

Designation: E 18 – 05

Standard Test Methods for Rockwell Hardness and Rockwell Superficial Hardness of Metallic Materials^{1,2}

This standard is issued under the fixed designation E 18; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ϵ) indicates an editorial change since the last revision or reapproval.

This standard has been approved for use by agencies of the Department of Defense.

1. Scope*

1.1 These test methods cover the determination of the Rockwell hardness and the Rockwell superficial hardness of metallic materials, including test methods for the verification of machines for Rockwell hardness testing (Part B) and the calibration of standardized hardness test blocks (Part C).

1.2 Values stated in inch-pound units are to be regarded as the standard. SI units are provided for information only.

1.3 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use. (See Note 6.)

NOTE 1-The National Institute of Standards and Technology (NIST) maintains the national Rockwell hardness standards for the United States. In June 1998, NIST released new Rockwell C scale (HRC) test blocks as Standard Reference Materials (SRMs). The blocks were calibrated using NIST's primary reference standardizing machine. The major benefit of the NIST standards is that their HRC levels are in line with the other industrialized countries around the world. The NIST HRC levels establish the hardness of materials slightly harder than the historical standards used in the United States for the past 75 years. The revision of E 18 requires that all performance verifications of Rockwell hardness indenters and hardness machines must be made using test blocks calibrated traceable to the Rockwell standards maintained by NIST. This can be accomplished through the use of commercial test blocks calibrated traceable to the NIST standards or by directly using the NIST SRMs. This requirement will apply only to the Rockwell scale(s) for which NIST supplies primary reference test blocks

Note 2—Previous editions of this standard have stated that the steel ball was the standard type of Rockwell indenter ball. Starting with this edition, the tungsten carbide ball is considered the standard type of Rockwell indenter ball. The use of tungsten carbide balls will provide an improvement to the Rockwell hardness test because of the tendency of steel balls to flatten with use, which results in an erroneously elevated hardness value. The user is cautioned that Rockwell hardness tests comparing the use of steel and tungsten carbide balls have been shown to give different results. For example, depending on the material tested and its hardness level, Rockwell B scale tests using a tungsten carbide ball indenter have given results up to one Rockwell point lower than when a steel ball indenter is used.

2. Referenced Documents

- 2.1 ASTM Standards: ³
- A 370 Test Methods and Definitions for Mechanical Testing of Steel Products
- **B** 19 Specification for Cartridge Brass Sheet, Strip, Plate, Bar, and Disks (Blanks)
- **B 36/B36** M Specification for Brass Plate, Sheet, Strip, and Rolled Bar
- **B** 96 Specification for Copper-Silicon Alloy Plate, Sheet, Strip, and Rolled Bar for General Purposes and Pressure Vessels
- **B** 97 Specification for Copper-Silicon Alloy Plate, Sheet, Strip, and Rolled Bar for General Purposes⁴
- **B** 103/B 103 M Specification for Phosphor Bronze Plate, Sheet, Strip, and Rolled Bar
- B 121/B 121 M Specification for Leaded Brass Plate, Sheet, Strip, and Rolled Bar
- B 122/B 122 M Specification for Copper-Nickel-Tin Alloy, Copper-Nickel-Zinc Alloy (Nickel Silver), and Copper-Nickel Alloy Plate, Sheet, Strip, and Rolled Bar
- B 130 Specification for Commercial Bronze Strip for Bullet Jackets
- **B** 134 Specification for Brass Wire
- B 152 Specification for Copper Sheet, Strip, Plate, and Rolled Bar
- B 291 Specification for Copper-Zinc-Manganese Alloy (Manganese Brass) Sheet and Strip
- **B** 370 Specification for Copper Sheet and Strip for Building Construction
- E 4 Practices for Force Verification of Testing Machines
- E 29 Practice for Using Significant Digits in Test Data to

¹ These test methods are under the jurisdiction of ASTM Committee E28 on Mechanical Testing and are the direct responsibility of Subcommittee E28.06 on Indentation Hardness Testing.

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² In this test method, the term Rockwell refers to an internationally recognized type of indentation hardness test as defined in Section 3, and not to the hardness testing equipment of a particular manufacturer.

³ For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

⁴ Withdrawn.

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Determine Conformance with Specifications

E 140 Hardness Conversion Tables for Metals

E 691 Practice for Conducting an Interlaboratory Study to Determine the Precision of a Test Method

3. Terminology

3.1 Definitions:

3.1.1 *calibration*—determination of the values of the significant parameters by comparison with values indicated by a reference instrument or by a set of reference standards.

3.1.2 *Rockwell hardness number, HR*—a number derived from the net increase in the depth of indentation as the force on an indenter is increased from a specified preliminary test force to a specified total test force and then returned to the preliminary test force.

3.1.2.1 *Discussion—Indenters*—Indenters for the Rockwell hardness test include a diamond spheroconical indenter and ball indenters of specified diameters. The tungsten carbide ball is considered to be the standard type of Rockwell indenter ball for all Rockwell ball scale hardness testing. Steel indenter balls may be used only if specified in a product specification or by special agreement.

3.1.2.2 *Discussion*—Rockwell hardness numbers are always quoted with a scale symbol representing the indenter and forces used. The hardness number is followed by the symbol HR and the scale designation. When a ball indenter is used, the scale designation is followed by the letter "W" to indicate the use of a tungsten carbide ball or the letter "S" to indicate the use of a steel ball.

3.1.2.3 *Examples*—64 HRC = Rockwell hardness number of 64 on Rockwell C scale. 81 HR30N = Rockwell superficial hardness number of 81 on Rockwell 30N scale. 72 HRBW = Rockwell hardness number of 72 on the Rockwell B scale measured using a tungsten carbide ball indenter.

3.1.3 *Rockwell hardness test*—an indentation hardness test using a verified machine to force a diamond spheroconical indenter (diamond indenter), or a ball indenter under specified conditions, into the surface of the material under test in two operations, and to measure the difference in depth of the indentation under the specified conditions of preliminary and total test forces (minor and major loads, respectively).

3.1.4 *Rockwell superficial hardness test*—same as the Rockwell hardness test except that smaller preliminary and total test forces are used.

3.1.5 *verification*—checking or testing to assure conformance with the specification.

