



Designation: E 319 – 85 (Reapproved 2003)

Standard Practice for the Evaluation of Single-Pan Mechanical Balances¹

This standard is issued under the fixed designation E 319; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ϵ) indicates an editorial change since the last revision or reapproval.

INTRODUCTION

The balance performs two basic functions: (1) it compares an unknown load with one or more weights, and (2) it indicates the difference between the two loads for differences smaller than the smallest weights normally used on the balance. The test procedure given herein measures the precision with which the balance can compare the two loads, and the rates at which systematic errors may affect the observed difference.

1. Scope

1.1 This practice covers testing procedures for evaluating the performance of single-arm balances required by ASTM standards.

1.2 This practice is intended for but not limited to sensitivity ratios of 10^6 or better and on-scale ranges of $1000xd$ or more where d = readability either directly or by estimation.

1.3 This practice can also be applied to other single-pan balances with mechanical weight changing of different capacities or sensitivities with appropriate test loads and calibration weights.

NOTE 1—Mechanical balances of this type have largely been replaced by automatic electronic balances incorporating a variety of operational principles. Nevertheless, some single-pan mechanical balances are still manufactured and many older balances will remain in service for years to come. One type of automatic electronic balance, the so-called “hybrid,” bears considerable similarity to single-pan mechanical balances of the null type. (1)²

1.4 *This standard does not purport to address all of the safety problems, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

2. Terminology

2.1 Definitions (1):

¹ This practice is under the jurisdiction of ASTM Committee E41 on Laboratory Apparatus and is the direct responsibility of Subcommittee E41.06 on Weighing Devices.

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² The boldface numbers in parentheses refer to the list of references at the end of this practice.

2.1.1 *accuracy*—the degree of agreement of the measurements with the true value of the magnitude of the quantity measured (2).

2.1.2 *correction for a weight*—the correction for the error in adjustment is:

$$Cr.W = A - N \quad (1)$$

where:

$Cr.W$ = correction for the error in adjustment to nominal value,

A = actual value of the weight, and

N = nominal value.

NOTE 2—In practice it is not possible to adjust weights exactly to their nominal values.

2.1.3 *correction for error in scale indication*—the correction for the scale indication, I , is:

$$Cr.I = A - I \quad (2)$$

NOTE 3—The correction for the scale is taken with reference to the measured value of a weight used as a test load during calibration of the on-scale range.

2.1.4 *index of precision*—the standard deviation, computed in any acceptable manner, for a collection of measurements involving a given pair of mass standards (3).

NOTE 4—The standard deviation is computed from the data provided by the instrument precision test (see Section 7) index of precision.

2.1.5 *null-type balance*—a balance which requires, as the final step in its operation, that the observer restore the angle of the balance beam to its original (or null) position. The least significant figures of the balance indication are obtained from this operation.

2.1.6 *optical-type balance*—in this type the least significant figures of the balance indication are related to the deflection angle of the beam from its original (or null) position. A scale placed on the moving beam is optically projected onto the (stationary) balance case to provide this indication.

2.1.7 *precision*—the repeatability of the balance indication with the same load under essentially the same conditions.

NOTE 5—The more closely the measurements are grouped, the smaller the index of precision will be. The precision must be measured under environmental conditions that represent the conditions under which the balance is normally used.

2.1.8 *readability*—the value of the smallest decimal subdivision of a scale division in terms of mass units, that can be read, when the balance is read in the intended manner.

NOTE 6—The readability of a particular instrument is not a measure of its performance as a weighing device. The relationship between the numerical value obtained by reading devices and the ability of the operator to estimate the location of the reference device or index is important. It is possible to introduce a large number of readable subdivisions of the main scale divisions that would increase the “readability” as defined but if the reading device cannot be reset to the same numerical value when the beam is in an immovable condition, or when the load on the beam is a constant value, the readability becomes meaningless. Readability substantially less than 1 standard deviation as determined by repeated measurement with a given test weight is usually superfluous.

2.1.9 *scale division*—the smallest graduated interval subdivided either by estimation or with the aid of a vernier. Subdivisions which appear as divisions on the vernier are not considered to be scale divisions, but rather parts of scale divisions.

