $C_5$ is determined with the number of pulse groups within the evaluation duration (in the example of the figure N = 3)

For the analysis of pulse groups, the value of  $AEL_{single}$  is determined for the corresponding pulse group duration  $t_{group}$ . For the determination of  $C_5$ , N is the number of pulse groups within  $T_2$  or the time base, whichever is smaller. The respective value of  $C_5$  is applied to  $AEL_{single}$  to obtain  $AEL_{s.p.train}$  that limits the AE of the pulse groups, where AE is the sum of the energy of the pulses contained within the pulse group.

For the application of  $C_5$  to groups of pulses, the AEL( $t_{group}$ ) applicable to the group needs to be determined, as well as the energy per group (AE<sub>group</sub>). For groups of pulses where the peak power of the pulses within the group varies, the group duration is not well defined. In order to simplify the evaluation,  $t_{group}$  can be set equal to the integration duration for which the energy per group (i.e. AE<sub>group</sub>) was determined; it is not necessary to determine the group duration based on the FWHM criterion, which for groups of pulses with varying peak power is not well defined. By setting  $t_{group}$  equal to the integration duration that is used to determine AE<sub>group</sub> (expressed as energy), the application of  $C_5$  to groups of pulses is a simple extension of requirement 2) of 4.3 f) where the average power per group (equal to the energy within the averaging duration  $t_{average}$  divided by the averaging duration) needs to be below the AEL( $t_{average}$ ) determined for the duration over which the power was averaged (AE<sub>group</sub> and AEL( $t_{group}$ ) expressed as power). As is common for the average power requirement, for irregular pulse trains, the averaging duration window (when expressed as energy: the

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integration duration window) has to be varied in temporal position and duration (for instance, if there are pulses with relatively low energy per pulse at the beginning or the end of the group of pulses, integration durations that exclude those low-energy pulses need to be considered also, not only the total group).

If individual pulses have sufficient temporal spacing (period larger than  $T_{crit}$ , see below), as a simplified analysis, they need not be considered for an analysis as a pulse group under 4.3 f) 3). The temporal spacing that is necessary for pulses to only be considered separate (and not analysed additionally as a group) depends on the angular subtense of the apparent source and the duration of the pulses  $t_{pulse}$  within the group. Note that there can be several levels of grouping, so that individual elements (with pulse duration t) within the group could themselves be "effective pulses", i.e. subgroups.

When the

- pulse group  $(t_{aroup})$  durations are between  $T_i$  and 0,25 s, and
- the angular subtense of the apparent source is larger than 5 mrad, and
- the period of the pulses (see Figure 2) is shorter than a critical period  $T_{crit}$  (if  $t_{pulse} < T_i$ , the value of  $t_{pulse}$  is set equal to  $T_i$ ; further, for the determination of  $T_{crit}$ ,  $\alpha_{max}$  is determined for  $t_{pulse}$ , not the group duration) where:

for  $\alpha \le \alpha_{max}$ :  $T_{crit} = 2 \cdot t_{pulse}$  where  $t_{pulse}$  is in seconds

for  $\alpha > \alpha_{max}$ :  $T_{crit} = 0.01 \ \alpha \ t_{pulse}^{0.5}$  where  $t_{pulse}$  is in seconds, and  $\alpha$  is in mrad, not being limited to  $\alpha_{max}$ , **iTeh STANDARD PREVIEW** 

then these pulses constitute a pulse group which is treated as effective pulses and  $C_5$  (where N is the number of groups within the time base of  $T_2$ , which ever is shorter) is applied to the AEL applicable to the pulse group. For the determination of AE,  $\alpha_{max}$  is determined using the duration of the evaluated pulse group  $t_{group}$  of sabove conditions are not fulfilled, then the pulses within the group of pulses that is considered to be analysed as "effective pulse" need not be grouped, i.e. the group of pulses does not need to be analysed as one "effective" pulse.

Note that if multiple pulses occur within  $T_i$ , the rule as stated in 4.3 f) 3) applies in parallel, i.e. they are counted as a single pulse to determine N and the energies of the individual pulses that occur within  $T_i$  are added to be compared to the AEL<sub>s.p.train</sub> of  $T_i$  where the corresponding  $C_5$  for emission durations  $t \le T_i$  is applied.