4. Significance and Use

4.1 The Rockwell hardness test is an empirical indentation hardness test. Rockwell hardness tests provide useful information about metallic materials. This information may correlate to tensile strength, wear resistance, ductility, and other physical characteristics of metallic materials, and may be useful in quality control and selection of materials.

4.2 Rockwell hardness testing at a specific location on a part may not represent the physical characteristics of the whole part or end product.

4.3 Rockwell hardness tests are considered satisfactory for acceptance testing of commercial shipments, and have been used extensively in industry for this purpose.

4.4 Performance verifications of Rockwell hardness indenters and hardness machines shall be made using test blocks calibrated traceable to the Rockwell standards maintained by NIST when primary reference test blocks are available from NIST for the specific Rockwell scale.

https://standards.iteh.ai/catalog/standards/sist/4e1ab5e5-cac6-4dad-85e4-d52c0df7dbad/astm-e18-05

A. GENERAL DESCRIPTION AND TEST PROCEDURE FOR ROCKWELL HARDNESS AND ROCKWELL SUPERFICIAL HARDNESS TESTS

5. Principles of Test and Apparatus

5.1 *General Principles*—The general principles of the Rockwell hardness test are illustrated in Fig. 1 (diamond indenter) and Fig. 2 (ball indenters) and the accompanying

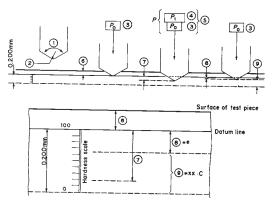


FIG. 1 Rockwell Hardness Test with Diamond Indenter (Rockwell C Example) (Table 1)

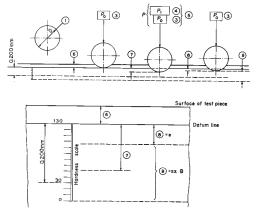


FIG. 2 Rockwell Hardness Test with Ball Indenter (Rockwell B Example) (Table 2)

Table 1 and Table 2. In the case of the Rockwell superficial test the general principles are illustrated in Fig. 3 (diamond indenter) and Fig. 4 (ball indenter) and the accompanying Table 3 and Table 4.



TABLE 1 Symbols and Designations Associated with Fig. 3

_		,	
	Number	Symbol	Designation
	1		Angle at the top of the diamond indenter (120°)
	2		Radius of curvature at the tip of the cone (0.200 mm)
	3	Po	Preliminary Test Force = 10 kgf (98 N)
	4	P_1	Additional Force = 140 kgf (1373 N)
	5	P	Total Test Force = $P_0 + P_1 = 10 + 140 = 150$ kgf (1471 N)
	6		Depth of penetration under preliminary test force before application of additional force
	7		Increase in depth of penetration under additional force
	8	е	Permanent increase in depth of penetration under preliminary test force after removal of additional force, the increase being expressed in units of 0.002 mm
_	9	xx HRC	Rockwell C hardness = 100 - e

TABLE 2 Symbols and Designations Associated with Fig. 2

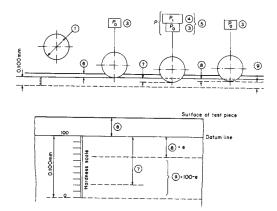


FIG. 4 Rockwell Superficial Hardness Test with Ball Indenter (Rockwell 30T Example) (Table 4)

