



Designation: C 692 – 06

# Standard Test Method for Evaluating the Influence of Thermal Insulations on External Stress Corrosion Cracking Tendency of Austenitic Stainless Steel<sup>1</sup>

This standard is issued under the fixed designation C 692; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reapproval.

## 1. Scope

1.1 This test method covers two procedures for the laboratory evaluation of thermal insulation materials to determine whether they contribute to external stress corrosion cracking (ESCC) of austenitic stainless steel due to soluble chlorides within the insulation. This laboratory procedure is not intended to cover all of the possible field conditions that contribute to ESCC.

1.2 While the 1977 edition of this test method (Dana test) is applicable only to wicking-type insulations, the procedures in this edition are intended to be applicable to all insulating materials, including cements, some of which disintegrate when tested in accordance with the 1977 edition. Wicking insulations are materials that wet through and through when partially (50 to 75 %) immersed in water for a short period of time (10 min or less).

1.3 These procedures are intended primarily as a preproduction test for qualification of the basic chemical composition of a particular manufacturer's product and are not intended to be routine tests for ongoing quality assurance or production lot compliance. Test Methods C 871, on the other hand, is used for confirmation of acceptable chemical properties of subsequent lots of insulation previously found acceptable by this test method.

1.4 The values stated in inch-pound units are to be regarded as the standard. The values given in parentheses are for information only.

1.5 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

<sup>1</sup> This test method is under the jurisdiction of ASTM Committee C16 on Thermal Insulation and is the direct responsibility of Subcommittee C16.31 on Chemical and Physical Properties.

Current edition approved April 1, 2006. Published May 2006. Originally approved in 1971. Last previous edition approved 2005 as C 692 – 05.

## 2. Referenced Documents

2.1 *ASTM Standards:*<sup>2</sup>

A 240/A 240M Specification for Chromium and Chromium-Nickel Stainless Steel Plate, Sheet, and Strip for Pressure Vessels and for General Applications

A 370 Test Methods and Definitions for Mechanical Testing of Steel Products

C 795 Specification for Thermal Insulation for Use in Contact with Austenitic Stainless Steel

C 871 Test Methods for Chemical Analysis of Thermal Insulation Materials for Leachable Chloride, Fluoride, Silicate, and Sodium Ions

G 30 Practice for Making and Using U-Bend Stress-Corrosion Test Specimens

## 3. Summary of Test Method

3.1 The procedures in this test method consist of using a specimen of insulation to conduct distilled (or deionized) water by wicking or dripping to an outside surface, through the insulation, to a hot inner surface of stressed Type 304 stainless steel for a period of 28 days. If leachable chlorides are present, they are carried along with the water and concentrated at the hot surface by evaporation in much the same way as has been experienced in actual industrial process situations.

3.2 Exposed stainless steel coupons are examined visually, and under 10 to 30 $\times$  magnification, if necessary, to detect ESCC after the prescribed period of exposure.

## 4. Significance and Use

4.1 An inherent characteristic of some alloys of austenitic stainless steel is their tendency to crack at stress points when exposed to certain corrosive environments. The mechanisms of ESCC are complex and not completely understood but are

<sup>2</sup> For referenced ASTM standards, visit the ASTM website, [www.astm.org](http://www.astm.org), or contact ASTM Customer Service at [service@astm.org](mailto:service@astm.org). For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

apparently related to certain metallurgical properties. Chloride ions concentrated at a stress point will catalyze crack formation. It has been reported that other halide ions do not promote ESCC to the same degree as does chloride using the test technology of Test Method C 692 (drip test).<sup>3</sup>

4.2 Chlorides are common to many environments, so great care shall be taken to protect austenitic stainless steel from chloride contamination.

4.3 Most thermal insulations will not, of themselves, cause stress corrosion cracking as shown by qualification tests. When exposed to elevated-temperature (boiling point range), environments containing chlorides, moisture, and oxygen, however, some insulation systems act as collecting media, trans-migrating and concentrating chlorides on heated stainless steel surfaces. If moisture is not present, the chloride salts cannot migrate, and stress corrosion cracking because of chloride-contaminated insulation cannot take place.

4.4 Insulation materials are available that are specially formulated to inhibit stress corrosion cracking in the presence of chlorides through modifications in basic composition or incorporation of certain chemical additives.

4.5 The ability of the 28-day test to measure the corrosion potential of insulation materials is documented by Karnes,<sup>4</sup> whose data appear to have been used for construction of the acceptability curve used in Specification C 795 and other specifications.

4.6 The metal for all of the coupons used in this test method (C 692) shall be qualified (see Section 13) to ascertain that under conditions of the test, chloride ions will cause the metal to crack, and deionized water alone will not cause cracks.

**5. Applicability (see also 10.2)**

5.1 While the original test procedure for the 1977 edition of this test method (Dana Test) was limited to “wicking-type insulations,” the “drip test procedure” given in this edition is applicable to all insulations when cut or formed into the required test specimen.

