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Crane safety - General design - Part 2: Load actions

Kransicherheit - Konstruktion allgemein - Teil 2: Lasteinwirkungen

Sécurité des appareils de levage à charge suspendue - Conception générale - Partie 2: Effets de charge

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Cranes

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Crane safety - General design - Part 2: Load actions

Sécurité des appareils de levage à charge suspendue -Conception générale - Partie 2: Charges Kransicherheit - Konstruktion allgemein - Teil 2: Lasteinwirkungen

This European Standard was approved by CEN on 14 June 2014.

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EUROPEAN COMMITTEE FOR STANDARDIZATION COMITÉ EUROPÉEN DE NORMALISATION EUROPÄISCHES KOMITEE FÜR NORMUNG

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Foreword

This document (EN 13001-2:2014) has been prepared by Technical Committee CEN/TC 147 "Crane — Safety", the secretariat of which is held by BSI.

This European Standard shall be given the status of a national standard, either by publication of an identical text or by endorsement, at the latest by February 2015 and conflicting national standards shall be withdrawn at the latest by February 2015.

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. CEN [and/or CENELEC] shall not be held responsible for identifying any or all such patent rights.

This document supersedes EN 13001-2:2011.

The major changes in this revision are in 4.2.2.2, 4.2.3.4, 4.2.4.10, 4.3.2, 4.3.4 and 4.3.7. There are new issues in 4.2.4.7, 4.2.4.8, Annex B, Annex C and Annex D.

This document has been prepared under a mandate given to CEN by the European Commission and the European Free Trade Association, and supports essential requirements of EU Directive(s).

For relationship with EU Directive(s), see informative Annex ZA, which is an integral part of this document.

This European Standard is one Part of EN 13001. The other parts are as follows:

- Part 1: General principles and requirements rds.iteh.ai)
- Part 2: Load actions
- SIST EN 13001-2:2014

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- Part 3-1: Limit states and proof of competence of steer structures -4dd9-9b4a-
- Part 3-2: Limit states and proof of competence of wire ropes in reeving systems
- Part 3-3: Limit states and proof of competence of wheel/rail contacts
- Part 3-4: Limit states and proof of competence of machinery
- Part 3-5: Limit states and proof of competence of forged hooks

For the relationship with other European Standards for cranes, see Annex E.

According to the CEN-CENELEC Internal Regulations, the national standards organizations of the following countries are bound to implement this European Standard: Austria, Belgium, Bulgaria, Croatia, Cyprus, Czech Republic, Denmark, Estonia, Finland, Former Yugoslav Republic of Macedonia, France, Germany, Greece, Hungary, Iceland, Ireland, Italy, Latvia, Lithuania, Luxembourg, Malta, Netherlands, Norway, Poland, Portugal, Romania, Slovakia, Slovenia, Spain, Sweden, Switzerland, Turkey and the United Kingdom.

Introduction

This European Standard has been prepared to be a harmonized standard to provide one means for the mechanical design and theoretical verification of cranes to conform to the essential health and safety requirements of the Machinery Directive, as amended. This standard also establishes interfaces between the user (purchaser) of the crane and the designer, as well as between the designer and the component manufacturer, in order to form a basis for selecting cranes and components.

This European Standard is a type C standard as stated in the EN ISO 12100.

The machinery concerned and the extent to which hazards are covered are indicated in the scope of this standard.

When provisions of this type C standard are different from those, which are stated in type A or B standards, the provisions of this type C standard take precedence over the provisions of the other standards, for machines that have been designed and built according to the provisions of this type C standard.

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1 Scope

This European Standard specifies load actions to be used together with the standard EN 13001-1 and EN 13001-3, and as such they specify conditions and requirements on design to prevent mechanical hazards of cranes, and provides a method of verification of those requirements.

NOTE Specific requirements for particular types of crane are given in the appropriate European Standard for the particular crane type.

The following is a list of significant hazardous situations and hazardous events that could result in risks to persons during normal use and foreseeable misuse. Clause 4 of this standard is necessary to reduce or eliminate the risks associated with the following hazards:

- a) Instability of the crane or its parts (tilting).
- b) Exceeding the limits of strength (yield, ultimate, fatigue).
- c) Elastic instability of the crane or its parts (buckling, bulging).
- d) Exceeding temperature limits of material or components.
- e) Exceeding the deformation limits.

This document is not applicable to cranes that are manufactured before the date of its publication as EN.

