# INTERNATIONAL STANDARD

ISO 6721-2

Second edition 2008-06-01

# Plastics — Determination of dynamic mechanical properties —

Part 2: **Torsion-pendulum method** 

Plastiques — Détermination des propriétés mécaniques dynamiques —

iTeh STPartie 2: Méthode au pendule de torsion (standards.iteh.ai)

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#### **Foreword**

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

International Standards are drafted in accordance with the rules given in the ISO/IEC Directives, Part 2.

The main task of technical committees is to prepare International Standards. Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights.

ISO 6721-2 was prepared by Technical Committee ISO/TC 61, *Plastics*, Subcommittee SC 2, *Mechanical properties*.

This second edition cancels and replaces the first edition (ISO 6721-2:1994), of which it constitutes a minor revision. It also incorporates the Technical Corrigendum ISO 6721-2:1994/Cor.1:1995. Apart from the inclusion of the Corrigendum (which concerns the last sentence in the first paragraph in Annex C), the main changes are the updating of the references and the correction of ISO 6721-3 to ISO 6721-1 in Subclause 5.6.

ISO 6721 consists of the following parts; hunder the ageneral title Plastics -46cc Determination of dynamic mechanical properties: 92d38ec9e7c8/iso-6721-2-2008

- Part 1: General principles
- Part 2: Torsion-pendulum method
- Part 3: Flexural vibration Resonance-curve method
- Part 4: Tensile vibration Non-resonance method
- Part 5: Flexural vibration Non-resonance method
- Part 6: Shear vibration Non-resonance method
- Part 7: Torsional vibration Non-resonance method
- Part 8: Longitudinal and shear vibration Wave-propagation method
- Part 9: Tensile vibration Sonic-pulse propagation method
- Part 10: Complex shear viscosity using a parallel-plate oscillatory rheometer

### Plastics — Determination of dynamic mechanical properties —

#### Part 2:

### Torsion-pendulum method

#### 1 Scope

This part of ISO 6721 specifies two methods (A and B) for determining the linear dynamic mechanical properties of plastics, i.e. the storage and loss components of the torsional modulus, as a function of temperature, for small deformations within the frequency range from 0,1 Hz to 10 Hz.

The temperature dependence of these properties, measured over a sufficiently broad range of temperatures (for example from –50 °C to +150 °C for the majority of commercially available plastics), gives information on the transition regions (for example the glass transition and the melting transition) of the polymer. It also provides information concerning the onset of plastic flow. The two methods described are not applicable to non-symmetrical laminates (see ISO 6721-3, *Plastics — Determination of dynamic mechanical properties — Part 3: Flexural vibration — Resonance-curve method).* The methods are not suitable for testing rubbers, for which the user is referred to ISO 4664-2, *Rubber, vulcanized or thermoplastic — Determination of dynamic properties — Part 2: Torsion pendulum methods at low frequencies.* 

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## 2 Normative references ds.iteh.ai/catalog/standards/sist/d0369802-db6f-46ce-a0c6-92d38ec9e7c8/iso-6721-2-2008

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 6721-1:2001, Plastics — Determination of dynamic mechanical properties — Part 1: General principles

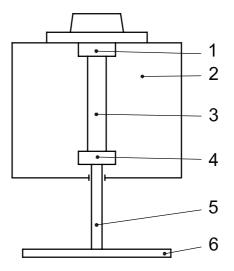
#### 3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 6721-1:2001, Clause 3, apply.

#### 4 Principle

A test specimen of uniform cross-section is gripped by two clamps, one of them fixed and the other connected to a disc, which acts as an inertial member, by a rod. The end of the specimen connected to the disc is excited, together with the disc, to execute freely decaying torsional oscillations. The oscillation mode is that designated IV in ISO 6721-1:2001, Table 2, and the type of modulus is  $G_{to}$  as defined in ISO 6721-1:2001, Table 3.

The inertial member is suspended either from the specimen (method A, see Figure 1) or from a wire (method B, see Figure 2). In the latter case, the wire is also part of the elastically oscillating system.