5.2 Heat treatment at some temperature (as recommended by the manufacturer) up to the maximum use temperature is sometimes necessary to make the insulating material “wick,” and thus testable by either insulation test procedure (see Sections 11 and 12).

5.3 If the test insulation cannot be made to wick in any way (such as in the case of organic or inorganic closed-cell foams), or when heat treatment of a component of the insulation (such as an attached exterior jacket material) exceeds the manufacturer’s recommended maximum temperature for the exterior component, then the 1½-in. (38-mm) wide test specimen is sliced into two ¾-in. (19-mm) thick segments. The two halves are held together with wire, pins, or a rubber band, and are tested by dripping into the crack between the two halves, thus simulating the situation where water penetrates the junction

between two sections of insulation. Wetting the mating faces on the two half sections facilitates water wicking down to the coupon surface.

5.4 Adhesives are tested by gluing together a test block of the insulation material to be used with the adhesive. The adhesive joint must come into contact with the stainless steel test coupon.

5.5 Cements with a clay binder are tested by casting a 1½-in. (38-mm) thick slab, drying, and using the drip procedure. Such a sample will disintegrate in the Dana test procedure.

5.6 The drip procedure has the potential to be used for the testing of coatings applied to the coupon prior to test. The corrosive liquids dripped into such a system are limited only by the imagination of the researcher.

**6. Apparatus for Dana Test Procedure**

6.1 *Enclosure*—In dusty environments, it is permissible for the test apparatus to be located in a cabinet or other closed structure provided with a blower to maintain a positive internal pressure, and equipped with a filter for intake air to minimize dust or other contamination. The test apparatus is normally housed in any suitable clean environment not subject to chloride contamination. The enclosure shall not be so tight as to exclude oxygen from the system, since oxygen is necessary for ESCC to occur.

6.2 *Pyrex Glass Wool.*

6.3 “*Cookie Cutter,*” made from ¼ in. (32 mm) thin wall electrical conduit (inside diameter 1.38 in. (35 mm)) to cut a 1⅜-in. (35-mm) diameter plug from 2-in. (51-mm) Pyrex Glass Wool.

6.4 *Specimen Holder,* as shown in Fig. 1, or equivalent.

6.5 *Precision Bender,* see Practice G 30.

6.6 *Wet-Grinding Belt Grinder,* 80-grit.

6.7 *Copper Lugs,* commercial 2/0–4/0 solderless, or 2 by ½ by ⅛ in. (51 by 13 by 3.2 mm) copper tabs.

6.8 *Silver Solder,* and chloride-free flux for use with stainless steel.

6.9 *Torch,* acetylene or propane.

6.10 *Bolt,* stainless steel, ⅜ in. (5 mm) in diameter and 2½-in. (65-mm) long with insulating washer and nut for electrically insulating the bolt from the U-bend specimen.

6.11 *Hand-Held Magnifier,* 10× or 30× binocular microscope, or both.

6.12 *Band Saw.*

6.13 *Hole Saw,* 2-in. (51-mm) outside diameter (optional).

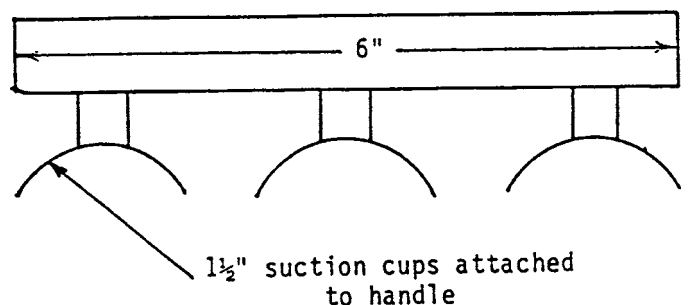


FIG. 1 Suction Cup Coupon Holder

<sup>3</sup> Private communication from authors of paper presented at Bal Harbour ASTM C16 Symposium on December 9, 1987. Whitaker, T. E., Whorlow, K. M., and Hutto, F. B., Jr., “New Developments in Test Technology for ASTM C692.”

<sup>4</sup> Karnes, H. F., “The Corrosion Potential of Wetted Thermal Insulation,” AICHE, 57th National Meeting, Minneapolis, MN, September 26 through 29, 1965.

6.14 *Crystallizing Dish*, of borosilicate glass, 7½ in. (190 mm) in diameter by 4 in. (100 mm) in depth, or stainless steel pan 9½ by 5½ by 4 in. (41 by 140 by 102 mm) deep.

6.15 *Electrical Transformer*, isolation-type. (approximately 150 mV/150 AMP).

6.16 *Thermocouple*, 28 gage or smaller.

6.17 *Epoxy Adhesive*, aluminum filled.