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2 Normative references

<u>SIST EN 13001-2:2014</u>

The following documents in whole or in partia are normatively referenced in this document and are indispensable for its application. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

EN 1990, Eurocode - Basis of structural design

EN 13001-1, Cranes — General Design — Part 1: General principles and requirements

ISO 4306-1:2007, Cranes — Vocabulary — Part 1: General

3 Terms, definitions, symbols and abbreviations

3.1 Terms and definitions

For the purposes of this document, the terms and definitions given in EN 1990, Clause 6 of ISO 4306-1:2007 and the following apply.

3.1.1

hoist load

sum of the masses lifted by the crane, taken as the maximum that the crane is designed to lift in the configuration and operational conditions being considered

3.1.2

single failure proof system

force carrying arrangement of several components, arranged so that in case of a failure of any single component in the arrangement, the capability to carry the force is not lost

3.2 Symbols and abbreviations

For the purposes of this document, the symbols and abbreviations given in Table 1 apply.

Symbols, abbreviations	Description					
A1 to A4	Load combinations including regular loads					
Α	Characteristic area of a crane member					
Ag	Projection of the hoist load on a plane normal to the direction of the wind velocity					
A _c	Area enclosed by the boundary of a lattice work member in the plane of its characteristic height d					
A _j	Area of an individual crane member projected to the plane of the characteristic height d					
b _h	Width of the rail head					
b	Characteristic width of a crane member					
B1 to B5	Load combinations including regular and occasional loads					
С	Spring constant					
C _o , C _a , C _{oy} , C _{oz}	Aerodynamic coefficients					
C1 to C11	Load combinations including regular, occasional and exceptional loads					
CFF, CFM	Coupled wheel pairs of system F/F or F/M					
d	Characteristic dimension of a crane member 2b-9c6c-4dd9-9b4a-					
d _i , d _n	Distance between wheel pair <i>i</i> or <i>n</i> and the guide means					
e _G	Width of the gap of a rail					
f	Friction coefficient					
f_{i}	Loads					
f_{q}	natural frequency					
$f_{\rm rec}$	Term used in calculating $v(z)$					
F	Force in general					
F, F_y, F_z	Wind loads					
Ê	Maximum buffer force					
F_{i}, F_{f}	Initial and final drive force					
ΔF	Change of drive force					
$F_{x1i}, F_{x2i}, F_{y1i}, F_{y2i}$	Tangential wheel forces					
F _y	Guide force					
F _{z1i} , F _{z2i}	Vertical wheel forces					

Table 1 — Symbols and abbreviations

Symbols, abbreviations	Description					
F/F, F/M	Abbreviations for Fixed/Fixed and Fixed/Moveable, characterizing the possibility of lateral movements of the crane wheels					
g	Acceleration due to gravity					
h	Distance between instantaneous slide pole and guide means of a skewing crane					
h(t)	Time dependent unevenness function					
h _s	Height of the step of a rail					
H ₁ , H ₂	Lateral wheel forces induced by drive forces acting on a crane or trolley with asymmetrical mass distribution					
HC1 to HC4	Stiffness classes					
HD1 to HD5	Classes of the type of hoist drive and its operation method					
i	Serial number					
IFF, IFM	Independent wheel pairs of system F/F or F/M					
j	Serial number					
k	Serial number					
K	Drag coefficient of terrain					
K ₁ , K ₂	Roughness factors					
l	Span of a crane dards.iteh.ai)					
la	Aerodynamic length of a crane member					
l _o https://	standards iteh ai/catalog/standards/sist/ac4f422b-9c6c-4dd9-9b4a- Geometric length of a crane member 9cact2d07eea/sist-en-13001-2-2014					
m _H	Mass of the hoist load					
т	Mass of the crane and the hoist load					
$\Delta m_{_{_{\rm H}}}$	Released or dropped part of the hoist load					
п	Number of wheels at each side of the crane runway					
n _m	Exponent used in calculating the shielding factor η					
р	Number of pairs of coupled wheels					
q	Equivalent static wind pressure					
\overline{q}	Mean wind pressure					
<i>q</i> (z)	Equivalent static storm wind pressure					
<i>q</i> (3)	Wind pressure at v(3)					
r	Wheel radius					
R	Out-of-service wind recurrence interval					
Re	Reynold number					
S g	Slack of the guide					
s _y	Lateral slip at the guide means					