### 6 Subclause 4.3 f) simplifications

### a) Constant peak power but shorter pulses

Depending on the angular subtense of the apparent source, it can be the case that the value of  $C_5$  is more restrictive for pulses with pulse durations less than  $T_i$  than for pulses with durations longer than  $T_i$  which is against general biophysical principles for cases where the peak power is the same.

### Interpretation

For the case of varying pulse duration within a pulse train, if the accessible emission for pulses longer than  $T_i$  is below the applicable AEL, then it can be assumed for the analysis that pulses with durations less than  $T_i$  but with the same (or lower) peak power as the longer pulses, are less critical. The rationale for this interpretation follows the principle that when pulses have the same peak power, the shorter pulse cannot be more restrictive than the longer one.

NOTE This interpretation can also be used to smooth the step function at  $T_i$  for the classification of products, i.e. the classification of a product may be based on the assumption of pulse durations longer than  $T_i$  even if they are shorter than  $T_i$  provided that the longer pulses satisfy the applicable AEL and the shorter pulses have the same or lower peak power compared to the longer pulses.

### b) Larger image of apparent source

For emission durations exceeding  $T_i$ , due to the step-function of  $C_5$  at 5 mrad and at  $\alpha_{max}$ , the AEL (as a function of  $C_5$  and  $C_6$ ) can be more restrictive for larger values of the angular subtense of the apparent source as compared to smaller ones, which is contrary to general biophysical principles.

### Interpretation

When the class of a laser product is determined with the extended analysis (subclause 5.4.3) and the apparent source is larger than 5 mrad, the classification may be based on a value of the angular subtense of the apparent source less than 5 mrad (resulting in a smaller  $C_6$  but also larger  $C_5$ ). That is, when the AE is below the AEL for an assumed smaller apparent source, the resulting class is applicable even though the image of the apparent source is larger than 5 mrad. This also applies in an equivalent way to the step function of  $C_5$  at  $\alpha_{max}$ .

### c) Using a square aperture stop

In some cases, such as 2D scanned laser beams, the use of a circular aperture stop to determine the accessible emission creates very complex pulse patterns.

### Interpretation

Analysis performed with a square aperture stop with 7 mm side length (for determination of accessible emission and pulse duration) can be assumed to be equivalent to, or more restrictive than, a circular aperture stop and is therefore a valid analysis.

### d) Applicability of simplified default analysis

For pulse durations longer than  $T_i$ , the value of  $C_5$  is smaller (more restrictive) for angular subtense values  $\alpha$  larger than 5 mrad compared to  $\alpha \le 5$  mrad. The assumption of  $\alpha = 1,5$  mrad is the basis of the simplified (default) evaluation. It is therefore not obvious if the simplified (default) analysis still applies in terms of being a restrictive simplifying analysis even for the case that the angular subtense of the apparent source is actually larger than 5 mrad, where  $C_5 \le 1$ 

larger than 5 mrad, where  $C_5 < 1$ . https://standards.teh.ai/catalog/standards/sist/d7ae388f-fb35-4e30-8974-

### Interpretation

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It is acceptable to make use of the simplified restrictive assumption of  $\alpha = 1,5 \text{ mrad}$  ( $C_6 = 1, C_5 = 1$ ) even for the case that the angular subtense of the source is larger than 5 mrad. This means it is not necessary to show that  $\alpha < 5$  mrad in order to apply  $C_6 = 1$  and  $C_5 = 1$  for the simplified (default) analysis, because overall this is a conservative simplification. Note that the simplified default analysis implies that the determination of the accessible emission is not limited by an angle of acceptance equal to  $\alpha_{max}$ .

### e) Determination of the most restrictive position

For the extended analysis, it is necessary to vary the position in the beam. For each position in the beam, the accommodation is varied and the most restrictive image is determined. For determining the most restrictive image (where the ratio AE/AEL is maximum) at a given position, requirement 3) of 4.3 f) is not applied. Otherwise a blurred (larger) image of the apparent source, resulting from variation of the accommodation, could appear more restrictive, which is contrary to general biophysical principles. Once the most restrictive image (and associated  $\alpha$ ) is identified for each position in the beam, all three requirements 4.3 f) are applied to determine the most restrictive position (identifying the position with the maximum ratio of AE/AEL).