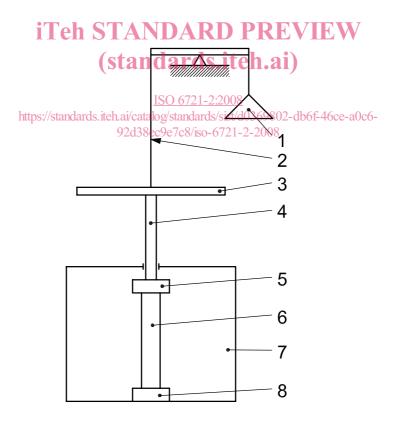


#### Key

- 1 upper (fixed) clamp
- 2 temperature-controlled chamber
- 3 test specimen

- 4 lower (movable) clamp
- 5 rod
- 6 inertial member

Figure 1 — Apparatus for method A



#### Key

- 1 counterweight
- 2 wire
- 3 inertial member
- 4 rod

- 5 upper (movable) clamp
- 6 test specimen
- 7 temperature-controlled chamber
- 8 lower (fixed) clamp

Figure 2 — Apparatus for method B

During a temperature run, the same inertial member can be used throughout the whole run, which results in a frequency decreasing naturally with increasing temperature, or the inertial member can be replaced at intervals by a member of different moment of inertia in order to keep the frequency approximately constant.

During the test, the frequency and the decaying amplitude are measured. From these quantities, the storage component  $G'_{to}$  and loss component  $G''_{to}$  of the torsional complex modulus  $G^*_{to}$  can be calculated.

#### 5 Test apparatus

#### 5.1 Pendulum

Two types of torsion pendulum are specified for use with this part of ISO 6721:

- a) the inertial member is suspended from the test specimen and the lower end of the specimen is excited (method A, Figure 1);
- b) the inertial member is suspended from a wire attached to a counterweight and the upper end of the specimen is excited (method B, Figure 2).

Both types of pendulum consists of an inertial member, two clamps for gripping the specimen (one of which is connected to the inertial member by a rod) and a temperature-controlled chamber enclosing the specimen and the clamps. For method B, a counterweight and connecting wire are also required.

# 5.2 Inertial membei Teh STANDARD PREVIEW 5.2.1 General (standards.iteh.ai)

The moment of inertia, *I*, of the inertial member which may be made of aluminium, for instance, shall be selected as a function of the torsional stiffness of the specimen; so that the temperature-dependent natural frequency of the system lies between approximately 0.11 Hz and 10 Hz.

When testing standard specimens (see 6.2), a moment of inertia, I, of about  $3 \times 10^{-5}$  kg·m<sup>2</sup> is recommended if the same inertial member is to be used throughout a run.

NOTE For certain materials, e.g. filled polymers, a value of I of about  $5 \times 10^{-5}$  kg·m<sup>2</sup> may be necessary.

If a constant frequency is desired over a broad temperature range, interchangeable inertial members with different values of I may be used, thereby permitting the moment of inertia to be varied in steps of less than 20 %, i.e. the frequency to be corrected in steps of less than 10 %. When testing standard specimens (see 6.2) at a frequency of about 1 Hz, a maximum moment of inertia of about  $3 \times 10^{-3}$  kg·m<sup>2</sup> is recommended.

#### 5.2.2 Method A (see Figure 1)

The total mass of the inertial member, the lower clamp and the connecting rod shall be such that the weight, W, carried by the specimen is not too high [see Annex A, Equation (A.2)].

#### 5.2.3 Method B (see Figure 2)

The total mass of the inertial member, the upper clamp and the rod must be balanced by a suitable counterweight, so that the longitudinal force, W, acting on the specimen is minimized [see Annex A, Equation (A.2)]. The wire supporting these parts is part of the elastically oscillating system.

#### 5.3 Clamps

The clamps shall be designed to prevent movement of the portion of the specimens gripped within them. They shall be self-aligning in order to ensure that the specimen axis remains aligned with the axis of rotation and

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the test specimen remains adequately secured over the whole temperature range without distortion occurring, thus allowing the free length of the specimen to be accurately determined.

The movable clamp shall be of low mass.

The moment of inertia of the whole system (consisting of the movable clamp, the inertial member and the connecting rod) shall be determined experimentally.

