# SLOVENSKI STANDARD SIST EN 13445-3:2002/A17:2008 <br> 01-januar-2008 

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Unfired pressure vessels - Part 3: Design

Unbefeuerte Druckbehälter - Teil 3: Konstruktion

Récipients sous pression non soumis a la flamme - Partie 3 : Conception
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Pressure vessels, gas cylinders

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# EUROPEAN STANDARD NORME EUROPÉENNE EUROPÄISCHE NORM 

EN 13445-3:2002/A17

ICS 23.020.30

## English Version

## Unfired pressure vessels - Part 3: Design

Récipients sous pression non soumis à la flamme - Partie 3
Unbefeuerte Druckbehälter - Teil 3: Konstruktion

This amendment A17 modifies the European Standard EN 13445-3:2002; it was approved by CEN on 26 May 2007.
CEN members are bound to comply with the CEN/CENELEC Internal Regulations which stipulate the conditions for inclusion of this amendment into the relevant national standard without any alteration. Up-to-date lists and bibliographical references concerning such national standards may be obtained on application to the CEN Management Centre or to any CEN member.

This amendment exists in three official versions (English, French, German). A version in any other language made by translation under the responsibility of a CEN member into its own language and notified to the CEN Management Centre has the same status as the official versions.

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EUROPEAN COMMITTEE FOR STANDARDIZATION COMITÉ EUROPÉEN DE NORMALISATION EUROPÄISCHES KOMITEE FÜR NORMUNG

Management Centre: rue de Stassart, 36 B-1050 Brussels
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## Foreword

This document (EN 13445-3:2002/A17:2007) has been prepared by Technical Committee CEN/TC 54 "Unfired pressure vessels", the secretariat of which is held by BSI.

This Amendment to the European Standard EN 13445-3:2002 shall be given the status of a national standard, either by publication of an identical text or by endorsement, at the latest by April 2008, and conflicting national standards shall be withdrawn at the latest by April 2008.

The document includes the text of the amendment itself. The corrected pages of EN 13445-3 will be delivered as issue 29 of the standard.

According to the CEN/CENELEC Internal Regulations, the national standards organizations of the following countries are bound to implement this European Standard: Austria, Belgium, Bulgaria, Cyprus, Czech Republic, Denmark, Estonia, Finland, France, Germany, Greece, Hungary, Iceland, Ireland, Italy, Latvia, Lithuania, Luxembourg, Malta, Netherlands, Norway, Poland, Portugal, Romania, Slovakia, Slovenia, Spain, Sweden, Switzerland and United Kingdom.

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## Annex J

(normative)

## Alternative method for the design of heat exchanger tube sheets

## J. 3 Specific symbols and abbreviations

Change the following symbols in Annex J.3.3:

## J.3.3 Symbols

Add the following symbols:
$A_{\mathrm{R}(\min )} \quad$ is the minimum area of the tubed region, $\left[\mathrm{mm}^{2}\right]$, see J.5.1.1.3.2;
$d_{1(a v)} \quad$ is the average of $d_{1(\min )}$ and $d_{1(\max )}$, [mm], see J.5.1.1.4;
$d_{1(\max )} \quad$ is the maximum value of $d_{1},[\mathrm{~mm}]$, see J.5.1.1.2;
$d_{1(\min )} \quad$ is the minimum value of $d_{1},[\mathrm{~mm}]$, see 5.5 .1 .1 .3 ; PREVIEW
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$j \quad$ is an integer to identify any trapezoidal area (tubed or untubed);
$k$ is an integer tolidentify an untubed (pass partition) zone; ca4-65e0-410d-ae6b-
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$N_{I(k)} \quad$ is the number of potential extra tubes in a given untubed trapezoidal area, [1], see J.5.1.1.3.2;
$N_{I(r)} \quad$ is the number of potential extra tubes in a given row, [1], see J.5.1.1.3.2;
$p_{b} \quad$ is the tube pitch in relation to the height of the trapezoidal area, [mm];
$p_{c} \quad$ is the tube pitch in relation to the width of the trapezoidal area, $[\mathrm{mm}]$;
$r \quad$ is an integer to identify a tube row;
$\Delta d_{(a c t)} \quad$ is the actual difference between $d_{1(\max )}$ and $d_{1(\min )},[\mathrm{mm}] ;$
$\Delta d_{(\text {all })} \quad$ is the allowable difference between $d_{1(\max )}$ and $d_{1(\min )},[\mathrm{mm}] ;$