2.1.10 *sensitivity weight*—a small weight used to measure the “on-scale” deflection of the balance indicator.

NOTE 7—With single-pan balances the sensitivity weight should be equal to the value of the smallest built-in weight represented by the first step on the dial for the smallest weights.

2.1.11 *test load*—a load chosen to represent the sample load in the test procedure.

2.1.12 *value of the division*—the change in load required to change the balance indication by one scale division. The reciprocal of the sensitivity is its most useful function.

3. Summary of Practice

3.1 The accuracy of the direct-reading scale, the smallest weight of the set of built-in weights, and uniformity of sensitivity between the upper and lower halves of full-scale deflections are verified by preliminary tests.

3.2 Estimates of rate of change of the zero with time, rate of change in the value of the scale division with time, and a quantitative measure of the variability or random error are provided by short tests for precision and bias.

3.3 An overall test of the direct-reading capability is provided by tests of the built-in weights.

4. Significance and Use

4.1 *Monitoring Weighing Performance*—This practice provides results in the form of control charts which measure the weighing capability at the time of the test. A series of tests at appropriate intervals will monitor balance performance over a

period of time. A marked change from expected performance may result from a variety of causes including: maladjustment, damage, dirt, foreign material, and thermal disturbances. If the test results are to indicate future performance, any disturbances that occur exterior to the balance must be brought under control (2).

4.2 *Acceptance Tests*—This practice may also be used as acceptance tests for new balances. For this purpose, the tests should be conducted under favorable, but not necessarily ideal, conditions. Since systematic error in the course of the zero and the course of the sensitivity may be caused by disturbances external to the balance, limits on these errors are not ordinarily prescribed in acceptance requirements.

5. Preparation of Apparatus

5.1 *Balance* (In all cases, the balance should be used in accordance with the manufacturer’s instructions):

5.1.1 The results obtained will depend on the environment. Select an area which is free of excessive vibration and air currents, where rapid changes in temperature and relative humidity will not be encountered, and where the floor is rigid enough to be free of a tilting effect on the balance indication. Place the balance on a sturdy bench. If the balance has been moved to a new location, permit it to come to thermal equilibrium for at least 1 h before performing the test, preferably several hours.

5.1.2 Inspect and test the balance to make sure that it is in proper mechanical order. Arrest and release the beam to make sure that readings are approximately repetitive. Observe the indication during arrest and release to ensure that there is no “kick” that would indicate that arrestment points might be out of adjustment. If necessary, have the balance adjusted by a competent balance technician.

5.1.3 Make a few trial measurements of the interval from zero to the full-scale indication.

5.2 *Reading the Balance*—The balance should be read in accordance with the instructions supplied by the manufacturer. Optical types should include the reading of verniers or micrometres. Null types should include the indication of the device for restoring to null including verniers or micrometres.

6. Preliminary Testing of Single-Arm Balances

6.1 *Summary of Method*—With single-pan balances the smallest built-in weight, indicated by the first step on the dial, is compared with a calibrated weight. The direct-reading scale is tested for agreement with the smallest built-in weight and the sensitivity is adjusted, if necessary, so that the indications of the scale are precise in terms of the calibrated weight. A “fifty-fifty” test verifies the accuracy of the midpoint at half-full scale. This test should be performed before proceeding to other tests. After the accuracy of adjustment of the smallest built-in weight is verified, this weight is used to test full-scale deflections. Tests are also made for the uniformity of deflection over the lower and upper halves of the full-scale deflection. The preliminary tests show either that the balance is operating properly, or that discrepancies indicate the presence of sources of error. Uncertainties of perhaps one millionth of the balance capacity may be caused by dirt or foreign material

in the bearings, or by unskilled handling, while larger discrepancies may be caused by worn or damaged knife-edges or other sources such as electrostatic effects. Any necessary cleaning or servicing should be done at this point. If discrepancies continue, other possible sources of uncertainty should be studied. There is no point in proceeding with routine test procedures until acceptable results can be obtained with the preliminary tests.