To prevent heat passing from the specimen out of the temperature-controlled chamber and in the opposite direction, the rod connecting the movable clamp and the inertial member shall be thermally non-conducting.

#### 5.4 Oscillation-inducing device

The oscillation-inducing device shall be capable of applying to the pendulum a torsional impulse such that the pendulum oscillates initially through an angle of not more than 1,5° in each direction for normal materials, or not more than 3° in each direction for low-modulus materials (such as elastomers).

#### 5.5 Oscillation-frequency and oscillation-amplitude recording equipment

Optical, electrical or other recording systems may be used provided they have no significant influence on the oscillating system. The entire equipment for measuring frequency and amplitude shall be accurate to  $\pm$  1 % (within the transition region  $\pm$  5 %).

### 5.6 Temperature-controlled chamber

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See ISO 6721-1:2001, Subclause 5.3.

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#### 5.7 Gas supply

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See ISO 6721-1:2001, Subclause 5:14 lards.iteh.ai/catalog/standards/sist/d0369802-db6f-46ce-a0c6-92d38ec9e7c8/iso-6721-2-2008

#### 5.8 Temperature-measurement device

See ISO 6721-1:2001, Subclause 5.5.

#### 5.9 Devices for measuring test-specimen dimensions

See ISO 6721-1:2001, Subclause 5.6.

#### 6 Test specimens

#### 6.1 General

See ISO 6721-1:2001, Clause 6.

#### 6.2 Shape and dimensions

Rectangular test specimens having the following dimensions are recommended:

free length, *L*: 40 mm to 120 mm, preferably 50 mm

width, *b*: 5 mm to 11 mm, preferably 10 mm

thickness, *h*: 0,13 mm to 2 mm, preferably 1 mm

Specimens which are rectangular in cross-section but whose thickness and/or width varies along the main axis of the specimen by more than 3 % of the mean value shall not be used. When comparing different materials, the dimensions of the specimens shall be identical. Specimen dimensions differing from the preferred ones (50 mm  $\times$  10 mm  $\times$  1 mm) should be chosen to conserve geometric similarity with the preferred specimen shape.

Alternative specimen shapes may be used (e.g. cylindrical or tubular); in such cases, dimensions and tolerances shall be agreed upon by the interested parties.

#### 6.3 Preparation

See ISO 6721-1:2001, Subclause 6.3.

#### 7 Number of specimens

See ISO 6721-1:2001, Clause 7.

#### 8 Conditioning

See ISO 6721-1:2001, Clause 8.

If mechanical conditioning of the specimen is required, the specimen shall be twisted through an angle greater than 5°, but less than 90° in both directions about the torsional-test axis and returned to its normal position.

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#### 9 Procedure

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**9.1 Test atmosphere** standards.iteh.ai/catalog/standards/sist/d0369802-db6f-46ce-a0c6-92d38ec9e7c8/iso-6721-2-2008

See ISO 6721-1:2001, Subclause 9.1.

#### 9.2 Measurement of specimen cross-section

See ISO 6721-1:2001, Subclause 9.2.

#### 9.3 Mounting the test specimens

Clamp the test specimen between the upper and lower clamps. The longitudinal axis of the test specimen shall coincide with the axis of rotation of the oscillating system. Any misalignment of the specimen will cause lateral oscillations that will interfere with the normal oscillation process.

After clamping the test specimen, measure the distance between the clamps (the free length L) to  $\pm$  0,5 %. When setting up the oscillating system in the chamber, check to make sure that the test specimen is not stressed.

After assembling the oscillating system complete with test specimen, and checking its alignment, start the heating or cooling (see 9.4).

#### 9.4 Varying the temperature

See ISO 6721-1:2001, Subclause 9.4.

#### 9.5 Performing the test

Start the free oscillations by setting the pendulum (5.1) in motion using the oscillation-inducing device (5.4).

Record the oscillation frequency and the oscillation amplitude as it decays.

Check that no amplitude decay is caused either by friction between moving and fixed parts of the apparatus or non-linear behaviour of the material under test (see ISO 6721-1:2001, Annex B).

If the frequency is kept fixed during a temperature run, ensure that the inertial member is changed as and when necessary.