Replace the following symbols:
$N_{I(\min )} \quad$ is the total minimum number of potential extra tubes for the whole tubed area, [1], see J.5.1.1.3.2;
$r_{o} \quad$ is the radius of the outermost tube hole centre [mm]; see Figure $\mathrm{J}-7(\mathrm{a})$ and NOTE in J.5.1.1.2 (also Figure 13.7-1);

## Delete the following symbol:

$\theta \quad$ is a factor dependant on the tube pitch [1]; see J.5.1.

## J. 5 Parameters for all types

## J.5.1 Diameters and widths

Replace 5.1.1 with the following text:

## J.5.1.1 Outside diameter $d_{1}$ of tubed region

## J.5.1.1.1 General

The procedure for calculating $l_{1}$ is given beiow. ARID PREVIIEW
NOTE Upper and lower limits for $d_{1}$ can be established by considering the space within the tubed area which is available for additional tubes. $d_{1}$ is calculated from the limits.

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J.5.1.1.2 Maximum diameter $d_{\text {h(max) }}$ 62/sist-en-13445-3-2002-a17-2008

Determine $d_{1(\max )}$ as follows:

$$
\begin{equation*}
d_{1(\max )}=2 r_{o}+d_{T} \tag{J.5.1-1}
\end{equation*}
$$

NOTE If an isolated tube or small group of tubes lies outside the main tubed region (by a distance of more than one pitch) it should be ignored when determining $r_{o}$ and $d_{\mathrm{T}}$.

## J.5.1.1.3 Minimum diameter $d_{1(\mathrm{~min})}$

## J.5.1.1.3.1 Defining trapezoidal areas

Draw the tangent lines to the outside tubes to enclose the tubed region within a polygon. The positions of the tie rods shall be ignored.

NOTE 1 An example is shown in Figures $\mathrm{J}-7$ (c) and $\mathrm{J}-7$ (d).
NOTE 2 For simplicity, where two tangent lines have nearly equal slopes, they can be replaced by a single tangent line if this line lies outside the centres of any tubes it crosses (i.e. it cuts less than half tube sections). (See area of height $b_{7}$ in Figure J-7(b).)

Divide the tubed region into (perforated or un-perforated) trapezoidal areas by drawing straight lines parallel to the tube rows.

Where the intersection of the tangent lines which form the polygon lies closer to the tube centreline, the construction line shall be through the tube centres (see Figure J-7(d)). Where the intersection of the tangent lines which form the polygon lies closer to the tangent line than to the tube centreline, the construction line shall be the tangent to the tube row (see Figure J-7(b)). This also applies when the intersection is mid-way between the tube centre line and the tube tangent line. Extend the construction lines to the enclosing polygon to form trapezoidal areas. Denote the heights of the trapezoidal areas by $b_{j}(j=1,2, \ldots$,$) and widths by$ $c_{j}(j=0,1,2, .$,$) .$

## J.5.1.1.3.2 Determination of $A_{R(\text { min })}$

Determine $A_{R(\min )}$ by one of the following three methods.
(a) Tube counting

Determine the total number of potential extra tubes $N_{I(\min )}$ as follows.
Calculate the tube pitches $p_{b}$ and $p_{c}$ as follows:
On triangular pitch:

$$
\begin{equation*}
p_{b}=0,866 p \tag{J.5.1-2}
\end{equation*}
$$

and
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$$
\begin{equation*}
p_{c}=p \tag{J.5.1-3}
\end{equation*}
$$

On square pitch:
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$$
\begin{equation*}
p_{b}=p \tag{J.5.1-4}
\end{equation*}
$$

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and

$$
\begin{equation*}
p_{c}=p \tag{J.5.1-5}
\end{equation*}
$$

For each tube row, count all unfilled positions within the row. For unfilled positions at the ends of the row, multiples of half a tube may be added when the tangent line lies inside the centre of the potential extra tube. This gives $N_{I(r)}$ for each row.