TABLE 3 S	vmbols and	Designations	Associated	with Fig. 3
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Number	Symbol	Designation	Number	Symbol	Designation
1	D	Diameter of ball = $\frac{1}{16}$ in. (1.588 mm)	1		Angle at the tip of the diamond indenter (120°)
3	Po	Preliminary Test Force = 10 kgf (98 N)	2		Radius of curvature at the tip of the cone (0.200
4	P_1	Additional force = 90 kgf (883 N)			mm)
5	P	Total Test Force = $P_0 + P_1 = 10 + 90 = 100$ kgf (981	3	Po	Preliminary Test Force = 3 kgf (29 N)
		N)	4	P_1	Additional force = 27 kgf (265 N)
6		Depth of penetration under preliminary test force	5	Р	Total Test Force = $P_0 + P_1 = 3 + 27 = 30$ kgf (294 N)
		before application of additional force	6		Depth of penetration under preliminary test force
7		Increase in depth of penetration under additional			before application of additional force
		force	7		Increase in depth of penetration under additional
8	е	Permanent increase in depth of penetration under			force
		preliminary test force after removal of the additional	8	е	Permanent increase in depth of penetration under
		force, the increase being expressed in units of			preliminary test force after removal of additional
		0.002 mm			force, the increase being expressed in units of
9	xx HRB	Rockwell B hardness = 130 - e			0.001 mm
			9	xx HR30N	Rockwell 30N hardness = 100 - e
			TABL	E 4 Symbol	s and Designations Associated with Fig. 4
1	e (1)			E 4 Symbol Symbol	s and Designations Associated with Fig. 4 Designation
				Symbol	Designation
		ASTM E alo / ⊕ lard@sist/4e1ab5	Number 1	Symbol	Designation
				Symbol $5^{-D}_{-P_0}$ dad -85	Designation Diameter of ball = 1/16 in. (1.588 mm) Preliminary Test Force = 3 kgf (29 N)
			Number	Symbol	Designation Diameter of ball = 1/16 in. (1.588 mm) Preliminary Test Force = 3 kgf (29 N) Additional force = 27 kgf (265 N)
		<u>dod ie o dao / o dardo</u> ist/4e1ab5	Number - 1 - 3 - 4	Symbol P_0 dad-85 P_1 P	DesignationDiameter of ball = $\frac{1}{16}$ in. (1.588 mm)Preliminary Test Force = 3 kgf (29 N)Additional force = 27 kgf (265 N)Total Test Force = $P_0 + P_1 = 3 + 27 = 30$ kgf (294 N)
		<u>ASTME</u> <u>ASTME</u> <u>ASTME</u> <u>ASTME</u> <u>ASTME</u> <u>ASTME</u> <u>Surface of test piece</u>	Number 	Symbol P_{P_0} Symbol P_1	Designation Diameter of ball = $\frac{1}{16}$ in. (1.588 mm) Preliminary Test Force = 3 kgf (29 N) Additional force = 27 kgf (265 N) Total Test Force = $P_0 + P_1 = 3 + 27 = 30$ kgf (294 N) Depth of penetration under preliminary test force
		ASTME A @ d ite @ data / @ da	Number 	Symbol P_0 dad-85 P_1 P	Designation Diameter of ball = $\frac{1}{16}$ in. (1.588 mm) Preliminary Test Force = 3 kgf (29 N) Additional force = 27 kgf (265 N) Total Test Force = $P_0 + P_1 = 3 + 27 = 30$ kgf (294 N) Depth of penetration under preliminary test force before application of additional force
		ASTME A Od ite O taio / O hard osist/4e lab5	Number - 1 - 3 - 4 - 5 - 6	Symbol D Podad-85 P1 P 	Designation Diameter of ball = $\frac{1}{16}$ in. (1.588 mm) Preliminary Test Force = 3 kgf (29 N) Additional force = 27 kgf (265 N) Total Test Force = $P_0 + P_1 = 3 + 27 = 30$ kgf (294 N) Depth of penetration under preliminary test force
		ASTME ASTME ASTME ASTME ASTME Surface of test piece Surface of test piece Dotum line	Number - 1 - 3 - 4 - 5 - 6	Symbol D Podad-85 P1 P 	Designation Diameter of ball = $\frac{1}{16}$ in. (1.588 mm) Preliminary Test Force = 3 kgf (29 N) Additional force = 27 kgf (265 N) Total Test Force = $P_0 + P_1 = 3 + 27 = 30$ kgf (294 N) Depth of penetration under preliminary test force before application of additional force Increase in depth of penetration under additional
		ASTM E ASTM E ASTM E ASTM E ASTM E Surface of test piece Surface of test piece	Number 65-63-06 4 5 6 7	Symbol - Podad-85 P1 P 	Designation Diameter of ball = $\frac{1}{16}$ in. (1.588 mm) Preliminary Test Force = 3 kgf (29 N) Additional force = 27 kgf (265 N) Total Test Force = $P_0 + P_1 = 3 + 27 = 30$ kgf (294 N) Depth of penetration under preliminary test force before application of additional force Increase in depth of penetration under additional force force
	J 	ASTME ASTME ASTME ASTME ASTME Surface of test piece Surface of test piece Dotum line	Number 65-63-06 4 5 6 7	Symbol - Podad-85 P1 P 	DesignationDiameter of ball = $\frac{1}{16}$ in. (1.588 mm)Preliminary Test Force = 3 kgf (29 N)Additional force = 27 kgf (265 N)Total Test Force = $P_0 + P_1 = 3 + 27 = 30$ kgf (294 N)Depth of penetration under preliminary test forcebefore application of additional forceIncrease in depth of penetration under additionalforcePermanent increase in depth of penetration under
		ASTM E ASTM E ASTM E ASTM E ASTM E Surface of test piece Surface of test piece	Number 65-63-06 4 5 6 7	Symbol - Podad-85 P1 P 	Designation Diameter of ball = $\frac{1}{16}$ in. (1.588 mm) Preliminary Test Force = 3 kgf (29 N) Additional force = 27 kgf (265 N) Total Test Force = $P_0 + P_1 = 3 + 27 = 30$ kgf (294 N) Depth of penetration under preliminary test force before application of additional force Increase in depth of penetration under additional force Permanent increase in depth of penetration under preliminary test force additional force
		Surface of test piece	Number 65-63-06 4 5 6 7	Symbol - Podad-85 P1 P 	Designation Diameter of ball = $\frac{1}{16}$ in. (1.588 mm) Preliminary Test Force = 3 kgf (29 N) Additional force = 27 kgf (265 N) Total Test Force = $P_0 + P_1 = 3 + 27 = 30$ kgf (294 N) Depth of penetration under preliminary test force before application of additional force Increase in depth of penetration under additional force Permanent increase in depth of penetration under preliminary test force after removal of the additional force, the increase being expressed in units of 0.001
	bockwell Sup	ASTM E ASTM E ASTM E ASTM E ASTM E Surface of test piece Surface of test piece	Number e5(3) c(4 5 6 7 8	Symbol 5-P _o dad-85 P ₁ P e	Designation Diameter of ball = $\frac{1}{16}$ in. (1.588 mm) Preliminary Test Force = 3 kgf (29 N) Additional force = 27 kgf (265 N) Total Test Force = $P_0 + P_1 = 3 + 27 = 30$ kgf (294 N) Depth of penetration under preliminary test force before application of additional force Increase in depth of penetration under additional force Permanent increase in depth of penetration under preliminary test force additional force, the increase being expressed in units of 0.001 mm

5.1.1 See Equipment Manufacturer's Instruction Manual for a description of the machine's characteristics, limitations, and respective operating procedures. Typical applications of the various hardness scales are shown in Tables 5 and 6. Rockwell hardness values are usually determined and reported in accordance with one of these standard scales. An indenter is forced into the surface of a test piece in two steps under specified conditions (see Section 7) and the difference in depth of indentation is measured as e.

5.1.2 The unit measurement for e is 0.002 mm and 0.001 mm for the Rockwell hardness test and Rockwell superficial hardness test, respectively. From the value of e, a number

known as the Rockwell hardness is derived. There is no Rockwell hardness value designated by a number alone because it is necessary to indicate which indenter and force have been employed in making the test (see Table 5 and Table 6).

5.2 Description of Machine and Method of Test—The tester for making Rockwell hardness determinations is a machine that measures hardness by determining the difference in penetration depths of an indenter under two specified forces, called preliminary and total test forces.

5.2.1 There are two general classifications of the Rockwell test: the Rockwell hardness test and the Rockwell superficial hardness test.

