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## Personal protective equipment — Test methods for sunglasses and related eyewear

*Équipement de protection individuelle — Méthodes d'essai pour lunettes de soleil et articles de lunetterie associés*

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## Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2. [www.iso.org/directives](http://www.iso.org/directives)

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights. Details of any patent rights identified during the development of the document will be in the Introduction and/or on the ISO list of patent declarations received. [www.iso.org/patents](http://www.iso.org/patents)

Any trade name used in this document is information given for the convenience of users and does not constitute an endorsement.

The committee responsible for this document is ISO/TC 94, *Personal safety — Protective clothing and equipment*, Subcommittee SC 6, *Eye and face protection*.

This corrected version of ISO 12311:2013 incorporates the following correction:

— the second paragraph of 9.7.3.1 has been added.

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# Personal protective equipment — Test methods for sunglasses and related eyewear

## 1 Scope

This International Standard specifies reference test methods for determining the properties of sunglasses given in ISO 12312 (all parts). It is applicable to all sunglasses and related eyewear.

Other test methods may be used if proven to be equivalent.

## 2 Normative references

The following documents, in whole or in part, are normatively referenced in this document and are indispensable for its application. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 37, *Rubber, vulcanized or thermoplastic — Determination of tensile stress-strain properties*

ISO 48, *Rubber, vulcanized or thermoplastic — Determination of hardness (hardness between 10 IRHD and 100 IRHD)*

ISO 1042:1998, *Laboratory glassware — One-mark volumetric flasks*

ISO 3696:1987, *Water for analytical laboratory use — Specification and test methods*

ISO 4007, *Personal protective equipment — Eye and face protection — Vocabulary*

ISO 8596, *Ophthalmic optics — Visual acuity testing — Standard optotype and its presentation*

ISO 11664-1, *Colorimetry — Part 1: CIE standard colorimetric observers*

ISO 11664-2, *Colorimetry — Part 2: CIE standard illuminants*

ISO 12312-1:2013, *Eye and face protection — Sunglasses and related eyewear — Part 1: Sunglasses for general use*

ISO/IEC Guide 98-3:2008, *Uncertainty of measurement — Part 3: Guide to the expression of uncertainty in measurement (GUM:1995)*

## 3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 4007 apply.

## 4 Prerequisites

The following parameters shall be specified prior to testing [see ISO 12312 (all parts)]:

- the number of specimens;
- specimen preparation;
- any conditioning prior to testing;
- characteristics to be assessed subjectively (inappropriate);

— pass/fail criteria.

## 5 General test requirements

Unless otherwise specified, the values stated in this International Standard are expressed as nominal values. Except for temperature limits, values which are not stated as maxima or minima shall be subject to a tolerance of  $\pm 5$  %. Unless otherwise specified, the ambient temperature for testing shall be between 16 °C and 32 °C. Where other temperature limits are specified they shall be subject to an accuracy of  $\pm 1$  °C. Relative humidity shall be maintained at  $(50 \pm 20)$  %.

Unless otherwise specified, the filters shall be tested at the reference points as defined in ISO 4007.

## 6 Test methods for assessing the construction and materials

### 6.1 Prior assessment of construction, marking and information

Prior to applying the test methods, a visual inspection shall be carried out with normal or corrected vision, without magnification. Marking and information supplied by the manufacturer and safety data sheets (if applicable) or declaration relevant to the materials used in its construction shall also be assessed.

### 6.2 Test method for assessment of filter material and surface quality

#### 6.2.1 Principle

The quality of the filter material and surface is assessed by visual inspection.

#### 6.2.2 Apparatus

A suitable apparatus is shown in [Figure 1](#).