NOTE 8—With null-type balances (including the hybrid) it is possible to use the flexure of a segment of metal, quartz, etc. as the main pivots instead of knife edges. A flexure pivot is by its nature free of problems of dirt. Flexures are also generally more robust than knives. The chief problem associated with flexures is that they act like springs and thus add a restoring force which may vary with time or temperature. This drawback can be minimized by careful design and all but eliminated by the use of servo-control in electronic balances.

6.2 Materials:

6.2.1 A watch or clock which indicates seconds,

6.2.2 Pencils for recording data,

6.2.3 Columnar data sheets (If balance performance will be monitored periodically, it may be useful to enter data directly into a personal computer which has been programmed for this task.),

6.2.4 A calibrated weight designated $S1$ which has the nominal value equal to the smallest interval on the dial-operated weights, and

6.2.5 Two weights of half of the nominal value of $S1$ designated $(\frac{1}{2})_1$ and $(\frac{1}{2})_2$. (These weights need not be calibrated but they should bear distinguishing marks, preferably one, and two dots.)

6.3 Procedure—Adjust the “no-load” readings to a point near the center of the vernier so that zero drift or other deviation will not cause a negative scale reading. Perform the preliminary tests, loading the pan and changing the dial settings according to the schedule in **Table 1**. Before releasing the beam, record the load on the pan and the dial setting so that the observation will be confined to the scale reading. Release the balance and observe the scale reading. Record the indication and verify the stability of the scale reading, then arrest the balance promptly.

6.4 Calculations for Preliminary Tests:

6.4.1 Compute $D1$, the value of the smallest built-in weight as follows:

$$D1 = [(a - b + f - e)/2] + S1 \quad (3)$$

where: a , b , f , and e are taken from **Table 1**, and $S1$ = calibrated value of test weight.

6.4.2 Compute $S1$ in scale divisions to verify the full-scale value on the direct-reading scale as follows:

$$S1 = (c - b + d - e)/2 \quad (4)$$

where c , b , d , and e are taken from **Table 1**. Adjust the balance sensitivity if necessary so that the full-scale reading equals $D1$.

6.4.3 Compute average scale difference, A , for lower 50 % of direct-reading scale as follows:

$$A = (g - f + j - k)/2 \quad (5)$$

6.4.4 Compute average scale difference, B , for upper 50 % of direct-reading scale as follows:

$$B = (h - g + i - j)/2 \quad (6)$$

A and B should agree within 3 standard deviations (see **7.5.3**). Any discrepancy smaller than 3 standard deviations may be ascribed to uncertainty in the preliminary measurements and does not necessarily indicate a real change in the value of the scale divisions.

6.4.5 Inspect the no-load readings, a , f , and k for agreement or zero drift.

6.4.6 See **Table 2** and **Fig. 1** for examples of calculations and observation form.

7. Instrument Precision (4)

7.1 Summary of Method:

7.1.1 A set of four readings is repeated four times, or more, to obtain pairs of readings with identical loads:

7.1.1.1 A reading near zero,

7.1.1.2 A reading near the upper end of the scale,

7.1.1.3 A reading near the upper end of the scale with a test load plus a small weight, and

7.1.1.4 A reading near zero with the test load but with the small weight removed.

7.1.2 Readings are taken at a steady pace as rapidly as practicable, consistent with good practice, and the time is observed at the start of each set of observations and at the end of the test.

TABLE 1 Schedule for Preliminary Tests of Single-Arm Balances

Observation	Time	Pan Load	Dial Setting	Scale Reading
a	Record the time	zero	0	...
b		$S1^A$	1	...
c		$S1^A$	0	...
d	Wait 30 s	$S1^A$	0	...
e		$S1^A$	1	...
f	Record the time	0	0	...
g		$(\frac{1}{2})_1^B$	0	...
h	Add $(\frac{1}{2})_2^B$	$(\frac{1}{2})_1 + (\frac{1}{2})_2^B$	0	...
i	Wait 30 s	$(\frac{1}{2})_1 + (\frac{1}{2})_2^B$	0	...
j	Remove $(\frac{1}{2})_1^B$	$(\frac{1}{2})_2^B$	0	...
k	Record the time	0	0	...

^A $S1$ = calibrated weight of nominal value equal to the smallest dial-operated weight.