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TABLE 5 Rockwell Hardness Scales

Scale Symbol	Indenter	Total Test Force, kgf	Dial Figures		Typical Applications of Scales Copper alloys, soft steels, aluminum alloys, malleable iron, etc.			
В	¹ /16-in. (1.588-mm) ball	100	red					
С	diamond	150	black		Steel, hard cast irons, pearlitic malleable iron, titanium, deep case hardened steel, and other materials harder than B100.			
А	diamond	60	black		Cemented carbides, thin steel, and shallow case-hardened steel.			
D	diamond	100	black		Thin steel and medium case hardened steel, and pearlitic malleable iron.			
E	1/8-in. (3.175-mm) ball	100	red		Cast iron, aluminum and magnesium alloys, bearing metals.			
F	¹ /16-in. (1.588-mm) ball	60	red		Annealed copper alloys, thin soft sheet metals.			
G	¹ /16-in. (1.588-mm) ball	150	red		Malleable irons, copper-nickel-zinc and cupro-nickel alloys. Upper limit G92 to avoid possible flattening of ball.			
Н	¹ /8-in. (3.175-mm) ball	60	red)	Aluminum, zinc, lead.			
K	¹ / ₈ -in. (3.175-mm) ball	150	red					
L	¹ / ₄ -in. (6.350-mm) ball	60	red					
М	¹ / ₄ -in. (6.350-mm) ball	100	red		Bearing metals and other very soft or thin materials. Use smallest ball and heaviest load that does			
Р	¹ / ₄ -in. (6.350-mm) ball	150	red	5	not give anvil effect.			
R	½-in. (12.70-mm) ball	60	red		•			
S	¹ /2-in. (12.70-mm) ball	100	red					
V	½-in. (12.70-mm) ball	150	red	J				

TABLE 6	Rockwell	Superficial	Hardness	Scales
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Total Test Force,			Scale Symbols		
,	N Scale, Diamond	T Scale, 1/16-in.	W Scale, ¹ /8-in.	X Scale, 1/4-in.	Y Scale, 1/2-in.
kgf (N)	Indenter	(1.588-mm) Ball	(3.175-mm) Ball	(6.350-mm) Ball	(12.70-mm) Ball
15 (147)	15N	15T	15W	15X	15Y
30 (294)	30N	30T	30W	30X	30Y
45 (441)	45N	45T	45W	45X	45Y

5.2.2 In the Rockwell hardness test the preliminary test force is 10 kgf (98 N). Total test forces are 60 kgf (589 N), 100 kgf (981 N) and 150 kgf (1471 N). In the Rockwell superficial hardness test the preliminary test force is 3 kgf (29 N) and total test forces are 15 kgf (147 N), 30 kgf (294 N), and 45 kgf (441 N). The indenter for either test shall be of a spheroconical or spherical configuration. Scales vary by a combination of total test force and type of indenter.

5.2.3 The difference in depth is normally measured by an electronic device or by a dial indicator. The hardness value, as read from the instrument, is an arbitrary number which is related to the difference in the depths produced by the two forces; and since the scales are reversed, the higher the number the harder the material.

5.2.4 In accordance with the operating procedures recommended by the manufacturer of the hardness tester, the test is started by applying the preliminary test force causing an initial penetration of the specimen. Since measurement of the difference in depth starts after the preliminary force has been applied, the dial gage pointer is set to zero if the instrument is a dial indicator model. On a digital readout instrument, the zero point is captured by the electronics automatically. The instrument shall be designed to eliminate the effect of impact in applying the preliminary test force.

5.2.5 The additional force is applied for the required dwell time and then removed. The return to the preliminary test force position holds the indenter at the point of deepest penetration yet allows elastic recovery to occur and the stretch of the frame to be factored out. The test result is displayed by the testing machine.

5.3 Indenters:

5.3.1 The standard Rockwell indenters are either diamond spheroconical indenters or indenters having tungsten carbide

balls 1.588 mm (1/16 in.), 3.175 mm (1/8 in.), 6.350 mm (1/4 in.), or 12.70 mm (1/2 in.) in diameter. Steel indenter balls may be used only if specified in a product specification or by special agreement. The diamond indenter shall conform to the requirements prescribed in 13.1.2.1. Indenter balls shall conform to the requirements prescribed in 13.1.2.2.

5.3.2 Dust, dirt, grease, and scale shall not be allowed to accumulate on the indenter as this will affect the test results.

5.4 *Anvils*—An anvil shall be used that is suitable for the specimen to be tested. The seating and supporting surfaces of all anvils shall be clean and smooth and shall be free from pits, deep scratches, and foreign material. If the provisions of 6.3 on thickness of the test piece are complied with, there will be no danger of indenting the anvil, but, if it is so thin that the impression shows through on the under side, the anvil may be damaged. Damage may also occur from accidental contacting of the anvil by the indenter. If the anvil is damaged from any cause, it shall be replaced. Anvils showing the least visible dent will give inaccurate results on thin material.

5.4.1 Cylindrical pieces shall be tested with a V-grooved anvil that will support the specimen with the axis of the V-groove directly under the indenter or on hard, parallel, twin cylinders properly positioned and clamped in their base.

5.4.2 Flat pieces shall be tested on a flat anvil that has a smooth, flat bearing surface whose plane is perpendicular to the axis of the indenter.

5.4.3 For thin materials or specimens that are not perfectly flat, an anvil having an elevated, flat spot about ¹/₄ in. (6 mm) in diameter shall be used. This spot shall be polished smooth and flat and shall have a Rockwell hardness of at least 60 HRC. Very soft material should not be tested on the spot anvil

because the applied force may cause the penetration of the anvil into the under side of the specimen regardless of its thickness.

5.4.4 When testing thin sheet material with a ball indenter, it is recommended that a diamond spot anvil be used.

NOTE 3—Caution: A diamond spot anvil should only be used with a superficial hardness tester and ball indenter. This recommendation should be followed, except when directed otherwise by material specification.

5.5 *Test Blocks*—Test blocks meeting the requirements of Part C shall be used to periodically verify the hardness tester.

6. Test Piece

6.1 The test shall be carried out on a smooth, even surface that is free from oxide scale, foreign matter, and, in particular, completely free from lubricants. An exception is made for reactive metals, such as titanium, that may adhere to the indenter. In such situations, a suitable lubricant such as kerosene may be used. The use of a lubricant shall be reported on the test report.

6.2 Preparation shall be carried out in such a way that any alteration of the surface hardness (for example, due to heat or cold-working) is minimized.

6.3 The thickness of the test piece or of the layer under test should be as dictated in Tables 7-9, and Table 10 and as presented graphically in Figs. 5 and 6. These tables were determined from studies on strips of carbon steel and give reliable results. For all other materials it is recommended that the thickness exceed 10 times the depth of indentation with a diamond indentor and 15 times the depth of indentation with a ball indentor. As a rule, no deformation should be visible on the back of the test piece after the test although not all such marking is indicative of a bad test.