6.18 *Drill Bit*, ⅜-in. (7-mm), cobalt steel preferred.

6.19 *Dye Penetrant and Developer*, available at most welding supply houses.

## 7. Apparatus for Drip Test Procedure

7.1 *Steam Heated Pipe*—A 5-ft (1.5-m) section of 1½ in. IPS pipe (inconel or other corrosion-resistant material), is heated either by a small self-contained steam boiler or by regulated house steam.

7.2 *Peristaltic Pump*—A multichannel peristaltic pump is used to supply 250 (±25) mL/day to each specimen.

7.3 *I.V. Bottles*, 1 L or equivalent, to individually supply each test specimen with test liquid.

7.4 *Specimen Holder*, for grinding. See Fig. 1.

7.5 *Precision Bender*, see Fig. 2 in the 1979 edition of Practice G 30.

7.6 *Wet-Sanding Belt Sander*, with 80-grit belt.

7.7 *Bolt*, stainless steel, ⅜ in. (5 mm) in diameter by 2½-in. (65-mm) long with nut.

7.8 *Hole Saw*, 2-in. (51-mm) outside diameter.

7.9 *Band Saw*.

7.10 *Thermocouple*, 28 gage or smaller.

7.11 *Heat Transfer Grease*, chloride free.

7.12 *Kimwipe Tissue*,<sup>5</sup> chloride free.

## 8. Reagents and Materials

8.1 *Distilled or Deionized Water*, containing less than 0.1 ppm chloride ions.

8.2 *Distilled or Deionized Water*, containing 1500 ppm chloride ion (2.473 g NaCl/L).

8.3 *Type 304 Stainless Steel Sheet*—16 gage, meeting the composition requirements of Specification A 240/A 240M. Certificates of chemical composition and mechanical properties, including ultimate tensile strength and yield strength by the 0.2 % offset method are required. Type 304 stainless steel meeting Specification A 240/A 240M shall have a carbon content in the range of 0.05–0.06 % and shall be solution-annealed.

## 9. Test Coupons

9.1 Shear 2 by 7-in. (51 by 178-mm) coupons from 16-gage Type 304 stainless sheet, as specified in 8.3, with the long dimension parallel to the long dimension of the sheet. (Long dimension parallel to sheet-rolling direction.)

9.2 Clean coupons with chloride-free liquid soap and water to remove any grease or other contamination.

9.3 Sensitize all coupons before bending by heating at 1200°F (649°C) in an argon (inert) or air (oxidizing) atmosphere for three hours. Let cool in the furnace after the sensitizing period.<sup>6</sup> Temperature of the coupons must be measured in the stack of coupons, not in the furnace itself, as the coupon temperatures “lag” the furnace temperature by at least 50 to 100°F (28 to 56°C).

9.4 A suggestion for sensitizing in an inert atmosphere is to use a stainless steel box with a tight-fitting cover to contain the argon around the coupons during sensitization.

9.5 Grip coupon with suction cup holder (see Fig. 1) or other means to facilitate wet grinding on an 80-grit belt grinder. Grind parallel to the long dimension of the coupon using an 80-grit wet belt with just enough pressure to remove the dull finish and leave the metal bright. Do not overgrind. The beltground face is the test surface to be exposed to the thermal insulation. The test area is the bent coupon surface that actually comes into contact with the insulation.

9.6 Smooth and round sheared edges to prevent accidental cutting of fingers.

9.7 Bend each ground coupon to a 1.00 ± 0.01-in. (25.4 ± 0.25-mm) outside radius using a roll bender as shown in Fig. 5 of the 1979 edition of Practice G 30 to produce a U-shape in which the “legs” are parallel to within ⅛ in. (1.6 mm).

9.8 Drill or punch a ⅜-in. (7-mm) hole in each end using the special jig shown in Fig. 3. Cobalt steel drill bits are used on 304 stainless steel as other bits dull quickly.

9.9 For the Dana test only, silver-solder a 2/0–4/0 solderless copper electrical connector to each leg with the hole in the connector centered on the drilled hole. While it has been conventional to solder one lug to an inside surface and the second to an outside surface, it is acceptable to solder both to outside surfaces for greater convenience. The body of the coupon is shielded from high soldering temperatures by placing a soaking-wet chloride-free cellulose pad on the coupon next to the weld area to act as a heat sink. Carefully remove all flux from the finished coupon by washing with hot

<sup>5</sup> Kimwipe is a trademarked product of Kimberly-Clark Corp., Roswell, GA.



FIG. 2 Typical External Stress Corrosion Cracks (5× Magnification)

<sup>6</sup> For a discussion of the effect of sensitizing stainless steel and its susceptibility to stress corrosion, refer to “Stress-Corrosion Cracking of Sensitized Stainless Steel in Oxygenated High Temperature Water,” Batelle Columbus Laboratories, Report No. BMI 1927, June 1972.