NOTE An example of this is shown in Figure J-7(e).
For a pass partition zone where the distance between the adjacent tube rows equals an integral number of tube pitches, count all the potential extra tube positions to obtain $N_{I(k)}$ for that zone.

NOTE Area of height $b_{3}$ in Figure $J-7(\mathrm{~d})$ is one where the distance between the adjacent tube rows equals an integral number of tube pitches.

For a pass partition zone or other untubed area, with arbitrary distances to the adjacent tube rows, calculate $N_{I(k)}$ for that zone as follows:

$$
\begin{equation*}
N_{I(k)}=\frac{\left[b_{k, p}+p_{b}\right]\left(c_{k-1, p}+c_{k, p}\right)}{2 p_{b} \cdot p_{c}} \tag{J.5.1-6}
\end{equation*}
$$

In Equation J.5.1-6, $b_{k}, p$ is the distance between the centrelines of adjacent tube rows and $p_{b}$ is the corresponding (vertical) pitch; $c_{k-1}, p$ and $c_{k}, p$ are the (upper and lower) widths of the trapezoidal area respectively; and $p_{c}$ is the corresponding (horizontal) pitch, see Figure J-7(d). The calculated number $N_{I(k)}$ for each partition zone of this type shall be rounded up to the nearest half tube.

NOTE The area of height $b_{5}, p$ in Figure $\mathrm{J}-7(\mathrm{~b})$ is an untubed area with an arbitrary distance between the adjacent tube rows.
$N_{I(\min )}$ is the sum of all the potential extra tubes from the rows, $N_{I(r)}$, and all the potential extra tubes from the pass partition zones, $N_{I(k)}$. In extreme cases (where the layout is fully packed) $N_{I(\min )}$ may equal zero.

Calculate area $A_{R(\min )}$ as follows:

$$
\begin{equation*}
A_{R(\min )}=\left(N_{T}+N_{I(\min )}\right) \cdot p_{b} \cdot p_{c} \tag{J.5.1-7}
\end{equation*}
$$

(b) Calculation of all the trapezoidal areas
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Calculate the values of $b_{J}$ and $c_{J}$ for each of the trapezoidal areas (see FigureJ-7(d)) as follows:

- in the perforated zones, the heights $b_{44}$ are to be calculated as the nearest multiple of $p_{b}$ and $\frac{d_{T}}{2}$. https://standards.iteh.ai/catalog/standards/sist/4a237ca4-65e0-410d-ae6bThe widths $c_{J}$ are similarly to be calculated as the nearest multiple of $p_{c}$ and $\frac{d_{T}}{2}$. In case of doubt, always assume the smaller value.
- for any pass partition zones, the height of the zone, whether or not it is an exact multiple of $p_{b}$, is inserted in Equation J.5.1-8.

Calculate $A_{R(\min )}$ to include all perforated and un-perforated areas as follows:

$$
\begin{equation*}
A_{R(\min )}=0,5 \cdot\left\{\left(c_{0}+c_{1}\right) \cdot b_{1}+\left(c_{1}+c_{2}\right) \cdot b_{2}+\left(c_{2}+c_{3}\right) \cdot b_{3} \ldots . .\right\}=\sum_{j=1}^{j=j_{\max }} 0,5 \cdot\left(c_{j-1}+c_{j}\right) \cdot b_{j} \tag{J.5.1-8}
\end{equation*}
$$

(c) Measurement of area

Measure area $A_{R(\min )}$

NOTE This could be done by computer or other device.

## J.5.1.1.3.3 Calculation of $d_{1(\min )}$

Calculate $d_{1(\min )}$ from $A_{R(\min )}$ as follows:

$$
\begin{equation*}
d_{1(\min )}=\sqrt{\frac{4 A_{R(\min )}}{\pi}} \tag{J.5.1-9}
\end{equation*}
$$