TABLE 7 A Minimum Thickness Guide for Selection of Scales Using the Diamond Indenter (see Fig. 5)

NOTE 1—For any given thickness, the indicated Rockwell hardness is the minimum value acceptable for testing. For a given hardness, material of any greater thickness than that corresponding to that hardness can be tested on the indicated scale.

Minimum	Thiskness		Rockwell Scale	
winimum			А	С
in.	mm	Hardness Reading	Approximate Hardness C-Scale ^A	Dial Reading
0.014	0.36			
0.016	0.41	86	69	
0.018	0.46	84	65	
0.020	0.51	82	61.5	
0.022	0.56	79	56	69
0.024	0.61	76	50	67
0.026	0.66	71	41	65
0.028	0.71	67	32	62
0.030	0.76	60	19	57
0.032	0.81			52
0.034	0.86			45
0.036	0.91			37
0.038	0.96			28
0.040	1.02			20

^A These approximate hardness numbers are for use in selecting a suitable scale and should not be used as hardness conversions. If necessary to convert test readings to another scale, refer to Hardness Conversion Tables E 140 (Relationship Between Brinell Hardness, Vickers Hardness, Rockwell Hardness, Rockwell Superficial Hardness, and Knoop Hardness).

TABLE 8 A Minimum Thickness Guide for Selection of Scales Using the $\frac{1}{16}$ -in. (1.588-mm) Diameter Ball Indenter (see Fig. 6)

NOTE 1—For any given thickness, the indicated Rockwell hardness is the minimum value acceptable for testing. For a given hardness, material of any greater thickness than that corresponding to that hardness can be tested on the indicated scale.

Minimum ⁻	Thickness	Rockwell Scale					
Minimum			F				
in.	mm	Hardness Reading	Hardness				
0.022	0.56						
0.024	0.61	98	72	94			
0.026	0.66	91	60	87			
0.028	0.71	85	49	80			
0.030	0.76	77	35	71			
0.032	0.81	69	21	62			
0.034	0.86			52			
0.036	0.91			40			
0.038	0.96			28			
0.040	1.02						

^A These approximate hardness numbers are for use in selecting a suitable scale and should not be used as hardness conversions. If necessary to convert test readings to another scale refer to Hardness Conversion Tables E 140 (Relationship Between Brinell Hardness, Vickers Hardness, Rockwell Hardness, Rockwell Superficial Hardness and Knoop Hardness).

6.4 For tests on convex cylindrical surfaces the corrections given in Tables 11-14 shall be applied. Corrections for tests on spherical and concave surfaces should be the subject of special agreement. When testing cylindrical specimens, the accuracy of the test will be seriously affected by alignment of elevating screw, V-anvil, indenters, surface finish, and the straightness of the cylinder. For diameters between those given in the tables, correction factors may be derived by linear interpolation. Tests performed on diameters smaller than those given in Tables 11-14 are not acceptable.

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6.5 Precautions for materials having excessive, timedependent plasticity (indentation creep): In the case of materials exhibiting plastic flow after application of the total test force, the indenter will continue to move. The total test force should be removed after the specified dwell time, and the time recorded after the test results (that is, 65 HRFW, 4 s) if longer than 3 s. When materials require the use of a dwell time greater than 3 s, this should be specified in the product specification.

7. Procedure

7.1 As part of the test procedure, periodic checks shall be performed. See Section 14 for recommendations.

7.2 The test is normally carried out at ambient temperature within the limits of 50 to 95° F (10 to 35° C). However, because temperature variation may affect the results, users of the Rockwell test may choose to control the temperature within a tighter range.

7.3 The test piece shall be supported rigidly so that no effects of displacement occur during the test.

7.4 Bring the indenter into contact with the test surface and apply the preliminary test force P_0 (minor load) of 10 kgf (98 N) for the Rockwell hardness test or 3 kgf (29 N) for Rockwell superficial hardness test in a direction perpendicular to the



TABLE 9 A Minimum Thickness Guide for Selection of Scales Using the Diamond Indenter (see Fig. 5)

NOTE 1—For any given thickness, the indicated Rockwell hardness is the minimum value acceptable for testing. For a given hardness, material of any greater thickness than that corresponding to that hardness can be tested on the indicated scale

Minimum	Thickness		Rockwell Superficial Scale							
winning	Minimum Thickness		5N	3	30N	45N				
in.	mm	Hardness Reading	Approximate Hardness C-Scale ^A	Hardness Reading	Approximate Hardness C-Scale ^A	Hardness Reading	Approximate Hardness C-Scale ^A			
0.006	0.15	92	65							
0.008	0.20	90	60							
0.010	0.25	88	55							
0.012	0.30	83	45	82	65	77	69.5			
0.014	0.36	76	32	78.5	61	74	67			
0.016	0.41	68	18	74	56	72	65			
0.018	0.46			66	47	68	61			
0.020	0.51			57	37	63	57			
0.022	0.56			47	26	58	52.5			
0.024	0.61					51	47			
0.026	0.66					37	35			
0.028	0.71					20	20.5			
0.030	0.76									

^A These approximate hardness numbers are for use in selecting a suitable scale, and should not be used as hardness conversions. If necessary to convert test readings to another scale, refer to Hardness Conversion Tables E 140 (Relationship Between Brinell Hardness, Vickers Hardness, Rockwell Hardness, Rockwell Superficial Hardness and Knoop Hardness).

TABLE 10 A Minimum Thickness Guide for Selection of Scales Using the 1/16 in. (1.588 mm) Diameter Ball Indenter (see Fig. 6)

NOTE 1—For any given thickness, the indicated Rockwell hardness is the minimum value acceptable for testing. For a given hardness, material of any greater thickness than that corresponding to that hardness can be tested on the indicated scale.