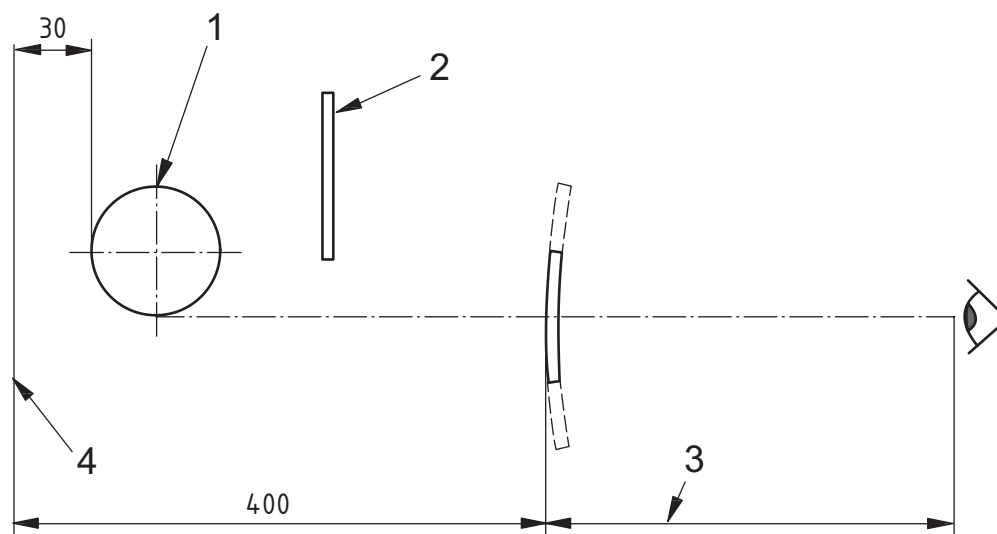
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Dimensions in millimetres

**Key**

- 1 lamp
- 2 adjustable opaque dull black mask
- 3 near vision distance ( $\approx 300$ )
- 4 dull black background ( $200 \times 360$ )

**Figure 1 — Arrangement of apparatus for assessment of quality of material and surface**

**6.2.3 Test procedure**

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Carry out the assessment of the quality of material and surface by visual inspection with the aid of a “light box” or illuminated grid.

**NOTE** One method of inspection in current use consists of an illuminated grid as a background to be viewed through the filter which is held at various distances from the eye. Another method is to illuminate the filter by means of a fluorescent lamp mounted within a dull black chamber and with the amount of illumination adjusted by means of an adjustable opaque black mask. A suitable arrangement is shown in [Figure 1](#).

**6.2.4 Verification and test report**

Except for a marginal area 5 mm wide at the edge of the eye protector, any significant defects likely to impair vision in use shall be recorded in the verification and test report.

**7 Test methods for measuring spectrophotometric properties****7.1 Measurement of spectral transmittance  $\tau(\lambda)$** **7.1.1 Spectral transmittance****7.1.1.1 General**

Test methods shall be used which have relative uncertainties in spectral transmittance less than or equal to those given in [Table 1](#).

**Table 1 — Relative uncertainty of measured spectral transmittance**

Spectral transmittance value		Uncertainty %
Less than %	to %	
100	17,8	±2 absolute
17,8	0,44	±10 relative
0,44	0,023	±15 relative
0,023	0,0012	±20 relative
0,0012	0,000023	±30 relative

The general methods of evaluating the components of uncertainty are set out in ISO/IEC Guide 98-3. [Annex A](#) shows how uncertainty of measurement is to be applied in the reporting of results and compliance and [Annex B](#) is a guide to the sources of uncertainty in spectrophotometry, their minimization and evaluation.

The location and direction of measurement of transmittance shall be as specified in ISO 12312-1. If the measurements are not made normal to the surface of the filter, then particular attention should be paid to the effects of beam displacement (see [Annex B](#)). If the direction of measurement is not specified then it shall be measured normal to the surface of the filter when unmounted.

Calculations shall be carried out at not more than 5 nm intervals ( $\Delta\lambda = 5$  nm) in the ultraviolet-visible region (280 nm to 780 nm) and not more than 10 nm in the infrared region (780 nm to 2 000 nm). The necessary data at these intervals are provided in [Annexes D, E, F, H and I](#).

#### 7.1.1.2 Test procedure

Place the filter in order to follow the location and direction of measurement of transmittance as specified in ISO 12312-1.

#### 7.1.2 Calculations of luminous transmittance $\tau_v$

Luminous transmittance is calculated as a percentage from the spectral transmittances and with reference to a standard observer and a source or illuminant. For the purposes of this International Standard all calculations use the CIE 2° Standard Observer [ISO 11664-1 and CIE Standard Illuminant D65 (ISO 11664-2)].

$$\tau_v = 100 \times \frac{\int_{380}^{780} \tau(\lambda) \cdot S_{D65}(\lambda) \cdot V(\lambda) \cdot d\lambda}{\int_{380}^{780} S_{D65}(\lambda) \cdot V(\lambda) \cdot d\lambda} \quad (1)$$

where

$\lambda$  is the wavelength of the light in nanometres;

$\tau(\lambda)$  is the spectral transmittance of the filter;

$V(\lambda)$  is the spectral luminous efficiency function for photopic vision;

$S_{D65}(\lambda)$  is the spectral distribution of radiation of CIE Standard Illuminant D65 (see ISO 11664-2).