### f) Application of total-on-time-pulse method

For regular pulse trains, as well as for varying pulse durations and/or varying period of pulses (but excluding strongly varying peak powers; see below), the total-on-time pulse (TOTP) method (see also IEC 60825-1:2007, subclause 8.3 f) 3b)) may be used as alternative to requirement 3) of 4.3 f), i.e. as alternative to the application of  $C_5$  to the single pulse AEL, provided that  $\alpha_{max}$  is determined for the TOTP (or using the worst case value of 100 mrad). This is more restrictive than the rules of 4.3 f) because it is equivalent to an unlimited  $C_5$  ( $C_5$  not limited to 0,2 or 0,4), and because the value of  $\alpha_{max}$  is typically larger for the TOTP as compared to the value applicable to the single pulse.

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For total-on-time-pulse (TOTP) method the following applies, as reproduced from IEC 60825-1:2007.

The AEL is determined by the duration of the TOTP, which is the sum of all pulse durations within the emission duration or  $T_2$ , whichever is smaller. Pulses with durations less than  $T_i$  are assigned pulse durations of  $T_i$ . If two or more pulses occur within a duration of  $T_i$  these pulse groups are assigned pulse durations of  $T_i$ . For comparison with the AEL for the corresponding duration, all individual pulse energies are added.

Note that the TOTP method in IEC 60825-1:2007 (incl. Corrigendum 1) was specified "For varying pulse widths or varying pulse intervals" and did not refer to varying peak powers. For the case of strongly varying peak powers, the TOTP method is not applicable, as adding pulses to the pulse train with small peak powers and low contributing energy-perpulse values might increase the AEL (by increasing the total-on-time) more than this increases the total energy, and thus would make the emission less critical as compared to an emission based on the pulses with the large peak power only.

### g) Varying peak power but constant pulse duration

For varying peak power but constant pulse durations (both less than or larger than  $T_i$ ), requirement 3) of 4.3 f) can be applied by counting the pulses for the determination of N based on the relative peak power, i.e. N is increased by 1,0 for each pulse with the maximum peak power, and by a value of less than 1,0 for pulses with lower peak power, such as for a pulse with 70 % peak power compared to the maximum peak power in the pulse train, N is increased by 0,7. For this, based on the strong non-linearity of thermally induced injury with temperature, it is justified not to count pulses with peak power (i.e. less than 10 % of the maximum peak power). Note that the resulting AEL sp.train is applied to the pulse with the largest AE, i.e. the largest energy per pulse, and that the interpretation in this paragraph applies only for the case of pulse trains with constant pulse durations.

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### INTERNATIONAL ELECTROTECHNICAL COMMISSION

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### SAFETY OF LASER PRODUCTS -

### Part 1: Equipment classification and requirements

### INTERPRETATION SHEET 2

This interpretation sheet has been prepared by IEC technical committee 76: Optical radiation safety and laser equipment.

The text of this interpretation sheet is based on the following documents:

(standard	S Report on voting	
76/588/FDIS	76/594/RVD	
CICT EN (0025 1 2014		

SIST EN 60825-1:2014

Full information on the voting for the approval of this interpretation sheet can be found in the report on voting indicated in the above table.

### Subclause 4.4 – Conventional lamp replacement

This subclause is clarified by the following:

Subclause 4.4 introduces a criterion based on radiance, which is a quantity not normally determined for laser products. This interpretation sheet clarifies the determination of radiance and the radiance limit.

### Interpretation

The angular subtense  $\alpha$  is determined based on the 50 % of the peak radiance (not averaged over an angle of acceptance larger than 1,5 mrad) of the apparent source, which is an equivalent criterion as given in IEC 62471:2006 and IEC 62471-5:2015. For inhomogeneous or multiple sources, the outer edge (defined by the 50 % level) of the apparent source profile is used to determine  $\alpha$  for the calculation of the radiance limit as well as for the limit regarding the minimum size of the apparent source, even if there are hotspots within the apparent source  $\alpha$  is determined at a distance of 200 mm from the closest point of human access.