Minimum Thickness		1	Rockwell Superficial Scale						
		1	5T	3	от	45T			
in.	mm	Hardness Reading	Approximate Hardness B-Scale ^A	Hardness Reading	Approximate Hardness B-Scale ^A	Hardness Reading	Approximate Hardness B-Scale ^A		
0.010	0.25	91	CU 93 CI	IL PIEV	Iew				
0.012	0.30	86	78						
0.014	0.36	81	62	80	96				
0.016	0.41	75	44	72	84	71	99		
0.018	0.46	68	24	E18-064	71	62	90		
0.020	0.51	ailante lovelatared	and a laist / la lab	5 5 55 11	1 05 58 150-0	53	10 80		
0.022	0.56	.arcalalo <u>g</u> /stalid	alus/sisi/401al	45 45	43-030-43-03200	43 43	FC10-70		
0.024	0.61			34	28	31	58		
0.026	0.66					18	45		
0.028	0.71					4	32		
0.030	0.76								

^A These approximate hardness numbers are for use in selecting a suitable scale, and should not be used as hardness conversions. If necessary to convert test readings to another scale refer to Hardness Conversion Tables E 140 (Relationship Between Brinell Hardness, Vickers Hardness, Rockwell Hardness, Rockwell Superficial Hardness and Knoop Hardness).

surface without shock or vibration. (See Table 15 for tolerances of test forces.) The dwell time for the preliminary test force shall not exceed 3 s.

7.5 Establish the reference position (see *Manufacturer's Instruction Manual*) and increase the force, without shock or vibration, over a period of 1 to 8 s by the value of the additional test force, P_1 (additional load) needed to obtain the required total test force *P* for a given hardness scale (see Tables 5 and 6).

7.6 While maintaining the preliminary test force P_0 , remove the additional test force P_1 in accordance with the following:

7.6.1 For materials which, under the conditions of the test, show no time-dependent plasticity, remove P_1 within 3 s after the total test force is applied.

7.6.2 For materials which, under the conditions of the test, show some time-dependent plasticity, remove P_1 within 5 to 6

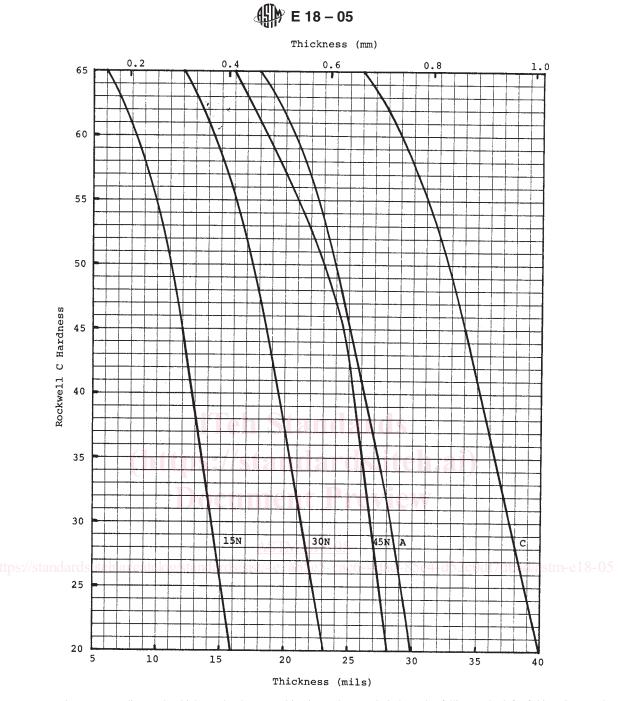
s when using diamond cone indenter and within 6 to 8 s when using a ball indenter after the application of the total test force begins.

7.6.3 In special cases where the material, under the conditions of the test, shows considerable time-dependent plasticity, remove P_1 within 20 to 25 s after the application of the total test force begins.

7.6.4 When materials require the use of a dwell time greater than 3 s, this shall be specified in the product specification, and the dwell time shall be recorded.

7.7 Throughout the test, the apparatus shall be protected from shock or vibration.

7.8 The Rockwell hardness number is derived from the differential increase in depth of indentation e and is usually read directly. The derivation of the Rockwell hardness number is illustrated in Figs. 1-4.



NOTE 1—Locate a point corresponding to the thickness-hardness combination to be tested. Only scales falling to the left of this point may be used to test this combination.

FIG. 5 Thickness Limits for Rockwell Hardness Testing Using the Diamond Indenter

7.9 After each change, or removal and replacement, of the indenter or the anvil, it shall be ascertained that the indenter (or the new anvil) is correctly mounted in its housing.

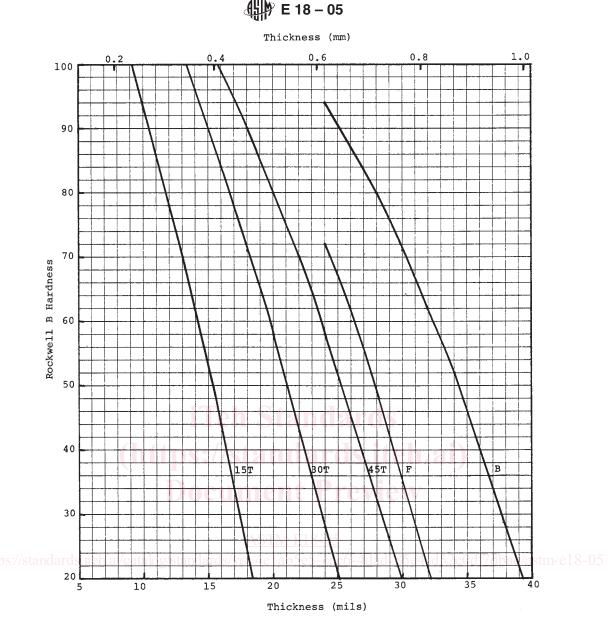
7.9.1 The first two readings after an indenter or anvil has been mounted shall be disregarded, and the operation of the machine checked with the appropriate standardized hardness test block.

NOTE 4—It is recognized that appropriate standardized test blocks are not available for all geometric shapes, or materials, or both.

7.10 The distance between the center of two adjacent indentations shall be at least three times the diameter of the indentation.

7.10.1 The distance from the center of any indentation to an edge of the test piece shall be at least two and a half times the diameter of the indentation.

7.11 Unless otherwise specified, all readings are to be reported to the nearest whole number, rounding in accordance with Practice E 29.



NOTE 1—Locate a point corresponding to the thickness-hardness combination to be tested. Only scales falling to the left of this point may be used to test this combination.

FIG. 6 Thickness Limits for Rockwell Hardness Testing Using the 1/16-in. (1.588-mm) Diameter Ball Indenter

8. Conversion to Other Hardness Scales or Tensile Strength Values

8.1 There is no general method of accurately converting the Rockwell hardness numbers on one scale to Rockwell hardness numbers on another scale, or to other types of hardness numbers, or to tensile strength values. Such conversions are, at best, approximations and, therefore, should be avoided except for special cases where a reliable basis for the approximate conversion has been obtained by comparison tests.