The values of  $S_{D65}(\lambda) \cdot V(\lambda)$  are given in [Annex D](#).

NOTE These calculations are normally carried out as summations and not as integrations. The equivalent summations are provided in [Annex C](#).

## 7.2 Measurement of uniformity of luminous transmittance

### 7.2.1 Unmounted filters covering one eye

#### 7.2.1.1 Test method

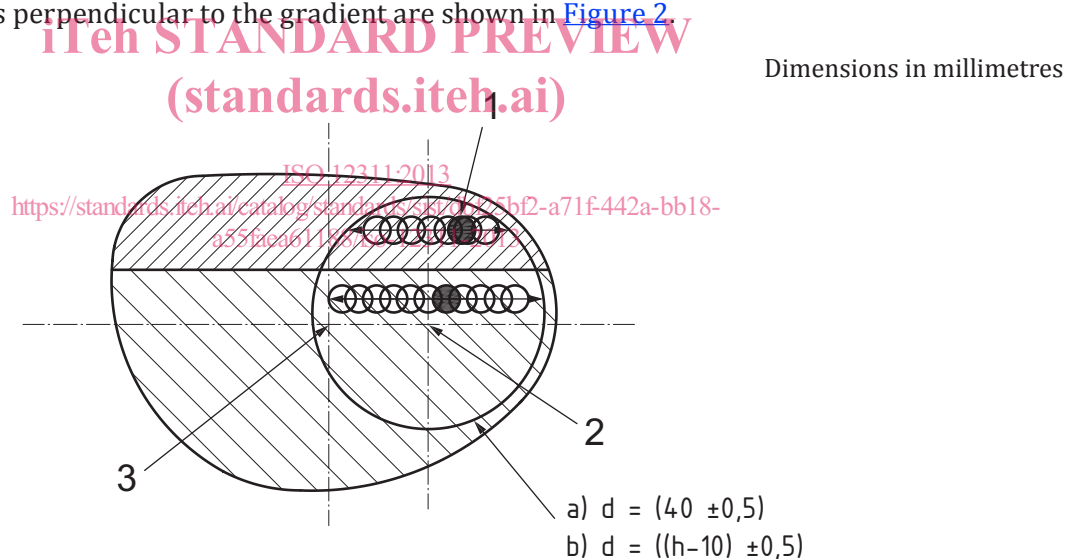
Locate the defined reference point defined in ISO 4007. Determine a circular area around the reference point with diameter  $d$  calculated as follows (see [Figure 2](#)):

- for filters equal to or greater than 50 mm in vertical depth at the reference point,  $d = (40,0 \pm 0,5)$  mm;
- for filters less than 50 mm in vertical depth at the reference point,  $d = [\text{vertical depth of filter (h)} - 10 \pm 0,5]$  mm.

A 5 mm wide portion around the edge of the filter shall be excluded from this circular area.

Scan this circular area with a 5 mm nominal diameter light beam white light or a narrow spectral band with a maximum spectral energy at  $(555 \pm 25)$  nm and measure the luminous transmittance with a detector whose spectral responsivity approximates that of the CIE 2° Standard Observer (ISO 11664-1). The effects of displacement of the light beam by any prismatic effect of the filter (see [B.3.4.1](#)) shall be compensated for, and variations in thickness shall be corrected as in [Annex L](#).

For filters with bands or gradients of different luminous transmittance, the requirement for variations in luminous transmittance applies in this circular area but perpendicular to the gradient (see [Figure 2](#)). Two example scans perpendicular to the gradient are shown in [Figure 2](#).



#### Key

- 1 light beam 5 mm diameter
- 2 reference point
- 3 geometric or boxed centre

**Figure 2 — Luminous transmittance uniformity measurement for filters with bands or gradients of different luminous transmittance**

The filter and the light beam are positioned so that the incident light falls normally on the surface of the filter at the reference point or parallel to that direction at other locations on the filter.

Measure and record the maximum value of luminous transmittance  $\tau_{vmax}$ , and the minimum value of luminous transmittance  $\tau_{vmin}$ .

### 7.2.1.2 Calculations

Calculate the value of  $\Delta_F$  as percentage, from the following formulae:

$$\Delta_F = 100 \times \frac{(\tau_{vmax} - \tau_{vmin})}{\tau_{vmax}} \quad (2)$$

where

$\tau_{vmax}$  is the maximum value of luminous transmittance;

$\tau_{vmin}$  is the minimum value of luminous transmittance.