Symbols, abbreviations	Description					
S _{yi}	Lateral slip at wheel pair <i>i</i>					
S	Load effect					
Ŝ	Maximum load effect					
S _i , S _f	Initial and final load effects					
ΔS	Change of load effect					
t	Time					
и	Buffer stroke					
û	Maximum buffer stroke					
v	Travelling speed of the crane					
\overline{v}	Constant mean wind velocity					
v *	Constant mean wind velocity if the wind direction is not normal to the longitudinal axis of the crane member under consideration					
<i>v</i> (z)	Equivalent static storm wind velocity					
v(z)*	Equivalent static storm wind velocity if the wind direction is not normal to the longitudinal axis of the crane member under consideration					
v(3)	Gust wind velocity averaged of a period of 3 seconds					
vg	Three seconds gust amplitude					
v _h	Hoisting speed SIST EN 13001-2:2014 https://standards.iteb.ai/catalog/standards/sist/ac4f122b_9c6c_4dd9_9b4a					
v _{h,max}	Maximum steady/hoisting speeden-13001-2-2014					
^𝒱 h,CS	Steady hoisting creep speed					
$v_{\rm m}(z)$	Ten minutes mean storm wind velocity in the height z					
v_{ref}	Reference storm wind velocity					
w _b	Distance between the guide means					
Z	Height above ground level					
<i>z</i> (<i>t</i>)	Time-dependent coordinate of the mass centre					
α _r	Relative aerodynamic length					
$a_{_{_{\mathbf{W}}}}$	Angle between the direction of the wind velocity \overline{v} or $v(z)$ and the longitudinal axis of the crane member under consideration					
α	Skewing angle					
α _g	Part of the skewing angle α due to the slack of the guide					
$\alpha_{\rm G}^{}, \alpha_{\rm s}^{}$	Terms used in calculating ϕ_4					
α _t	Part of the skewing angle α due to tolerances					
а _w	Part of the skewing angle α due to wear					
β	Angle between horizontal plane and non-horizontal wind direction					

Symbols, abbreviations	Description						
β_2	Term used in calculating ϕ_2						
β_3	Term used in calculating ϕ_3						
γ _f	Overall safety factor						
γ _m	Resistance coefficient						
γ _n	Risk coefficient						
γ _p	Partial safety factor						
γ _s	Additional safety factor for stability						
δ	Term used in calculating ϕ_1						
^E s	Conventional start force factor						
€ _M	Conventional mean drive force factor						
η	Shielding factor						
$\eta_{_{\sf W}}$	Factor for remaining hoist load in out of service condition						
λ	Aerodynamic slenderness ratio PREVIEW						
μ, μ'							
F	Term used in calculating the guide force F_y						
F _{1i} , F _{2i}	Terms used in calculating (H-2 and F y1i standards.iteh.ai/catalog/standards/sist/ac4f422b-9c6c-4dd9-9b4a-						
ξ	Term used in calculating ϕ_7 13001-2-2014						
^خ 1i', ^خ 2i	Term used in calculating F_{x1i} and F_{x2i}						
$\xi_{\rm G}(\alpha_{\rm G}),\xi_{\rm s}(\alpha_{\rm s})$	Curve factors						
ρ	Density of the air						
φ	Solidity ratio						
ϕ_{i}	Dynamic factors						
$\phi_1^{}$	Dynamic factor acting on the mass of the crane						
ϕ_2	Dynamic factor on hoist load when hoisting an unrestrained grounded load in regular operation						
$\phi_{_{ m 2C}}$	Dynamic factor on hoist load when hoisting an unrestrained grounded load under exceptional conditions						
$\phi_{2,\min}$	Term used in calculating ϕ_2						
ϕ_3	Dynamic factor for inertial and gravity effects by sudden release of a part of the hoist load						
ϕ_4	Dynamic factor for loads caused by travelling on uneven surface						
ϕ_5	Dynamic factor for loads caused by acceleration of all crane drives						
ϕ_6	Dynamic factor for test loads						

Symbols, abbreviations	Description				
$\phi_{_{7}}$	Dynamic factor for loads due to buffer forces				
$\phi_8^{}$	Gust response factor				
$\phi_{\rm L}^{},\phi_{\rm ML}^{}$	Factors for calculation of force in case the load or moment limiter is activated				
Ψ	Reduction factor used in calculating aerodynamic coefficients				

4 Safety requirements and/or measures

4.1 General

Loads and load combinations, as given in 4.2 and 4.3, shall only be applied as relevant for specified configurations and operational conditions of the crane.