NOTE 5—The Standard Hardness Conversion Tables E 140, for Metals, give approximate conversion values for specific materials such as steel, austenitic stainless steel, nickel and high-nickel alloys, cartridge brass, copper alloys, and alloyed white cast irons.

NOTE 6—ASTM Specifications giving approximate hardness-tensile strength relationships are listed in Appendix X1.

9. Report

9.1 The report shall include the following information:

9.1.1 The Rockwell hardness number (see 3.1.2).

9.1.1.1 All reports of Rockwell hardness test readings shall indicate the scale used and also the ambient temperature of test if it was outside the 50 to 95°F (10 to 35°C) range (see 7.2). Unless otherwise specified, all readings are to be reported to the nearest whole number, rounding to be in accordance with Practice E 29.

🕼 E 18 – 05

TABLE 11	Corrections to Be	e Added to Rockw	ell C, A, and D Value	s Obtained on Convex	Cylindrical Surfaces ^A	of Various Diameters

				Diameters of	f Convex Cylindr	ical Surfaces			
Dial Reading	¹ ⁄ ₄ in. (6.4 mm)	³⁄≋ in. (10 mm)	½ in. (13 mm)	⁵⁄≋ in. (16 mm)	³ ⁄4 in. (19 mm)	⅔ in. (22 mm)	1 in. (25 mm)	1¼ in. (32 mm)	1½ in. (38 mm)
			Cor	rections to be Ad	lded to Rockwell	C, A, and D Valu	les ^B		
20	6.0	4.5	3.5	2.5	2.0	1.5	1.5	1.0	1.0
25	5.5	4.0	3.0	2.5	2.0	1.5	1.0	1.0	1.0
30	5.0	3.5	2.5	2.0	1.5	1.5	1.0	1.0	0.5
35	4.0	3.0	2.0	1.5	1.5	1.0	1.0	0.5	0.5
40	3.5	2.5	2.0	1.5	1.0	1.0	1.0	0.5	0.5
45	3.0	2.0	1.5	1.0	1.0	1.0	0.5	0.5	0.5
50	2.5	2.0	1.5	1.0	1.0	0.5	0.5	0.5	0.5
55	2.0	1.5	1.0	1.0	0.5	0.5	0.5	0.5	0
60	1.5	1.0	1.0	0.5	0.5	0.5	0.5	0	0
65	1.5	1.0	1.0	0.5	0.5	0.5	0.5	0	0
70	1.0	1.0	0.5	0.5	0.5	0.5	0.5	0	0
75	1.0	0.5	0.5	0.5	0.5	0.5	0	0	0
80	0.5	0.5	0.5	0.5	0.5	0	0	0	0
85	0.5	0.5	0.5	0	0	0	0	0	0
90	0.5	0	0	0	0	0	0	0	0

^A When testing cylindrical specimens, the accuracy of the test will be seriously affected by alignment of elevating screw, V-anvil, indenters, surface finish, and the straightness of the cylinder.

^B These corrections are approximate only and represent the averages to the nearest 0.5 Rockwell number, of numerous actual observations.

TABLE 12 Corrections to Be Added to Rockwell B, F, and G Values Obtained on Convex Cylindrical Surfaces^A of Various Diameters

	Diameters of Convex Cylindrical Surfaces							
Hardness Reading	¹ ⁄4 in. (6.4 mm)	³⁄₃ in. (10 mm)	½ in. (13 mm)	⁵‰ in. (16 mm)	³ ⁄4 in. (19 mm)	⁷ ⁄ ₈ in. (22 mm)	1 in. (25 mm)	
	Corrections to be Added to Rockwell B, F, and G Values ^B							
0	12.5	8.5	6.5	5.5	4.5	3.5	3.0	
10	12.0	8.0	6.0	5.0	4.0	3.5	3.0	
20	11.0	7.5	5.50	4.5	4.0	3.5	3.0	
30	10.0	6.5	5.0	4.5	3.5	3.0	2.5	
40	9.0	6.0	4.5	4.0	3.0	2.5	2.5	
50	8.0	5.5	4.0	3.5	3.0	2.5	2.0	
60	7.0	5.0	3.5	3.0	2.5	2.0	2.0	
70	6.0	4.0	3.0	2.5	2.0	2.0	1.5	
80	5.0	3.5	2.5	2.0	1.5	1.5	1.5	
90	4.0	3.0	2.0	1.5	1.5	1.5	1.0	
100	3.5	2.5	1.5 S I M	E18-0.5	1.0	1.0	0.5	

^A When testing cylindrical specimens, the accuracy of the test will be seriously affected by alignment of elevating screw, V-anvil, indenters, surface finish, and the straightness of the cylinder.

^B These corrections are approximate only and represent the averages to the nearest 0.5 Rockwell number, of numerous actual observations.

9.1.2 The time of application of the total test force if greater than 3 s.

9.1.3 Any lubricant that is used on the test surface (see 6.1).

10. Precision and Bias ⁵

10.1 *Precision*—A precision and bias study was conducted in 2000 in accordance with Practice 691. A total of 18 Rockwell hardness test blocks meeting the requirements of this standard were used for the study. Tests were performed using the following six Rockwell scales: HRA, HRC, HR30N, HRBS, HRES, and HR30TS. Test blocks in three different hardness levels in each scale were provided for the total of 18 blocks (see Table 16).

NOTE 7—The tests on the HRB, HRE and HR30T scales were made using a steel ball indenter. A subset of these tests are now being repeated using a tungsten carbide ball indenter and will be added to the Table 16 by November 2008.

10.2 The types of laboratories chosen to participate in this study were a combination of one commercial testing laboratory, five in-house laboratories and three test block manufacturer calibration laboratories. They were instructed to test each block three times in specific locations around the surface of the blocks in accordance with this standard.

10.3 The results given in Table 16 may be useful in interpreting measurement differences as follows.

10.3.1 The value of r indicates the typical amount of variation that can be expected between test results obtained for the same material by the same operator using the same hardness tester on the same day. When comparing two test results made under these conditions, a measurement difference of less than the r value for that Rockwell scale is an indication that the results may be equivalent.