### 7.2.1.3 Test report

Record  $\Delta_F$  as the uniformity of luminous transmittance.

## 7.2.2 Mounted filters and unmounted filters covering both eyes

### 7.2.2.1 Test method

Locate the defined reference points defined in ISO 4007. Define two circular areas around the reference points with diameter  $d$ , calculated as follows:

Circular areas are determined around each of these centres with diameters  $d$ , calculated as follows:

- a) for filters equal to or greater than 50 mm in vertical depth at the reference point,  $d = (40,0 \pm 0,5)$  mm;
- b) for filters less than 50 mm in vertical depth at the reference point,  $d = [\text{vertical depth of filter (h)} - 10 \pm 0,5]$  mm.

A 5 mm wide portion around the edge of the filter shall be excluded from this circular area.

Scan this circular area with a 5 mm nominal diameter light beam white light or a narrow spectral band with a maximum spectral energy at  $(555 \pm 25)$  nm and measure the luminous transmittance with a detector whose spectral responsivity approximates that of the CIE 2° Standard Observer (ISO 11664-1). The effects of displacement of the light beam by the any prismatic effect of the filter (see B.3.4.1) shall be compensated for and variations in thickness shall be corrected as in Annex L.

For filters with bands or gradients of different luminous transmittance, assessments of variations in luminous transmittance shall be for sections parallel to the line joining the reference points.

Measure and record the value of luminous transmittance  $\tau_{VL}$  at the left eye reference point and the value of luminous transmittance  $\tau_{VR}$  at the right eye reference point.

### 7.2.2.2 Calculations

Divide the absolute difference between the values of the luminous transmittance at the two reference points  $\tau_{VL}$  and  $\tau_{VR}$  by the higher value of the luminous transmittance at one of the two reference points and express this ratio, as a percentage  $\Delta_P$ .

$$\Delta_P = 100 \times \frac{|\tau_{VR} - \tau_{VL}|}{\max(\tau_{VR}, \tau_{VL})} \quad (3)$$

where

$\tau_{VL}$  is the value of luminous transmittance at the reference point of the left filter;

$\tau_{VR}$  is the value of luminous transmittance at the reference point of the right filter.

**EXAMPLE** If one filter transmits 38,0 % and the other transmits 40,0 %, then the result is  $100 \times (2,0/40,0) = 5,0$  %.

### 7.2.2.3 Test report

Record the value  $\Delta_P$  as a percentage.

## 7.3 Calculation of ultraviolet transmittance

### 7.3.1 Solar UV-transmittance $\tau_{SUV}$

The calculation of  $\tau_{SUV}$  (see ISO 4007) as a percentage is:

$$\tau_{SUV} = 100 \times \frac{\int_{280}^{380} \tau(\lambda) \cdot E_s(\lambda) \cdot S(\lambda) \cdot d\lambda}{\int_{280}^{380} E_s(\lambda) \cdot S(\lambda) \cdot d\lambda} = 100 \times \frac{\int_{280}^{380} \tau(\lambda) \cdot W(\lambda) \cdot d\lambda}{\int_{280}^{380} W(\lambda) \cdot d\lambda} \quad (4)$$

where

$\lambda$  is the wavelength in nanometres;

$\tau(\lambda)$  is the spectral transmittance;

$E_s(\lambda)$  is the solar radiation at sea level for air mass 2;<sup>[7]</sup>

$S(\lambda)$  is the relative spectral effectiveness function for UV radiation;<sup>[8]</sup>

$W(\lambda) = E_s(\lambda) \cdot S(\lambda)$  and is the complete weighting function of this product.

The values of  $E_s(\lambda)$ ,  $S(\lambda)$  and  $W(\lambda)$  are given in [Annex E](#).

### 7.3.2 Solar UVA-transmittance $\tau_{SUA}$

Solar UVA-transmittance is the result of the mean of the spectral transmittance between 315 nm and 380 nm and appropriate weighting functions.

The calculation of  $\tau_{\text{SUVA}}$  (see ISO 4007) as a percentage is as follows:

$$\tau_{\text{SUVA}} = 100 \times \frac{\int_{315}^{380} \tau(\lambda) \cdot E_{\text{S}}(\lambda) \cdot S(\lambda) \cdot d\lambda}{\int_{315}^{380} E_{\text{S}}(\lambda) \cdot S(\lambda) \cdot d\lambda} = 100 \times \frac{\int_{315}^{380} \tau(\lambda) \cdot W(\lambda) \cdot d\lambda}{\int_{315}^{380} W(\lambda) \cdot d\lambda} \quad (5)$$

where

$\lambda$  is the wavelength in nanometres;

$\tau(\lambda)$  is the spectral transmittance;

$E_{\text{S}}(\lambda)$  is the solar radiation at sea level for air mass 2; [7]

$S(\lambda)$  is the relative spectral effectiveness function for UV radiation; [8]

$W(\lambda) = E_{\text{S}}(\lambda) \cdot S(\lambda)$  and is the complete weighting function of this product.