#### 10 Expression of results

#### 10.1 Symbols and correction factors

- b width, in metres, of a rectangular specimen
- h thickness, in metres, of a rectangular specimen
- L free length, in metres, of specimen
- I moment of inertia, expressed in kilogram metre squared ( $kg \cdot m^2$ ), of the inertial member (if appropriate, including the movable clamp and the connecting rod)
- $f_{\rm d}$  frequency, in hertz, of the damped oscillating system en. 21
- $f_0$  frequency, in hertz, of the pendulum as used in method B, without the specimen

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- 1 logarithmic decrement for damped oscillations of pendulum plus specimen
- $\Lambda_0$  logarithmic decrement for damped oscillations of a method B pendulum, without the specimen
- $F_{
  m g}$  so-called dimensional factor for the specimen, expressed in reciprocal cubic metres (m $^{-3}$ )

For specimens with a rectangular cross-section:

$$F_{\mathsf{q}} = 3L/bh^3F_{\mathsf{c}} \tag{1}$$

where  $F_{c}$  is the so-called dimensional correction factor.

When  $0 \le h/b \le 0.6$ 

$$F_{\rm c} = 1 - 0.63h/b \tag{2}$$

When  $0.6 \le h/b \le 1$ 

$$F_{\rm c} = 0.843/(1 + h^2/b^2) \tag{3}$$

For specimens with a circular cross-section:

$$F_{\mathsf{q}} = 32L/\pi d^4 \tag{4}$$

where d is the diameter, in metres, of the specimen.

 $F_{\mathsf{d}}$  damping correction factor, given by the equation

$$F_{d} = 1 - (\Lambda/2\pi)^{2} \tag{5}$$

 $G'_{to}$  torsional storage modulus, in pascals, of the specimen

 $G''_{to}$  torsional loss modulus, in pascals, of the specimen

NOTE 1 For reasons given in Annex B, the symbol  $F_{\rm d}$  used for the damping correction factor has a different subscript from that used previously in ISO 537 (now withdrawn).

NOTE 2 Equations (2) and (3) are only approximately valid, the maximum error being 0,9 % (see Annex C).

NOTE 3 The dimensional factor does not include any length corrections to allow for clamping effects. Therefore, only measurements carried out on specimens with the same thickness, width and length ratios will yield accurately comparable results (see ISO 6721-1:2001, Table 1 and Note 6 to Definition 3.1).

#### 10.2 Calculation of logarithmic decrement, $\Lambda$

The logarithmic decrement,  $\Lambda$ , may be calculated using the following equation:

$$\Lambda = \ln \left( X_q / X_{q+1} \right) \tag{6}$$

where  $X_q$  and  $X_{q+1}$  are the amplitudes of two successive oscillations in the same direction (see ISO 6721-1:2001, Definition 3.10).

To calculate  $\Lambda$  from the amplitudes of any two oscillations p and q in the same direction, use the equation

$$\Lambda = \frac{1}{p-q} \ln \left( X_{qh} / X_{p'} \right) \text{ and ards. iteh. ai/catalog/standards/sist/d0369802-db6f-46ce-a0c6-92d38ec9e7c8/iso-6721-2-2008}$$
(7)

where

 $X_n$  is the amplitude of the pth oscillation;

 $X_q$  is the amplitude of the qth oscillation.

The following equation shall be used in the case of amplitudes that cannot be recorded on a damped sinusoidal curve with an accurate baseline (see Figure 3):

$$\Lambda = \ln\left(X_q^* / X_{q+1}^*\right) = \frac{1}{p-q} \ln\left(X_q^* / X_p^*\right) \tag{8}$$

where  $\boldsymbol{X}_{p}^{\star},...,$   $\boldsymbol{X}_{q}^{\star},$   $\boldsymbol{X}_{q+1}^{\star}$  are the differences between successive positive and negative amplitudes of the oscillation concerned,

i.e. 
$$X_q^* = X_q^+ - X_q^-$$

NOTE Equation (8) only corrects for a constant shift in the baseline, not for a time-dependent baseline drift. A time-dependent baseline drift may be caused by the non-oscillating part of the relaxation process, following application of the single pulse to start the system oscillating. It can be decreased by using double-pulse starting, with each pulse applied in a different direction.