10.3.2 The value of R indicates the typical amount of variation that can be expected between test results obtained for the same material by different operators using different hardness testers on different days. When comparing two test results made under these conditions, a measurement difference of less

⁵ Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR: E28–1021.

TABLE 13 Corrections to Be Added to Rockwell Superficial 15N, 30N, and 45N Values Obtained on Convex Cylindrical Surfaces of Various Diameters^A

	Diameters of Convex Cylindrical Surfaces							
Hardness Reading	⅓ in. (3.2 mm)	¹ ⁄4 in. (6.4 mm)	³∕₃ in. (10 mm)	½ in. (13 mm)	³⁄₄ in. (19 mm)	1 in. (25 mm)		
	Corrections to be Added to Rockwell Superficial 15N, 30N, and 45N Values ^B							
20	6.0	3.0	2.0	1.5	1.5	1.5		
25	5.5	3.0	2.0	1.5	1.5	1.0		
30	5.5	3.0	2.0	1.5	1.0	1.0		
35	5.0	2.5	2.0	1.5	1.0	1.0		
40	4.5	2.5	1.5	1.5	1.0	1.0		
45	4.0	2.0	1.5	1.0	1.0	1.0		
50	3.5	2.0	1.5	1.0	1.0	0.5		
55	3.5	2.0	1.5	1.0	0.5	0.5		
60	3.0	1.5	1.0	1.0	0.5	0.5		
65	2.5	1.5	1.0	0.5	0.5	0.5		
70	2.0	1.0	1.0	0.5	0.5	0.5		
75	1.5	1.0	0.5	0.5	0.5	0		
80	1.0	0.5	0.5	0.5	0	0		
85	0.5	0.5	0.5	0.5	0	0		
90	0	0	0	0	0	0		

^A When testing cylindrical specimens the accuracy of the test will be seriously affected by alignment of elevating screw, V-anvil, indenters, surface finish, and the straightness of the cylinder.

^B These corrections are approximate only and represent the averages, to the nearest 0.5 Rockwell superficial number, of numerous actual observations.

TABLE 14 Corrections to Be Added to Rockwell Superficial 15T, 30T, and 45T Values Obtained on Convex Cylindrical Surfaces^A of Various Diameters

	Diameters of Convex Cylindrical Surfaces						
Hardness Reading	¹⁄ଃ in. (3.2 mm)	¹ / ₄ in. (6.4 mm)	³ / ₈ in. (10 mm)	½ in. (13 mm)	⁵⁄≋ in. ∫ (16 mm)	³ ⁄4 in. (19 mm)	1 in. (25 mm)
	Corrections to be Added to Rockwell Superficial 15T, 30T, and 45T Values ^B						
20	13.0	9.0	6.0	4.5	4.5 91	3.0	2.0
30	11.5	7.5	5.0	3.5	3.5	2.5	2.0
40	10.0	6.5	4.5	3.5	3.0	2.5	2.0
50	8.5	5.5	4.0	3.0	2.5	2.0	1.5
60	6.5	4.5	3.0	2.5	2.0	1.5	1.5
70	5.0	3.5	2.5	2.0	1.5	1.0	1.0
80	3.0	2.0	1.5	1.5	1.0	1.0	0.5
90	1.5	1.0	1.0 CTM	0.5	0.5	0.5	0.5

^A When testing cylindrical specimens, the accuracy of the test will be seriously affected by alignment of elevating screw, V-anvil, indenters, surface finish, and the straightness of the cylinder. ^B These corrections are approximate only and represent the averages, to the nearest 0.5 Rockwell superficial number, of numerous actual observations.

TABLE 15 Tolerances on Applied Forces

_	Load, kgf (N)	Tolerance, kgf (N)	Test Block Avera	
_	10 (98)	±0.20 (±1.96)	62.8 HRA	
	60 (589)	±0.45 (±4.41)	73.1 HRA	
	100 (981)	±0.65 (±6.37)	83.9 HRA	
	150 (147)	±0.90 (±8.83)	25.0 HRC	
	3 (29)	±0.060 (±0.589)	45.0 HRC	
	15 (147)	±0.100 (±0.981)	65.0 HRC	
	30 (294)	±0.200 (±1.961)	45.9 HR30N	
	45 (441)	±0.300 (±2.943)	64.0 HR30N	
_			81.9 HB30N	

than the R value for that Rockwell scale is an indication that the results may be equivalent.

10.3.3 Any judgments based on 10.3.1 and 10.3.2 would have an approximate 95 % probability of being correct.

10.4 This precision and bias study was conducted on a selected number of the most commonly used Rockwell scales. For Rockwell scales not listed, the r and R values may be estimated using the conversion tables of E 140 to determine a corresponding increment of hardness for the scale of interest at the hardness level of interest. The user is cautioned that

TABLE 16 Results of the Precision and Bias Study

TABLE TO TRESURE OF the Treelaton and Dias ofday								
Test Block	Average Hardness	Sr	SR	r	R			
62.8 HRA	62.50	0.164	0.538	0.459	1.506			
73.1 HRA	73.04	0.138	0.358	0.387	1.002			
83.9 HRA	84.54	0.085	0.468	0.238	1.309			
25.0 HRC	24.99	0.335	0.440	0.937	1.232			
45.0 HRC	45.35	0.156	0.259	0.438	0.725			
65.0 HRC	65.78	0.153	0.389	0.427	1.089			
45.9 HR30N	46.75	0.299	2.489	0.837	6.969			
64.0 HR30N	64.74	0.248	0.651	0.694	1.822			
81.9 HR30N	82.52	0.195	0.499	0.547	1.396			
20.0 HRBS	20.45	0.502	1.480	1.405	4.144			
60.0 HRBS	60.72	0.230	0.410	0.643	1.149			
95.0 HRBS	96.52	0.289	0.345	0.808	0.967			
62.5 HRES	65.03	0.427	1.052	1.194	2.945			
81.0 HRES	79.82	0.251	0.474	0.703	1.328			
100.0 HRES	92.45	0.311	0.536	0.871	1.500			
22.0 HR30TS	24.04	0.292	1.466	0.818	4.106			
56.4 HR30TS	55.37	0.374	1.063	1.048	2.977			
79.0 HR30TS	78.88	0.274	0.835	0.766	2.338			

estimating the r and R values in this way, decreases the probability of them being correct.

10.5 Although the precision values given in Table 16 provide guidance on interpreting differences in Rockwell