The values of  $E_{\text{S}}(\lambda)$ ,  $S(\lambda)$  and  $W(\lambda)$  are given in [Annex E](#).

### 7.3.3 Solar UVB-transmittance $\tau_{\text{SUVB}}$

Solar UVB-transmittance is the result of the mean of the spectral transmittance between 280 nm and 315 nm and appropriate weighting functions.

The calculation of  $\tau_{\text{SUVB}}$  (see ISO 4007) as a percentage is as follows:

$$\tau_{\text{SUVB}} = 100 \times \frac{\int_{280}^{315} \tau(\lambda) \cdot E_{\text{S}}(\lambda) \cdot S(\lambda) \cdot d\lambda}{\int_{280}^{315} E_{\text{S}}(\lambda) \cdot S(\lambda) \cdot d\lambda} = 100 \times \frac{\int_{280}^{315} \tau(\lambda) \cdot W(\lambda) \cdot d\lambda}{\int_{280}^{315} W(\lambda) \cdot d\lambda} \quad (6)$$

where

$\lambda$  is the wavelength in nanometres;

$\tau(\lambda)$  is the spectral transmittance;

$E_{\text{S}}(\lambda)$  is the solar radiation at sea level for air mass 2; [7]

$S(\lambda)$  is the relative spectral effectiveness function for UV radiation; [8]

$W(\lambda) = E_{\text{S}}(\lambda) \cdot S(\lambda)$  and is the complete weighting function of this product.

The values of  $E_{\text{S}}(\lambda)$ ,  $S(\lambda)$  and  $W(\lambda)$  are given in [Annex E](#).

#### 7.4 Calculation of solar blue-light transmittance $\tau_{sb}$

Solar blue-light transmittance is the result of the mean of the spectral transmittance between 380 nm and 500 nm and appropriate weighting functions. The calculation of  $\tau_{sb}$  (see ISO 4007) as a percentage is as follows:

$$\tau_{sb} = 100 \times \frac{\int_{380}^{500} \tau(\lambda) \cdot E_s(\lambda) \cdot B(\lambda) \cdot d\lambda}{\int_{380}^{500} E_s(\lambda) \cdot B(\lambda) \cdot d\lambda} = 100 \times \frac{\int_{380}^{500} \tau(\lambda) \cdot W_B(\lambda) \cdot d\lambda}{\int_{380}^{500} W_B(\lambda) \cdot d\lambda} \quad (7)$$

where

$\lambda$  is the wavelength in nanometres;

$\tau(\lambda)$  is the spectral transmittance;

$E_s(\lambda)$  is the solar radiation at sea level for air mass 2; [7]

$B(\lambda)$  is the blue-light hazard function; [9]

$W_B(\lambda) = E_s(\lambda) \cdot B(\lambda)$  and is the complete weighting function of this product.

The values of  $E_s(\lambda)$ ,  $B(\lambda)$  and  $W_B(\lambda)$  are given in Annex E.

#### 7.5 Calculation of solar IR transmittance $\tau_{SIR}$

The calculation of solar IR transmittance  $\tau_{SIR}$  (see ISO 4007) as a percentage is obtained by integration between the limits 780 nm and 2 000 nm as follows:

$$\tau_{SIR} = 100 \times \frac{\int_{780}^{2000} \tau(\lambda) \cdot E_s(\lambda) \cdot d\lambda}{\int_{780}^{2000} E_s(\lambda) \cdot d\lambda} \quad (8)$$

where

$\lambda$  is the wavelength in nanometres;

$\tau(\lambda)$  is the spectral transmittance;

$E_s(\lambda)$  is the spectral distribution of solar radiation at sea level for air mass 2. [7]

The values of  $E_s(\lambda)$  are given in Annex F.

#### 7.6 Measurement of absolute spectral reflectance $\rho(\lambda)$

The test methods to be used shall have relative uncertainties in spectral reflectance less than or equal to those given in Table 2. The angle of incidence is to be  $\leq 17^\circ$