^B $(\frac{1}{2})_1$ and $(\frac{1}{2})_2$ = weights of nominal value equal to $\frac{1}{2} S1$ (not necessarily calibrated but marked for identification).

TABLE 2 Example of Preliminary Test of Direct Reading Balance

Observation	Time	Load	Dial	Scale Reading
a	1:30 p.m.	0	0	6.4
b		S1	1	6.45
c		S1	0	1006.5
d	1:34 ½	S1	0	1006.5
e		S1	1	6.5
f		0	0	6.4
g	1:39	(500 mg) ₁	0	506.5
h		(500 mg) ₁ + (500 mg) ₂		1006.25
i		(500 mg) ₁ + (500 mg) ₂	0	1006.3
j		(500 mg) ₂	0	506.15
k		0	0	6.4

Calculations:

$$D1 = [(a - b + f - e)/2] + S1 = [(6.4 - 6.45 + 6.4 - 6.5)/2] + 1000 = 999.925$$

$$S1 (= 1000.006 \text{ mg}) = [(c - b + d - e)/2] = [(1006.5 - 6.45 + 1006.5 - 6.5)/2] = 1000.025 \text{ scale divisions}$$

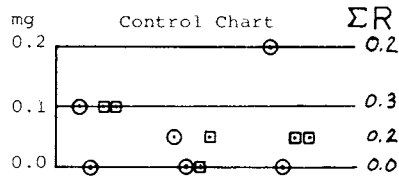
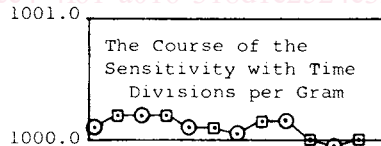
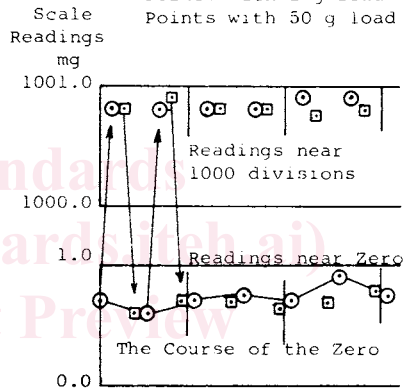
$$A = (g - f + j - k) = (506.5 - 6.4 + 506.15 - 6.4)/2 = 499.925$$

$$B = (h - g + i - j) = (1006.25 - 506.5 + 1006.3 - 506.15)/2 = 499.95$$

Date: May 5, Observer: John Doe Balance: No. 177811

- Instructions**
1. Load the pan with a small weight equal to the first interval on the dial (1 g for this test) and leave it on the pan throughout the test.
 2. Set the dial to 1 g.
 3. Set the zero reading to some small positive number.
 4. Record the zero reading.
 5. Change dial from 1 to 0, and record reading near full scale.
 6. Add 50 g load, change dial to 50, and record reading near full scale.
 7. Change dial from 50 to 51 and record reading near zero.
 8. Record time at end of each group of four readings.
 9. Continue with groups of 4 readings as illustrated.
 10. Subtract the readings near zero from the readings near full scale to obtain points for the Course of the Sensitivity.
 11. Separate the readings into groups of two pairs as illustrated.
 12. Record differences within the duplicate pairs near zero and near 1 g as points on the Control Chart.
 13. Compute the average difference within duplicate pairs and divide by 0.798 to get an estimate of the standard deviation of a single substitution weighing.

Legend:
 Points with 1 g load = ○
 Points with 50 g load = □



$$\Sigma R = 0.7 \text{ mg}$$

Estimate of the Standard Deviation of a Single Substitution Weighing

$$S.D. = \frac{0.7 \text{ mg}}{12} \times \frac{1}{0.798} = 0.073 \text{ mg}$$

FIG. 1 Calculations and Observation Form for Test of Precision

7.1.3 The balance indications are plotted on a graph to provide a visual presentation of errors. The zero readings are connected to show the course of the zero with time. The response of the balance to the small weight is plotted. The

course of the sensitivity with time is represented by a plot of the interval from zero to full-scale angular motion of the beam,