The load actions shall be taken into account in proofs against failure by uncontrolled movement, yielding, elastic instability and, where applicable, against fatigue.

4.2 Loads

4.2.1 General

4.2.1.1 Introduction

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The loads acting on a crane are divided into the categories of regular, occasional and exceptional as given in 4.2.1.2, 4.2.1.3 and 4.2.1.4. For the proof calculation of means of access, loads only acting locally are given in 4.2.4.13. Combinations of regular, occasional and lexceptional loads into load combinations A, B and C are given in 4.3. 9cacf2d07eea/sist-en-13001-2-2014

4.2.1.2 Regular loads

Regular loads are those loads that occur frequently under normal operation.

- a) Hoisting and gravity effects acting on the mass of the crane;
- b) inertial and gravity effects acting vertically on the hoist load;
- c) loads caused by travelling on uneven surface;
- d) loads caused by acceleration of all crane drives;
- e) loads induced by displacements.

4.2.1.3 Occasional loads

- a) Loads due to in-service wind;
- b) snow and ice loads;
- c) loads due to temperature variation;
- d) loads caused by skewing.

Occasional loads occur infrequently. They are usually neglected in fatigue assessment.

4.2.1.4 Exceptional loads

- a) Loads caused by hoisting a grounded load under exceptional circumstances;
- b) loads due to out-of-service wind;
- c) test loads;
- d) loads due to buffer forces;
- e) loads due to tilting forces;
- f) loads caused by emergency cut-out;
- g) loads due to dynamic cut-off by lifting force limiting device;
- h) loads due to dynamic cut-off by lifting moment limiting device;
- i) loads due to unintentional loss of hoist load;
- j) loads caused by failure of mechanism or components;
- k) loads due to external excitation of grane support D PREVIEW
- I) loads caused by erection and dismantlingards.iteh.ai)

Exceptional loads are also infrequent and are likewise usually excluded from fatigue assessment.

4.2.2 Regular loads ystandards.iteh.ai/catalog/standards/sist/ac4f422b-9c6c-4dd9-9b4a-9cacf2d07eea/sist-en-13001-2-2014

4.2.2.1 Hoisting and gravity effects acting on the mass of the crane

When lifting the load off the ground or when releasing the load or parts of the load, the crane structure is under effect of vibration excitation, which shall be taken into account as a load effect. The gravitational force induced by the mass of the crane or crane part shall be multiplied by the factor ϕ_1 . Dependent upon the gravitational load effect of the mass and load combination in question, the factor ϕ_1 is calculated in accordance with either Formula (1) or (2). For definitions of unfavourable and favourable load effects see 4.3.3.

The gravitational load effect of the mass is unfavourable, Formula (1) applies:

$$\phi_1 = 1 + \delta \qquad \text{with } 0 \le \delta \le 0, 1 \tag{1}$$

The gravitational load effect of the mass is favourable, Formula (2) applies:

$$\phi_1 = 1 - \delta \qquad \text{with } 0 \le \delta \le 0,05 \tag{2}$$

The maximum values of δ from the Formulae (1) and (2) shall be used unless other values are justified by measurements, calculations or obtained from the appropriate European Standard for the particular type of crane.

The mass of the crane includes those components which are always in place during operation except for the net load itself. For some cranes or applications, it may be necessary to add mass to account for accumulation of debris.

4.2.2.2 Hoisting an unrestrained grounded load

When hoisting an unrestrained grounded load, the crane is subject to dynamic effects of transferring the load off the ground onto the crane. These dynamic effects shall be taken into account by multiplying the gravitational force due to the mass of the hoist load m_{μ} by a factor ϕ_2 , see Figure 1.

The mass of the hoist load includes the masses of the payload, lifting attachments and a portion of the suspended hoist ropes or chains.

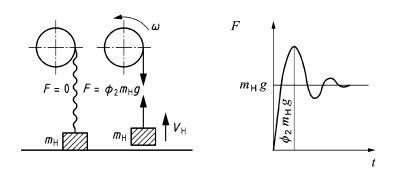


Figure 1 — Dynamic effects when hoisting a grounded load

The values of ϕ_2 and ϕ_{2C} shall be either calculated from the Formula (3) or be determined experimentally or by dynamic analysis. Where the Formula (3) is not used, the true characteristics of the drive system and the elastic properties of the overall load supporting system shall be taken into account. The dynamic factor ϕ_2 (and respectively ϕ_{2C} for Load combination C1, see 4.2.4.1) is calculated with the Formula (3):

 $\phi_2 = \phi_{2,\min} + \beta_2 \times v_h \qquad \frac{\text{SIST EN 13001-2.2014}}{\text{https://standards.iteh.ai/catalog/standards/sist/ac4f422b-9c6c-4dd9-9b4a-}$ (3) 9cacf2d07eea/sist-en-13001-2-2014

where

 β_2 is the factor dependent upon the stiffness class of the crane in accordance with the Table 2,

 $v_{\rm h}$ is the characteristic hoisting speed of the load in [m/s] in accordance with the Table 3, different for calculations of ϕ_2 and $\phi_{2\rm C}$,

 $\phi_{2\min}$ is the minimum value of ϕ_2 and ϕ_{2C} in accordance with Table 4.

For the purposes of this standard, cranes may be assigned to stiffness classes ranging from HC1 to HC4 in accordance with the elastic properties of the crane and its support. The stiffness classes given in the Table 2 shall be selected on the basis of the characteristic vertical load displacement δ .

Stiffness class	Factor β_2 [s/m]			
HC1	0,8 m ≤ δ	0,17		
HC2	0,3 m ≤ δ < 0,8 m	0,34		
HC3	0,15 m ≤ δ < 0,3 m	0,51		
HC4	δ < 0,15 m	0,68		
The stiffness classes were called hoisting classes in the earlier versions of this standard.				

The characteristic vertical load displacement δ shall be obtained by measurement or calculated from the elasticity of the crane structure, the rope system and the crane support, using the maximum hoist load value and setting the partial safety factors and dynamic factors to 1,0. Product type crane standards may give specific guidance on selection of stiffness classes.

Where the characteristic vertical load displacement δ varies for differing crane configurations, the maximum value of δ may be used for the selection of the stiffness class.

For the purposes of this standard, hoist drives shall be assigned to classes HD1 to HD5 depending on the control characteristics as the weight of the load is transferred from the ground onto the crane. The hoist drive classes are specified as follows:

- HD1: Creep speed is not available or the start of the drive without creep speed is possible;
- HD2: Hoist drive can only start at creep speed of at least a preset duration;
- HD3: Hoist drive control maintains creep speed until the load is lifted off the ground;
- HD4: Step-less hoist drive control, which performs with continuously increasing speed;
- HD5: Step-less hoist drive control automatically ensures that the dynamic factor ϕ_2 does not exceed $\phi_{2,\min}$.

See Annex B for illustration of the types of hoist drives.

The characteristic hoisting speed $v_{\rm h}$ to be used in load combinations A, B and C is given in the Table 3.

Load combination	(standards iteh ai)					Factor calculated by	
(see 4.3.6)	HD1	HD <u>2ISTE</u>	N 130 HP3 :2014	HD4	HD5	Formula (3)	
A1, B1	https://standard V _{h,max}	s.iteh.ai/catalog/s 9cact©807eea	tandards/sist/ac4 v /sist-erÞ, ¢§ 001-2	4225-9c6c-4dd 0,5 · V -2014 h,max	$v_{\rm h}^{0-9b4a-} = 0$	ϕ_2	
C1	-	$v_{h,max}$	_	$v_{h,\max}$	$0,5 \cdot v_{\mathrm{h,max}}$	$\phi_{_{\rm 2C}}$	
Key							

Table 3 — Characteristic hoisting speeds v_b for calculation of ϕ_a and ϕ_b

 $v_{\rm h,max}$ for load combinations A1 and B1: the maximum steady hoisting speed of the load;

 $v_{h,max}$ for load combination C1 (see 4.2.4.1): the maximum hoisting speed resulting from all drives (e.g. luffing and hoisting motion) contributing to the hoisting speed of the load;

 $v_{h,CS}$ is the steady hoisting creep speed.

The minimum value $\phi_{2,\min}$ depends upon the combination of the classes HC and HD and shall be selected in accordance with the Table 4.

Ŷ2,min						
Stiffness	Hoist drive class					
class	HD1	HD2	HD3	HD4	HD5	
HC1	1.05	1.05	1.05	1.05	1.05	
HC2	1.1	1.1	1.05	1.1	1.05	
HC3	1.15	1.15	1.05	1.15	1.05	
HC4	1.2	1.2	1.05	1.2	1.05	

Table 4 — Selection of ϕ_{2m}